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The wave-induced velocity in an opposing wind predicted Figure 2.2 by potential flow theory. kz is the non-dimensional height above the waves



Figure 2.3 The variation of velocity in a direction perpendicular to the flow induces a difference in the direction of the friction forces and a torque resulting in a rotational motion. [After Le Mehaute (67)]





Figure 2.4a The theoretical wave growth coupling coefficient as a function of C/u_{\star} . [after Phillips (93)].



Figure 2.4b The theoretical wave decay coupling coefficient as a function of C/u_* . [after Phillips (93)].





Figure 2.7 The phase angle of the pressure signal relative to the water surface as a function of C/u_{*}, measured by Longuet-Higgins et al. (74), + ; Shemdin and Hsu (111), • ; and Dobson (26), * . The broken lines indicate the envelope of Kendall's (57) wind tunnel measurements and the continuous curve is calculated from Miles formula (78). [After Phillips 94)]



Figure 2.9 Dimensionless growth (or decay) rates as a function of U/C, following wind, opposing wind. [After Stewart and Teague (124)]

Dimensionless Growth Rate







Photograph of existing wave flume.



Figure 2.10 Definition sketch of stresses exerted at the water surface



Figure 3.3 Dimensions of wave absorbing beach (all dimensions in cms).



WAVE GENERATION













Figure 3.8b Photograph of the complete wind-wave flume.



Figure 3.9 Fan and Flume Characteristics



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flume inlet.

Figure 3.10





Figure 3.13a Cross-section velocity contours within the flume at the beach inlet.







Figure 3.14 Relationship between fan speed and free stream wind velocity.



Figure 3.15

Time series of water surface elevation for sinusoidal wave maker motion at various frequencies.





Figure 3.16a Spectra of water surface elevation for sinusoidal wave maker motion at various frequencies.



frequency = 1.5 Hz



frequency = 2.0 Hz

Figure 3.16b Spectra of water surface elevation for sinusoidal wave maker motion of various frequencies.



Figure 3.17 Transfer functions relating initial command wave record to realized water surface record.













Figure 3.19c Wave maker transfer function at mid-flume working section. Input spectral variance = $1.5 V^2$.



Figure 3.19d Wave maker transfer function at mid-flume working section. Input spectral variance = $2 V^2$.













Figure 3.20 Phase of transfer function between command signal and water surface.



Figure 3.21 Average wave maker transfer function at mid-flume working section.



Figure 3.22 The theoretical transfer function H_3 between the piston stroke and wave as given by Eq. 3.22.



Figure 3.23 Theoretical transfer function between input signal and wave.



Figure 3.24 Average wave maker transfer function at beach station.



Figure 3.25 Comparison between target wave height spectrum and realised spectrum.



Figure 3.26 Comparison of wave height spectra at mid-flume with and without temporary absorbing beach at the wave maker.



Figure 3.27 Water level setup for various values of u*



Figure 4.1 Photograph of wave height probe.



Figure 4.2 Schematic illustration of water surface elevation measurements system.


Figure 4.3 Circuit diagram of bridge for the electrical resistance wave gauges.





Figure 4.5 Typical wave gauge calibration curve.



Figure 4.6 Stability of wave gauge output in still water.



Figure 4.7 Wave follower system.



Figure 4.8 Photograph of wave follower drive system.





Figure 4.9 A comparison of the spectra of water surface elevation and motion of the wave follower.





Figure 4.11 Coherence function between water surface elevation and wave follower position.



Figure 4.12 Spectrum of wave follower position in still water.





Figure 4.14 Dimensions of disk pressure probe.



Figure 4.16 Schematic diagram of pressure recording system.







Schematic diagram of pressure transducer calibration system. Figure 4.18



Figure 4.19 Typical pressure transducer calibration curve.





Figure 4.22 Response of total head probe to pitch or yaw











φ







Figure 4.26a Transfer function between wave follower motion and induced pressure for the disk-static system.



Figure 4.26b Transfer function between wave follower motion and induced pressure for the disk-total system.



Figure 4.29 Mounting and adjustment system for hot film probe.



Figure 4.28a





Figure 4.31 Anemometer cooling laws for the probe at an angle ψ to the fluid flow.



Figure 4.32 1







t(s)

Fan speed = 170 rpm



t(s)



t(s)

Fan speed = 0 rpm

Figure 7.la



t(s)

Fan speed = 230 rpm



t(s)

Fan speed = 205 rpm



t(s) Fan speed = 185 rpm

Figure 7.1b



t(s)

Fan speed = 310 rpm



t(s)



t(s) Fan speed = 260 rpm

Figure 7.1c



t(s) Fan speed = 415 rpm



t(s)



t(s) Fan speed = 345 rpm

Figure 7.1d



t(s)

Fan speed = 550 rpm



t(s) Fan speed = 500 rpm



t(s) Fan speed = 455 rpm

Figure 7.le



Figure 7.2 Phase angle between wave induced pressure and water surface elevation as a function of U_{∞}/C .



Figure 7.3 Wave induced pressure as a function of the potential flow solution.
















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Figure 8.2 Shear velocity u_{\star} as a function of U_{∞} for various frequencies of mechanically generated waves.



Figure 8.3 Comparison of u values from this study with data from following wind studies.



Fan speed = 150 rpm



t(s)

Fan speed = 100 rpm

Figure 8.4a



Fan speed = 250 rpm



t(s)

Fan speed = 200 rpm

Figure 8.4b



Fan speed = 250 rpm



t(s)



Figure 8.4b



Fan speed = 350 rpm



t(s)

Fan speed = 300 rpm

Figure 8.4c



Fan speed = 450 rpm



t(s)

Fan speed = 400 rpm

Figure 8.4d

2

2

1



3

3

5

5



t(s)





Fan speed = 500 rpm

1.8

1.8 -1.9 8.9

9

Ø

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0

w(ms⁻¹

u(ms⁻¹) 9. 9

(աա)և





Fan speed = 600 rpm

Figure 8.4f



Figure 8.5 Phase angle between \tilde{u} and η in a stationary coordinate system as a function of U_{∞}/C .



Figure 8.6 Phase angle between \tilde{w} and η in a stationary coordinate system as a function of U_{∞}/C .



Figure 8.7 Wave induced velocity in the x direction in a stationary coordinate system as a function of the potential flow solution.



Figure 8.8 Wave induced velocity in the z direction in a stationary coordinate system as a function of the potential flow solution.





Phase angle between \widetilde{w} and η in a wave following Figure 8.10 coordinate system as a function of U_{m}/C .



Wave induced velocity in the x direction in a wave Figure 8.11 following coordinate system as a function of the potential flow solution.



Figure 8.12

 $10^{1} \text{ amp (} \widetilde{u} \text{) } / \mathrm{U}_{\infty}^{\circ}$

Wave induced velocity in the z direction in a wave following coordinate system as a function of the potential flow solution.







Figure 8.14a

Spectra, phase and coherence results for 1 Hz waves and a fan speed of 100 $\rm rpm_{\circ}$





Spectra, phase and coherence results for 1 Hz waves and a fan speed of 200 $\mbox{rpm}.$



Figure 8.14c

Spectra, phase and coherence results for 1 Hz waves and a fan speed of 300 rpm.



Spectra, phase and coherence results for 1 Hz waves and a fan speed of 400 rpm.



and a fan speed of 500 rpm.





Figure 8.15 The total Reynolds stress u"u" as a function of the wave induced Reynolds stress predicted by potential theory. (stationary coordinate system).





The total Reynolds stress w"w" as a function of the wave induced Reynolds stress predicted by potential coordinate system).



Figure 8.17 The total Reynolds stress u"w" as a function of the wave induced velocity function squared. (stationary coordinate system).



Figure 8.18

The total Reynolds stress u"u" as a function of the wave-induced Reynolds stress predicted by potential theory. (Wave following coordinate system).







Figure 8.20

The total Reynolds stress u"w" as a function of the wave induced velocity function squared. (wave following coordinate system).



Figure 8.21 The total Reynolds stress $\overline{u''w''}$ as a function of U_{∞}^{2} (wave following coordinate system).







Figure 8.22b Spectrum of the product w"w".





Figure 8.22d Spectrum of the momentum flux term u"w" in a following wind. [after Chao and Hsu (21)].



Figure 8.22e Spectrum of the momentum flux term w"w" in a following wind. [after Chao and Hsu (21)].



Figure 8.22f

Spectrum of the momentum flux term u"w" in a following wind. [after Chao and Hsu (21)].



Snyder et al. (117)

This study









-550:



Figure 9.2c Wave decay in an opposing wind as a function of duration.




Wave decay in an opposing wind as a function of duration.





100 rpm

200 rpm



300 rpm

400 rpm



500 rpm

600 rpm

Figure 10.1a The response of f = 0.75 Hz waves to opposing winds.

268.





100 rpm

200 rpm



300 rpm

400 rpm



500 rpm

600 rpm

Figure 10.1b The response of f = 1.00 Hz waves to opposing winds.

269.







100 rpm

200 rpm



300 rpm

400 rpm



500 rpm

600 rpm

Figure 10.1c The response of f = 1.25 Hz waves to opposing winds.



271.

0 rpm



100 rpm

200 rpm



300 rpm

400 rpm



500 rpm

600 rpm



200 rpm



300 rpm



400 rpm



500 rpm

600 rpm

Figure 10.1e

.le The response of f = 1.75 Hz waves to opposing winds.





100 rpm

200 rpm



300 rpm

400 rpm



500 rpm

600 rpm

Figure 10.1f The response of f = 2.00 Hz waves to opposing winds.



Figure A.1 Schematic diagram of the N tube and N volume system analysed by Bergh and Tijdeman (6).



Figure E.2 Applied and measured pressures together with tube transfer functions.







The effect of changing the record length on the spectrum of a narrow band signal.

277.



Figure C.2 Crosscorrelograms for signals with various phase differences.



Figure D.la Folding of the Fourier transform of a finite time series.



Figure D.lb

Folding of real and imaginary parts of the finite discrete Fourier transform.







(b) Result after signal (a) is processed in the forward direction.



(c) Result after signal (b) is processed in the reverse direction.

Figure D.2 Test of computer program for transfer function correction. Signals (a) and (c) are identical indicating correct operation of program.



Figure E.l Schematic diagram of system effects on pressure signal.

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5

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 $\Lambda p_1(w)$ and $[p_D(w) - p_t^{(w)}]$

0,0 B.Ø ω 0 \odot 5 Ď

Initial differential pressure records and regenerated records indicating that TUBTRN.FOR is performing correctly. $\Delta p_2(w)$ and $[p_D(w) - p_s]$

E E

0

0

α

Figure F.l

281.



Figure G.1 Schematic diagram of system effects on velocity measurements.



filters.





Transfer function for low pass filter with cut-off frequency of 10 Hz and 50 filter weights.

287.

φ

filter weights.

Transfer function for band reject filter with cut-off frequencies at 7.5 Hz and 17.5 Hz and 200 filter weights.