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References

- Adshead, N.D., 1995. Geology, Alteration and Geochemistry of the Osborne Cu-Au deposit, Cloncurry District, NW Queensland. Unpublished Ph.D. thesis, James Cook University, Townsville.
- Adshead-Bell, N.S., 1998. Evolution of the Starra and Selwyn High-Strain Zones, Eastern Fold Belt, Mount Isa Inlier: Implications for Au-Cu Mineralization. *Economic Geology*, 93, 1450-1462.
- Akande, S.O., Horn, E.E., Reutel, C., 1988. Mineralogy, fluid inclusion and genesis of the Arafu and Akwana Pb-Zn-F mineralization, middle Benue Trough, Nigeria. *J. Afr. Earth Science*, 7, 167-180.
- Akima, H., 1978. A Method of bivariate interpolation and smooth surface fitting for irregularly distributed data points. *ACM Trans. Math. Software*, 4, 56-76.
- Andrews, S. J., 1998. Stratigraphy and depositional setting of the upper McNamara Group, Lawn Hill Region, Northwest Queensland. *Economic Geology*, 93, 1132-1152.
- Barnhill, R.E., 1985. Surfaces in Computer-Aided geometric design: a survey with new results. *Computer-Aided Geometric Design*, 2, 1-17.
- Bear, J., 1972. *Dynamics of Fluids in Porous Media*. American Elsevier, New York.
- Beardmore, T.J., Newberry, S.P., Laing, W.P., 1988. The Maronan Supergroup: an inferred early volcanosedimentary rift sequence in the Mount Isa Inlier and its implications for ensalicy rifting in the Middle Proterozoic of northwest Queensland. *Precambrian Research*, 40, 487-507.
- Bell, T.H., 1983. Thrusting and Duplex Formation at Mount Isa, Queensland, Australia. *Nature*, 304, 493-497.
- Bell, T.H., Perkins, W.G., Swager, C.P., 1988. Structural controls on the development and localization of syntectonic copper mineralisation at Mount Isa, Queensland. *Economic Geology*, 83, 69-85.
- Bell, TH. & Hickey, K.A., 1998. Multiple Deformations with Successive Subvertical and Subhorizontal Axial Planes in the Mount Isa Region: Their Impact on Geometric Development and Significance for Mineralization and Exploration. *Economic Geology*, 93, 1269-1289.

- Bethke, C.M., 1985. A numerical model of compaction-driven groundwater flow and heat transfer and its Application to the paleohydrology of intracratonic sedimentary basins. *Journal of Geophysical Research*, 90b, 6817-6828.
- Betts, P.G., 2001. Three-dimensional structure along the inverted Palaeoproterozoic Fiery Creek Fault system, Mt Isa terrane, Australia. *Journal of Structural Geology*, 23, 1953–1969.
- Betts, P. G., Lister, G. S., O’Dea, M. G., 1998. Asymmetric extension of the Middle Proterozoic lithosphere, Mount Isa Inlier, Queensland, Australia. *Tectonophysics*, 296, 293–316.
- Betts, P. G., Lister, G. S., Pound, K. S., 1999. Architecture of a Palaeoproterozoic rift system: evidence from the Fiery Creek Dome region, Mt Isa Terrane. *Australian Journal of Earth Sciences*, 46, 533–554.
- Betts, P.G., Lister, G.S. 2002. Geodynamically indicated targeting strategy for shale-hosted massive sulfide Pb-Zn-Ag mineralisation in the Western Fold Belt, Mt Isa terrane. *Australian Journal of Earth Sciences*, 49, 985–1010.
- Betts, P.G., Giles, D., Lister, G.S., 2003. Tectonic Environment of Shale-Hosted Massive Sulfide Pb-Zn-Ag Deposits of Proterozoic Northeastern Australia. *Economic Geology*, 98, 557-576.
- Betts, P.G., Giles, D., Lister, G.S., 2004. Areomagnetic patterns of half-graben and basin inversion: implication for sediment-hosted massive sulfide Pb-Zn Ag exploration. *Journal of Structural Geology*, 26, 1137-1156.
- Beaudoin, G., Taylor, B. E., Sangster, D. F., 1992. Silver-lead-zinc veins and crustal hydrology during Eocene extension, southeastern British Columbia, Canada: *Geochim. Cosmochim. Acta*, 56, 3513-3529.
- Bézier, P., 1974. Mathematical and practical possibilities of UNISURF. *Computer-Aided Geometric Design*, Barnhill, R.E., Riesenfeld, R.F. (Eds.), Academic Press, New York, 127-152.
- Bjørlykke, A., Sangster, D. F., Fehn, U., 1991. Relationships between high heat producing (HHP) granites and stratabound lead-zinc deposits. Source, Transport and Deposition of metals. Pagel, M and Lery, J L. Rotterdam, Balkeema. *Proceedings of the 25 Yr SGA Anniversary Meeting, Nancy, France: 257-260.*
- Blake, D.H., 1987. Geology of the Mt. Isa Inlier and environs. Queensland and Northern Territory. *Bureau of Mineral Resources Bulletin*, 225.

- Blake, D.H., Etheridge, M.A., Page, R.W., Stewart, A.J., Williams, P.R., Wyborn, L.A.I., 1990. Mount Isa Inlier – Regional Geology and Mineralization. *Australasian Institute of Mining & Metallurgy*, 14, 915-925.
- Blake, D.H., Stewart, A.J., 1992. Stratigraphic and Tectonic Framework, Mount Isa Inlier. In: Stewart, A.J. & Blake, D.H. (Eds.) *Detailed Studies of the Mount Isa Inlier*. AGSO Bulletin, 243, 1-11.
- Brace, W. F., 1968. The mechanical effects of pore pressure on the fracturing of rocks. *Research in Tectonics*. Baer, A J, and Norris, D.K., Geological Survey of Canada. Paper 68-52, 113-124.
- Bradley, D.C., Leach, D.L., 2003. Tectonic controls of Mississippi Valley-type lead–zinc mineralization in orogenic forelands. *Mineralium Deposita*, 38, 6, 652 – 667.
- Bredehoeft, J.D., Hanshaw, B.B., 1968. On the maintenance of anomalous fluid pressures: I, Thick sedimentary sequences. *Geological Society of America Bulletin* 79, 1097-1106.
- Briggs, I.C., 1974. Machine contouring using minimal curvature. *Geophysics*, 39, 1, 39-48.
- Broadbent G. C., Myers R. E., Wright J. V., 1998. Geology and origin of shale hosted Zn–Pb–Ag mineralization at the Century deposit, Northwest Queensland, Australia. *Economic Geology* 93, 1264–1294.
- Broadbent, G. C., 1999. Geology and origin of shale-hosted Zn–Pb–Ag mineralization at the Century deposit, northwest Queensland, Australia. Unpublished PhD thesis, James Cook University, Townsville.
- Britto, A.M., Gunn, M.J., 1987. *Critical State Soil Mechanics via Finite Elements*. Ellis Horwood Lmtd., Chichester.
- Brown, M.C., Oliver, N.H.S., Dickens, G.R., 2004. Veins and hydrothermal fluid flow in the Mt. Whaleback Iron Ore District, eastern Hamersley Province, Western Australia. *Precambrian Research*, 128, 441-474.
- Buck, W. R. and Lavier, L. L., 2003, A numerical model of lithospheric extension producing fault-bounded basins and ranges: *Int. Geol. Rev.*, 45, 712-723.

- Butera, K., 2004. The role of mafic rocks in the genesis of IOCG and Base Metal deposits, Mount Isa Eastern Succession, NW Queensland, Australia. In: Barnicoat, A.C., Korsch, R.J. (Eds.) Extended abstracts of the Predictive Mineral Discovery Co-operative Research Centre Conference 2004, Barossa Valley.
- Carr, G.R., 1996. Recent developments in the use of Pb-isotope models in Proterozoic terranes. Abstract: Economic Geology Research Contribution, James Cook University, North Queensland, 55, 33-35.
- Carter, E.K., Brooks, J.H., Walker, K.R., 1961. The Precambrian mineral belt of north-western Queensland. Bulletin, Bureau Mineral Resources, Australia, 51.
- Chapman, L.H., 2004. Geology and Mineralization Styles of the George Fisher Zn-Pb-Ag Deposit, Mount Isa, Australia. *Economic Geology*, 99, 233-255.
- Chauvet, A., Piantone, P., Barbanson, L., Nehlig, P., Pedroletti, I., 2001, Gold deposit formation during collapse tectonics: structural, mineralogical, geochronological and fluid inclusion constraints in the Ouro Preto gold mines, Quadrilátero Ferrífero, Brazil: *Economic Geology*, 96, 25-48.
- Chen, W.F., 1982. *Plasticity in Reinforced Concrete*. McGraw-Hill, New York.
- Clifford, M., Kelso, I., 2002. Pasminco ore grade control and mineral resources: internal report.
- Connolly, J. A. D., 1997. Devolatilization-generated fluid pressure and deformation-propagated fluid flow during prograde regional metamorphism: *J. Geophys. Res.*, 102, 18149-18173.
- Connors, K. A., Page, R. W., 1995. Relations between magmatism, metamorphism and deformation in the western Mt Isa Inlier, Australia. *Precambrian Research*, 71, 131–153.
- Connors, K.A., Lister, G.S., 1995. Polyphase deformation in the western Mount Isa Inlier, Australia: episodic or continuous deformation? *Journal of Structural Geology*, 17, 3, 305-328.
- Cooke, D.R., Bull, S., Large, R.R., 2003. Processes of ore formation in the stratiform sediment-hosted Zn–Pb deposits of Northern Australia: testing the Century model. *Journal of Geochemical Exploration*, 78-79, 519-524.
- Cox, S.F., 1995. Faulting processes at high fluid pressures: An example of fault-valve behaviour from the Wattle Gully Fault, Victoria, Australia. *Journal of Geophysical Research* 100, 12841-12860.

- Cox, S.F., 1999. Deformation controls on the dynamics of fluid flow in mesothermal gold systems. In: McCaffery, K.J.W., Lonergan, L., Wilkinson, J.J. (Eds.), *Fractures, Fluid Flow and Mineralization Geological Society Special Publication 155*, 123-140.
- Crawford, A. J., Corbett, K. D., Everard, J., 1992. Geochemical and tectonic setting of a Cambrian VHMS-rich volcanic belt: the Mount Read Volcanics, western Tasmania: *Economic Geology*, 87, 597-619.
- Cundall, P. Board, M., 1988. A microcomputer program for modelling large-strain plasticity problems. In: Swoboda, C. (Ed.), *Numerical Methods in Geomechanics. Proceedings of the 16th International Conference on Numerical Methods in Geomechanics*, 2101-2108.
- Dadet, P., Marchesseau, J., Millon, R., Motti, E., 1970. Mineral occurrences related to stratigraphy and tectonics in Tertiary sediments near Umm Lajj, eastern Red Sea, Saudi Arabia, *Philos Trans. R. Soc. London Series A*, 267, 99-106.
- Darcy, H., 1856. *Les fontaines publiques de la ville de Dijon*. Dalmont, Paris.
- Davis, B.K., Pollard, P.J., Lally, J.H., McNaughton, J., Blake, K., Williams, P.J., 2001. Deformation history of the Naraku Batholith, Mt Isa Inlier, Australia: implications for pluton ages and geometries from structural study of the Dipvale Granodiorite and Levian Granite. *Australian Journal of Earth Sciences*, 48, 113-129.
- Davis, T.P., 2004. Mine-Scale Structural Controls on the Mount Isa Zn-Pb-Cu Ore Bodies. *Economic Geology*, 99, 543-559.
- de Boor, C., 1972. On calculating with B-splines. *Journal of Approximation Theory*, 6, 50-62.
- de Boorder, H., Spakman, W., White, S. H., Wortel, M. J. R., 1998. Late Cenozoic mineralization, orogenic collapse and slab detachment in the European Alpine Belt: *Eth. Plan. Sci. Lett.*, 164, 569-575.
- de Jong, G., Williams, P.J., 1995. Giant Metasomatic System formed during Exhumation of Mid Crustal Proterozoic rocks in the vicinity of the Cloncurry fault, NW Queensland. *Australian Journal of Earth Sciences*, 42, 281-290.
- de Kemp, E.A., 2000. 3-D visualization of structural field data: examples from the Archean Caopatina Formation, Abitibi greenstone belt, Quebec, Canada *Computers & Geosciences*, 26, 5, 509-530.

- Degens, E.T., Ross, D.A., 1969. Hot brines and recent heavy metal deposits in the Red Sea: a geophysical and geochemical account. Springer, New York.
- Dixon, P. R., Rye, D. M., Janecky, D. R., 1991. Fluid flow connections to basement rocks below sedimentary basins: evidence from the base metal deposits in Ireland: *Geophys. Res. Lett.*, 18, 943-946.
- Derrick, G. M., 1982. A Proterozoic rift zone at Mount Isa, Queensland, and implications for mineralisation. *BMR Journal of Australian Geology and Geophysics* 7, 81–92.
- Dipple, G.M., Ferry, J.M., 1992. Metasomatism and fluid flow in ductile fault zones. *Contributions to Mineralogy and Petrology* 112, 2-3, 149-164.
- Dixon, P. R., Rye, D. M., Janecky, D. R., 1991. Fluid flow connections to basement rocks below sedimentary basins: evidence from the base metal deposits in Ireland. *Geophys. Res. Lett.*, 18, 943-946.
- Domenico, P.A., Schwartz, F.W., 1997. *Physical and Chemical Hydrogeology*. 2nd edition, John Wiley & Sons, New York.
- Drummond, B.J., Goleby, B.R., Goncharov, A.G., Wyborn, L.A.I., Collins, C.D.N., MaCready, T., 1998. Crustal-scale structures in the Proterozoic Mount Isa Inlier of north Australia: their seismic response and influence on mineralisation. *Tectonophysics*, 288, 43-56.
- Duanne, M.J., de Wit, M.J., 1988. Pb-Zn ore deposits of the northern Caledonides – products of continental scale fluid mixing and tectonic expulsion during continental collision. *Geology*, 16, 999-1002.
- Dullien, F.A.L., 1979. *Porous Media Fluid Transport and Pore Structure*. Academic Press Inc., New York.
- Edmond, J.M., Paterson, M.S., 1972. Volume Changes During the Deformation of Rocks at High Pressures. *Int. J. Rock. Mech. Min. Sci.* 9, 161-182.
- El Arif, M.M., 1984. Strat-bound and stratiform iron sulfides, sulfur and galena in the Miocene evaporates, Ranga, Red Sea, Egypt (with special emphasis on their diagenetic crystallization rhythmities). In: Wauschkuhn, A., Kluth, C., Zimmermann, R.A. (Eds.) *Syngeneses and epigenesis in the formation of mineral deposits*. Springer, New York, 457-467.

- England, P. C., Houseman, G. A., 1988. The mechanics of the Tibetan Plateau: *Phil. Trans. R. Soc. Lond.*, A326, 301-320.
- Etheridge, M.A., Wall, V.J., Cox, S.F., 1984. High fluid pressure during regional metamorphism and Deformation: implications for mass transport and deformation mechanisms. *Journal of Geophysical Research*, 89, 4344-4358.
- Etheridge, M.A., Wall, V.J., Vernon, R.H., 1983. The role of the fluid phase during regional metamorphism and Deformation. *Journal of Metamorphic Geology*, 1, 205-226.
- Etheridge, M.A., Rutland, R.W.D., Wyborn, L.A.I., 1987. Orogenesis and Tectonic Process in the Early to Middle Proterozoic of Northern Australia. American Geophysical Union, *Geodynamic Series* 17, 131-147.
- Everett, C. E., Rye, D. M., Ellam, R. M., 2003. Source or sink? An assessment of the role of the Old Red Sandstone in the genesis of the Irish Zn-Pb deposits: *Economic Geology*, 98, 31-50.
- Farin, G., 1988. *Curves and surfaces for Computer-Aided geometric design, A Practical Guide*. Academic Press, San Diego, pp. 334.
- Farrington, J.L., 1952. A preliminary description of the Nigerian lead-zinc field. *Economic Geology*, 47, 583-608.
- Feltrin, L., Oliver, N.H.S., Kelso, I.J., King, S., 2003. Basement metal scavenging during basin evolution: Cambrian and Proterozoic interaction at the Century Zn-Pb-Ag Deposit, Northern Australia, *Journal of Geochemical Exploration*, 78-79, 159-162.
- Ferry, J. M., Dipple, G. M., 1991. Fluid flow, mineral reactions, and metasomatism. *Geology*, 19, 211-214.
- Foster, D.R.W., 2003. Proterozoic low-pressure metamorphism in the Mount Isa Inlier, northwest Queensland, Australia, with particular emphasis on the use of calcic amphibole chemistry as temperature-pressure indicators. Unpublished PhD thesis, James Cook University, Australia.
- Franklin, J.A., Dusseault, M.B., 1989. *Rock Engineering*. McGraw-Hill, USA.
- Freeze, R.A., Witherspoon, P.A., 1966. Theoretical Analysis of Regional Groundwater Flow: 1. Analytical and Numerical Solutions to the Mathematical Model. *Water Resources Research* 2, 4, 641-656.

- Freeze, R.A., Cherry, J.A., 1979. *Groundwater*. Prentice Hall, N.J.
- French, T., 1997. Genesis of albitites and anthophyllite bearing lithologies of the Osborne Cu-Au deposit, Cloncurry District, Mt. Isa Inlier, N.W. Queensland. Unpublished Hons. thesis. James Cook University.
- Ge, S., Garven, G., 1992. Hydromechanical modelling of tectonically driven groundwater flow with application to the Arkoma foreland basin. *Journal of Geophysical Research*, 97, 9119-9144.
- Garven, G., 1985. The Role of Regional Fluid Flow in the Genesis of the Pine Point Deposit, Western Canada Sedimentary Basin. *Economic Geology*, 80, 307-324.
- Garven, G., Raffensperger, J.P., 1997. Hydrogeology and geochemistry of ore genesis in sedimentary basins. In: Barnes, H.L. (Ed.), *Geochemistry of hydrothermal ore deposits*, 125-189.
- Garven, G., Freeze, R.A., 1984a. Theoretical analysis of the role of groundwater flow in the genesis of stratabound ore deposits. 1. Mathematical and numerical model. *American Journal of Science*, 284, 1085-1124.
- Garven, G., Freeze, R.A., 1984b. Theoretical analysis of the role of groundwater flow in the genesis of stratabound ore deposits. 1. Quantitative results. *American Journal of Science*, 284, 1125-1174.
- Garven, G., Bull, S.W., Large, R.R., 2001. Hydrothermal fluid flow models of stratiform ore genesis in the McArthur Basin, Northern Territory, Australia. *Geofluids*, 1, 4, 289-313.
- Giles, D., Nutman, A.P., 2002. SHRIMP U-Pb monazite dating of 1600–1580 Ma amphibolite facies metamorphism in the southeastern Mt Isa Block, Australia *Australian Journal of Earth Sciences*, 49, 455-465.
- Giles, D., Nutman, A.P., 2003. SHRIMP U-Pb zircon dating of the host rocks of the Cannington Ag-Pb-Zn deposit, southeastern Mt Isa Block, Australia. *Australian Journal of Earth Sciences*, 50, 295-309.
- Goodfellow, W.D., 1993. Geology and genesis of stratiform sediment-hosted (SEDEX) zinc-lead-silver sulphide deposits. In: Kirkham, R. V., Sinclair, W. D., Thorpe, R. I., Duke, J. M. (Eds.) *Mineral deposit modeling*. Special Paper-Geological Association of Canada, 40, 201-251.

- Gow, P.A., Upton, P., Zhao, C., Hill, K.C., 2002. Copper-gold mineralisation in New Guinea: numerical modelling of collision, fluid flow and intrusion-related hydrothermal systems. *Australian Journal of Earth Sciences* 49, 753-771.
- Grant, N.K., 1971. South Atlantic, Benue trough, and the Gulf of Guinea Cretaceous triple junction. *Bulletin Geol. Society America*, 82, 2295-2298.
- Greenkorn, R.A., 1983. *Flow Phenomenon in Porous Media. Fundamentals and Applications in Petroleum, Water and Food Production.* Marcel Dekker Inc., New York.
- Hackett, J.P., Bischoff, J.L., 1973. New data on the stratigraphy, extent and geological history of the Red Sea geothermal deposits. *Economic Geology*, 68, 533-564.
- Hagemann, S.G., Barley, M.E., Folkert, S.L., Yardley, B.W., Banks, D.A., 1999. A hydrothermal origin for the giant Tom Price iron ore deposit, In: Stanley et al. (Eds.), *Mineral Deposits: Processes to Processing*, 41-44.
- Hand, M., Rubatto, D., 2002. The Scale of the Thermal Problem in the Mt Isa Inlier. In: Preiss, V.P. (Ed.), *Geoscience 2002: Expanding Horizons. Abstracts of the 16th Australian Geological Convention, Adelaide, July 2002*, 67, pp.173.
- Handin, J., Hager, R.V. Jr., Fiedman, M. & Feather, J.N., 1963. Experimental Deformation of Sedimentary Rocks Under Confining Pressure: Pore Pressure Tests. *Bull. Am. Assc. Petrol. Geol.* 47, 717-755.
- Harmsworth, R.A., Kneeshaw, M., Morris, R.C., Robinson, C.J., Shrivastava, P.K., 1990. BIF-derived iron ores of the Hamersley Province. In: Hughes, F.E. (Ed.), *Geology of the Mineral Deposits of Australia and Papua New Guinea*, Australasian Institute of Mining and Metallurgy Monograph 14, 617-642.
- Hein, K. A. A., 2002. Geology of the Ranger uranium mine, Northern Territory, Australia; structural constraints on the timing of uranium emplacement: *Ore Geology Reviews*, 20, 83-108.
- Heinrich, C. A., Walshe, J. L., Harrold, B. P., 1996. Chemical mass transfer of ore-forming hydrothermal systems: current practice and problems: *Ore Geology Reviews*, 10, 319-338.
- Hill, E.J., Loosveld, R.J.H., Oliver, N.H.S., 1992. Structure and geochronology of the Tommy Creek Block, Mount Isa Inlier. In: Stewart, A.J. & Blake, D.H. (Eds.) *Detailed Studies of the Mount Isa Inlier.* AGSO Bulletin, 243.

- Hobbs, B.E., Means, W. D., Williams, P.F., 1976. *An Outline of Structural Geology*. John Wiley & Sons, New York, NY.
- Hobbs, B.E., Muhlhaus, H.B., Ord, A., 1990. Instability, softening and localization of deformation. In: Knipe, R.J., Rutter, E.H. (Eds.), *Deformation Mechanisms, Rheology and Tectonics*. Geological Society Special Publication, 143-165.
- Holcome, R.J., Pearson, P.J., Oliver, N.H.S., 1992. Structure of the Mary Kathleen Fold Belt. In: Sinclair, A.J., Blake, D.H. (Eds.), *Detailed studies of the Mt Isa Inlier*, Australian Geological Survey Organisation Bulletin, Canberra, 243, 257-287.
- Holcombe, R.J., Pearson, P.J. & Oliver, N.H.S., 1991. Geometry of a Middle Proterozoic Extensional Decollement in North-Eastern Australia. *Tectonophysics*, 191, 255-274.
- Holyland, P.W., Ridley, J.R., Vernacombe, J.R., 1993. Stress Mapping Technology (SMT). In: Parnell, J., Ruffel, A.H., Moles, N.R. (Eds), *Geofluids '93: Contributions to an International Conference on Fluid Evolution, Migration and Interaction in Rocks*, Geological Society of London, pp. 272-275.
- Holyland, P.W., Ojala, V.J., 1997. Computer-aided structural targeting in mineral exploration: two- and three-dimensional stress mapping. *Australian Journal of Earth Sciences*, 44, 421-432.
- Houlding, S.W., 1994. *3D Geoscience Modeling, Computer techniques for geological characterization*. Springer-Verlag, New York, pp. 304.
- Hubbert, M.K., 1940. The Theory of Ground-Water Motion, Part 1. *The Journal of Geology*, 48, 8, 785-944.
- Hubbert, M.K., Ruby, W.W., 1959. Role of fluid pressure in mechanics of overthrust faulting. Part 1: Mechanics of fluid filled porous solids and its application to overthrust faulting. *Bull. Geol. Soc. Am.*, 70, 115-166.
- Idnurm, M., 2000. Towards a high resolution Late Palaeoproterozoic-earliest Mesoproterozoic apparent polar wander path for northern Australia. *Australian Journal of Earth Sciences*, 47, 405-429.
- Ireland, T., Bull, S.W., large, R.R., 2003. Mass flow sedimentology within the HYC Zn–Pb–Ag deposit, Northern Territory, Australia: evidence for syn-sedimentary ore genesis. *Mineralium Deposita*, 39, 2, 143 – 158.

- Itasca, 2000a. FLAC, Fast Lagrangian Analysis of Continua, 2nd Edition, Itasca Consulting Group Inc. Minnesota, USA.
- Itasca, 2000b. UDEC, Universal Distinct Element Code, Itasca Consulting Group Inc. Minnesota, USA.
- Jackson, M.J., Scott, D.L., Rawlings, D.J., 2000. Stratigraphic framework for the Leichhardt and Calvert Superbasins: review and correlations of the pre-1700 Ma successions between Mt Isa and McArthur River. *Australian Journal of Earth Sciences* 47, 381–404.
- Jaeger, J.C, 1969. *Elasticity, Fracture and Flow*. 3rd Edition, Chapman and Hall, London.
- Jaeger, J.C, Cook, N.G.W., 1976. *Fundamentals of Rock Mechanics*. 2nd Edition, Chapman and Hall, London.
- Jiang, Z., Oliver, N.H.S., Barr, T., Power, W.L., Ord, A., 1997. Numerical Modelling of Fault-Controlled Fluid Flow in the Genesis of Tin Deposits of the Malage Ore Field, Gejiu Mining District, China. *Economic Geology*, 92, 228-247.
- Johnston, J. D., 1999. Regional fluid flow and the genesis of Irish Carboniferous base metal deposits: *Mineralium Deposita*, 34, 571-598.
- Kendrick, M.A., Burgess, R., Patrick, R.A.D., Turner, G., 2002a. Hydrothermal Fluid Origins in a Fluorite-Rich Mississippi Valley-Type District: Combined Noble Gas (He, Ar, Kr) and Halogen (Cl, Br, I) Analysis of Fluid Inclusions from the South Pennine Ore Field, United Kingdom. *Economic Geology*, 97, 435-453.
- Kendrick, M.A., Burgess, R., Leach, D. Patrick, R.A.D., 2002b. Hydrothermal Fluid Origins in Mississippi Valley-Type Ore Districts: Combined Noble Gas (He, Ar, Kr) and Halogen (Cl, Br, I) Analysis of Fluid Inclusions from the Illinois-Kentucky Fluorspar District, Viburnum Trend, and tri-State Districts, Midcontinent, United States. *Economic Geology*, 97, 453-471.
- Kissen, I.G., 1978. The principal distinctive features of the hydrodynamic regime of intensive earth crust downwarping areas. In: Ronai, A., Remi, M. (Eds.) *Hydrogeology of great Sedimentary Basins: Publication of the International Association of Hydrological Sciences*, pp.178-185.
- Konikow, L.F., Bredehoeft, J.D., 1992. Groundwater models cannot be validated. *Advances in Water Resources*, 15, 75-83.

- Koons, P.O., Craw, D., Cox, S.C., Upton, P., Templeton, A.S., Chamberlain, C.P., 1998. Fluid flow during active oblique convergence: A Southern Alps model from mechanical and geochemical observations. *Geology*, 26, 159-162.
- Krassay, A.A., Bradshaw, B.E., Domagala, J., Jackson, M.J., 2000a. Siliclastic shoreline to growth-faulted, turbiditic sub-basins: the Proterozoic River Supersequence of the upper McNamara Group on the Lawn Hill Platform, northern Australia. *Australian Journal of Earth Sciences*, 47, 533-562.
- Krassay, A.A., Domagala, J., Bradshaw, B.E., Southgate, P.N., 2000b. Lowstand ramps, fans and deep-water Paleoproterozoic and Mesoproterozoic facies of the Lawn Hill Platform: the Term, Lawn, Wide and Doom Supersequences of the Isa Superbasin, northern Australia. *Australian Journal of Earth Sciences*, 47, 563-597.
- Kuznir, N.J., Park, R.G., 1987. The extensional strength of the continental lithosphere: its dependence on geothermal gradient, and crustal composition and thickness. In: Dewey, J.F., Hancock, P.L. (Eds.) *Continental Extensional Tectonics*, Geological Society Special Publication, 28, 35-52.
- Laing, W.P., 1993. Structural/metasomatic controls on ore deposits in the east Mount Isa Block: the key to tonnes and grade. *Australian Institute of Geoscientists, Bulletin*, 13, 17-24.
- Laing, W.P., 1998. Structural-metasomatic Environment of the East Mt. Isa Block base metal-gold Province. *Australian Journal of Earth Sciences*, 45, 413-428.
- Large, D.E., 1980. Geological parameters associated with sediment-hosted, submarine exhalative Pb-Zn deposits: an empirical model for mineral exploration. *Geologisches Jahrbuch*, 40, 59-129.
- Li, Z.X., Powell, C. McA., Bowman, R., 1993. Timing and genesis of Hamersley iron-ore deposits. *Exploration Geophysics*, 24, 631-636.
- Lister, G. S., Davis, G. A., 1989. The origin of metamorphic core complexes and detachment faults formed during Tertiary continental extension in the northern Colorado River region, U.S.A. *Journal of Structural Geology*, 11, 65-94.
- Lynch, H.D., Morgan, P., 1987. The tensile strength of the lithosphere and the localization of extension. In: Dewey, J.F., Hancock, P.L. (Eds.) *Continental Extensional Tectonics*, Geological Society Special Publication, 28, 53-65.

- Macready, T., Goleby, B.R., Goncharov, A., Drummond, B.J. & Lister, G.S., 1998. A framework of overprinting orogens based on interpretation of the Mount Isa deep seismic transect. *Economic Geology*, 93, 1422-1434.
- Mair, J.L., Ojala, V.J., Salier, B.P., Groves, D.I., Brown, S.M., 2000. Application of stress mapping in cross-section to understanding ore geometry, predicting ore zones and development of drilling strategies. *Australian Journal of Earth Sciences*, 47, 895-912.
- Mallet, J.L., 2002. *Geomodeling*. Oxford University Press, New York, pp. 599.
- Malavieille, J., Taboada, A., 1991. Kinematic model for postorogenic Basin and range extension: *Geology*, 19, 555-558.
- Mares, V.M., 1998. Structure, Eastern Fold Belt, Mount Isa Inlier. *Australian Journal of Earth Sciences*, 45, 3, 373-387.
- Mark, G., 1999. Petrogenesis of Mesoproterozoic K-rich granitoids, southern Mount Angelay igneous complex, Cloncurry district, northwest Queensland. *Australian Journal of Earth Sciences*, 46, 933-949.
- Mark, G., 2001. Nd isotope and petrogenetic constraints for the origin of the Mount Angelay igneous complex: implications for the origin of intrusions in the Cloncurry district, NE Australia. *Precambrian Research*, 105, 17-35
- Mark, G., Williams, P.J., Ryan, C., Mernagh, T., 2001. Fluid chemistry and ore-forming processes at the Ernest Henry Fe oxide-copper-gold deposit, NW Queensland. In: Williams, P.J. (Ed) *A Hydrothermal Odyssey, Extended Conference Abstracts*, JCU, Economic geology Research Unit Contribution 59, 124-125.
- Martin, D.M., Li, Z.X., Nemchin, A.A., Powell, C.M., 1998. A pre- 2.2 Ga age for giant hematite ores of the Hamersley Province, Australia. *Economic Geology*, 93, 1084-1090.
- McClay, K. R., Ellis, P. G., 1987. Geometries of extension fault systems developed in model experiments: *Geology*, 15, 341-344.
- McLellan, J.G., 2000. *Structural Controls and Numerical Modelling of Mineralisation at the Osborne Cu-Au Deposit, Mount Isa Block, N.W. Queensland*. Hons. Thesis. James Cook University.

- McLellan, J.G., Oliver, N.H.S., Schaub, P.M., 2004. Fluid Flow in Extensional Environments; Numerical Modelling with an Application to Hamersley Iron Ores. *Journal of Structural Geology*, 26,6-7, 1157-1171.
- Mises, R.Von., 1913. *Mechanik der festen Körper im plastisch deformablen Zustand*. Nachr. Ges. Wiss. Göttingen, Mathematisch-physikalische Klasse, 582-592.
- Möller, P., Weise, S. M., and others, 1997. Paleofluids and recent fluids in the upper continental crust: results from the German continental deep drilling program (KTB). *J. Geophys. Res.*, 102, 18233-18254.
- Moore, J. C., Shipley, T. H., Goldberg, D., and many others, 1995, Abnormal fluid pressures and fault-zone dilation in the Barbados accretionary prism: evidence from logging while drilling. *Geology*, 23, 605-608.
- Morris, R.C., 1980. A textural and mineralogical study of the relationship of iron ore to banded iron formation in the Hamersley Iron Province of Western Australia. *Economic Geology* 75, 185-209.
- Morris, R.C., 1985. Genesis of iron ore in banded iron-formation by supergene and supergene-metamorphic processes – A conceptual model. In: Wolff, K.H. (Ed.) *Handbook of Strata-bound and Stratiform Ore deposits*, 13, 73-235.
- Morrison, J., 1994, Meteoric water-rock interaction in the lower plate of the Whipple Mountain metamorphic core complex, California: *J. Metamorphic Geology*, 12, 827-840.
- Mustard, R., Blenkinsop, T., McKeagney, C., Huddleston-Holmes, C., Partington, G., 2004. New perspectives on IOCG deposits, Mt Isa Eastern Succession, northwest Queensland. *Society of Economic Geologists 2004: Predictive Mineral Discovery Under Cover. Extended Abstracts Volume*, 281-284.
- Nesbitt, B.E., Muehlenbachs, K., 1989. Origins and movement of fluids during deformation and metamorphism in the Canadian Cordillera. *Science*, 245, 733-736.
- Nesbitt, B. E., Mendoza, C. A., Kerrick, D. M., 1995. Surface fluid convection during Cordilleran extension and the generation of metamorphic CO₂ contributions to Cenozoic atmospheres: *Geology*, 23, 99-101.

- Neuzil, C.E., 1995. Abnormal Pressures as Hydrodynamic Phenomena. *American Journal of Science* 295, 742-786.
- Nye, J.F., 1964. *Physical properties of crystals*. Clarendon, Oxford, U.K.
- O'Dea, M.G., Lister, G.S., 1997. The Evolution of the Mount Isa Orogen – from Start to Finish. *Geodynamics & Ore Deposits Conference*, 19-21 Feb 1997.
- O'Dea, M.G., Lister, G.S., Betts, P.G., Pound, K.S., 1997. A shortened intraplate rift system in the Proterozoic Mt Isa terrain, NW Queensland, Australia. *Tectonics* 16, 425-441.
- O'Dea, M.G., Lister, G.S., 1995. The role of ductility contrast and basement architecture in the structural evolution of the Crystal Creek block, Mount Isa Inlier, NW Queensland, Australia. *Journal of Structural Geology*, 17, 7, 949-960.
- O'Dea, M.G., Lister, G.S., MaCready, T., Betts, P.G., Oliver, N.H.S., Pound, K.S., Huang, W., Valenta, R.K., 1997. *Orogeny Through Time*. Geological Society Special Publication. No.121, 99-122.
- Oliver, J., 1986. Fluids expelled tectonically from orogenic belts: Their role in hydrocarbon migration and other geologic phenomena. *Geology*, 14, 99-102.
- Oliver N. H. S., Cartwright I., Rawling T. R., Pearson P. J., 1994. High Temperature Fluid-Rock Interaction and Scapolitization in an Extension-related Hydrothermal System, Mary Kathleen, Australia. *Journal of Petrology*, 35, 1455-1493.
- Oliver, N.H.S., 1995. Hydrothermal history of the Mary Kathleen Fold Belt, Mount Isa Block, Queensland. *Australian Journal of Earth Sciences*, 42, 267-279.
- Oliver, N.H.S., 1996. Review and classification of structural controls on fluid flow during regional metamorphism. *Journal of Metamorphic Geology*, 14, 477-492.
- Oliver, N.H.S., Valenta, R.K., Wall, V.J., 1990. The effect of heterogeneous stress and strain on metamorphic fluid flow, Mary Kathleen, Australia, and a model for large-scale fluid circulation. *Journal of Metamorphic Geology* 8, 311-331.
- Oliver, N.H.S., Dickens, G.R., 1999. Hematite ores of Australia formed by syntectonic heated meteoric fluids. In: Stanley et al., (Eds.) *Mineral Deposits: Processes to Processing*, 889-892.

- Oliver, N.H.S., Pearson, P.J., Holcombe, R.J., Ord, A., 1999. Mary Kathleen Metamorphic-hydrothermal uranium-rare-earth element deposit: Ore genesis and Numerical Model of Coupled Deformation and Fluid Flow. *Australian Journal of Earth Sciences*, 46, 467-484.
- Oliver, N.H.S., Ord, A., Valenta, R.K., Upton, P., 2001a. Deformation, Fluid Flow, and Ore Genesis in Heterogeneous Rocks, with Examples and Numerical Models from the Mount Isa District, Australia. *Society of Economic Geologists, Reviews*, 14, 51-74.
- Oliver, N. H. S., Mark G., Rubenach, M. J., Pollard, P. J., Williams, P. J., Marshall, L. K., 2001b. Intrusion-related albitisation as a chemical precursor to ironstone-Cu-Au mineralisation in the Cloncurry District - geochemical and isotopic evidence. In Mark, G., Oliver, N. H. S. & Foster, D. R. W. (Eds.) *Mineralisation, alteration and magmatism in the Eastern Fold Belt, Mount Isa Block, Australia. Geol. Soc. Austr. Specialist Group in Economic Geology, Spec. Publ.* 5.
- Oliver, N. H. S., Bons, P. D., 2001. Mechanisms of fluid flow and fluid-rock interaction in fossil metamorphic-hydrothermal systems inferred from vein-wallrock patterns, geometry, and microstructure. *Geofluids*, 1, 137-151.
- Ord, A., 1991a. Deformation of Rock: A Pressure-Sensitive, Dilatant Material. *Pure and Applied Geophysics* 137, 4, 337-366.
- Ord, A., 1991b. Fluid flow through patterned shear zones. *Computer Methods and Advances in Geomechanics*. Beer, G., Booker, J. R., Carter, J. P. (Eds). Rotterdam, Balkema, 393-398.
- Ord, A., Oliver, N.H.S., 1997. Mechanical Controls on Fluid Flow during Regional Metamorphism: Some Numerical Models. *Journal Metamorphic Geology*, 15, 345-359.
- Ord A., Hobbs B.E., Zhang Y., Broadbent G.C., Brown, M., Willetts G., Sorjonen-Ward P., Walshe J.L., Zhao C., 2002. Geodynamic modelling of the Century deposit, Mt Isa Province, Queensland. *Australian Journal of Earth Sciences*, 49, 6, 1011-1039.
- Overveld, C.W., 1995. Pondering on discrete smoothing and interpolation. *Computer-Aided Design*, 27, 5, 377-384.
- Oyarzun, R., Rodriguez, M., Pincheira, M., and Others, 1999. The Candelaria (Cu-Fe-Au) and Punta del Cobre (Cu-Fe) deposits (Copiapo, Chile): a case for extension-related granitoid emplacement and mineralization processes? *Mineralium Deposita*, 34, 799-801.
- Page, R.W., Bell, T.H., 1986. Isotopic and structural responses of granite to successive deformation and metamorphism. *Journal of Geology*, 94, 365-379.

- Page, R. W., 1988. Geochronology of early to middle Proterozoic fold belts in northern Australia: a review. *Precambrian Research*, 40-41, 1–19.
- Page, R.W., Sun, S.S., 1998. Aspects of geochronology and crustal evolution in the Eastern Fold Belt, Mt Isa Inlier. *Australian Journal of Earth Sciences*, 45, 343-363.
- Page, R. W., Sweet, I. P., 1998. Geochronology of basin phases in the western Mt Isa Inlier, and correlation with the McArthur Basin. *Australian Journal of Earth Sciences*, 45, 219–232.
- Page R. W., Jackson, M. J., Krassay, A. A., 2000. Constraining sequence stratigraphy in north Australian basins: SHRIMP U–Pb zircon geochronology between Mt Isa and McArthur River. *Australian Journal of Earth Sciences*, 47, 431–459.
- Pearson, P.J., Holcome, R.J., Page, R.W., 1992. Synkinematic emplacement of the Middle Proterozoic Wonga Batholith into a mid-crustal extensional shear zone, Mount Isa Inlier, Queensland, Australia. In: Sinclair, A.J., Blake, D.H. (Eds.), *Detailed studies of the Mt Isa Inlier*, Australian Geological Survey Organisation Bulletin, Canberra, 243.
- Perkins, C., Wyborn, L.A.I., 1998. Age of Cu-Au mineralisation, Cloncurry District, eastern Mt. Isa Inlier, Queensland, as determined by Ar/Ar dating. *Australian Journal of Earth Sciences*, 45, 233-246.
- Perring, C.S., Pollard, P.J., Dong, G., Nunn, A.J., Blake, K.L., 2000. The Lightning Creek Sill Complex, Cloncurry District, Northwest Queensland: A source of fluids for Fe Oxide Cu-Au mineralisation and Sodic-Calcic Alteration. *Economic Geology*, 95, 1067-1089.
- Pfiffner, O.A., Ramsey, J.G., 1982. Constraints on geological strain rates: arguments from finite strain rates of naturally deformed rocks. *Journal of Geophysical Research*, 87, 311-21.
- Pietrantonio, G., Riguzzi, F., 2004. Three-dimensional strain tensor estimation by GPS observations: methodological aspects and geophysical applications. *Journal of Geodynamics*, 38, 1-18.
- Plumb, K. A., Derrick, G. M., 1975. Geology of the Proterozoic rocks of the Kimberley to Mount Isa Region. In: *Economic Geology of Australia and Papua New Guinea*, pp. 217–252. Australian Institute of Mining and Metallurgy Monograph Series 5.
- Plumb, K. A., Derrick, G. M., Wilson, I.H., 1980. Precambrian geology of the McArthur River Mount Isa Region, northern Australia. In: Henderson, R.A., Stephenson, P.J. (Eds.) *The*

Geology and Geophysics of Northeastern Australia. Geological Society of Australia, Queensland Division, 77-88.

Pollard, P.J., Mark, G., Mitchell, L., 1998. Geochemistry of post-1540 Ma granites in the Cloncurry District. *Economic Geology*, 93, 1330-1344.

Pollard, P., 2001. Sodic(-calcic) alteration in Fe-oxide-Cu-Au districts: an origin via unmixing of magmatic H₂O-CO₂-NaCl+- CaCl₂-KCl fluids. *Mineralium Deposita*, 36, 93-100.

Powell, C. McA., Oliver, N.H.S., Li, Z.X., Martin, D. McB., Ronaszeki, J., 1999. Synorogenic hydrothermal Origin for giant Hamersley iron oxide. *Geology* 27, 175-178.

Powell, C. McA., Li, Z.X., Martin, D. McB., 1998. Tectonic evolution of the Paleoproterozoic Ophthalmia fold and thrust belt: 14th Australian Geological Convention [abs.], Geological Society of Australia, p. 361.

QDNRME, 2000. Queensland Department of Natural Resources Mines and Energy. North West Queensland Mineral Province Report, Queensland Government.

Reynolds, S. J., Lister, G. S., 1987. Structural aspects of fluid-rock interactions in detachment zones: *Geology*, 15, 362-366

Romm, E.S., 1966. Flow characteristics of fractured rocks. Nedra, Moscow.

Rotherham, J.F., Blake, K.L., Cartwright, I., Williams, P.J., 1998. Stable Isotope Evidence for the origin of the Mesoproterozoic Starra Au-Cu Deposit, Cloncurry District, Northwest Queensland. *Economic Geology*, 93, 1435-1449.

Rubenach, M.J., 1992. Proterozoic low-pressure high-temperature Metamorphism and Anticlockwise P-T-t path for the Hazeldene area, Mount Isa Inlier, Queensland, Australia. *Journal of Metamorphic Geology*, 10, 333-346.

Rubenach, M.J., Barker, A.J., 1998. Metamorphic and Metasomatic Evolution of the Snake Creek Anticline, Eastern Succession, Mt Isa Inlier. *Australian Journal of Earth Sciences*, 45, 363-372.

Rubenach, M., Adshead, N., Oliver, N.H.S., Tullemans, F., Esser, D., Stein, H., 2001. The Osborne Cu-Au Deposit: Geochronology, and Genesis of Mineralisation in Relation to Host Albitites and Ironstones. In: Williams, P.J. (Ed) A Hydrothermal Odyssey, Extended Conference Abstracts, JCU, Economic geology Research Unit Contribution 59, 172-173.

- Rubenach, M.J., Lewthwaite, K.A., 2002. Metasomatic albitites and related biotite-rich schists from a low-pressure polymetamorphic terrane, Snake Creek Anticline, Mount Isa Inlier, north-eastern Australia: microstructures and P-T-d paths. *Journal of Metamorphic Geology*, 20, 191-202.
- Rudnicki, J.W., Rice, J.R., 1975. Conditions for the Localization of Deformation in Pressure Sensitive Materials. *J. Mech. and Phys. Sol.*, 23, 371-394.
- Ruffell, A.H., Moles, N.R., Parnell, J., 1998. Characterisation and prediction of sediment-hosted ore deposits using sequence stratigraphy. *Ore Geology Reviews*, 12, 207-223.
- Russell, M.J., 1978. Downward-excavating hydrothermal cells and Irish-type ore deposits: importance of an underlying thick Caledonian prism. *Trans. Inst. Min. Metal.*, 87b, 168-171.
- Russell, M. J., 1986. Extension and convection: a genetic model for the Irish Carboniferous base metal and barite deposits. *Geology and genesis of mineral deposits in Ireland*. Andrew, C J, Crowe, R. W. A., Finlay, S., Pennell, W. M., Pyne, J. F. (Eds). Dublin, Irish Association for Economic Geology, 545-553.
- Sangster, D.F., 1983. Sediment-hosted stratiform lead-zinc deposits. *Min. Assoc. Canada Short Course Handbook*, 8, pp.309.
- Sawkins, F.J., 1990. *Metal Deposits in Relation to Plate Tectonics*. Springer-Verlag, New York, pp. 388.
- Sayab, M., 2004a. Microstructural evidence for N-S shortening in the Mount Isa Inlier: the preservation of early W-E trending foliations in porphyroblasts revealed by independent 3-D measurement techniques. *Journal of Structural Geology* (in press).
- Sayab, M., 2004b. Decompression through an early clockwise P-T path in the Mount Isa Inlier: implications for early N-S shortening orogenesis. *Journal of Metamorphic Geology* (in press).
- Schaubs P.M., Zhao C., 2002. Numerical models of gold-deposit formation in the Bendigo-Ballarat Zone, Victoria. *Australian Journal of Earth Sciences*, 49, 6, 1077-1096.
- Schmitt, J.-M., Makhoukhi, S., Goblet, P., 1991. Modelling of structure-induced hydrothermal circulations in a Mississippi Valley Type deposit. *Source, Transport and Deposition of metals*. Pagel, M and Lery, J L. Rotterdam, Balkema. Proceedings of the 25 Yr SGA Anniversary Meeting, Nancy, France.

- Scott, D. L., Bradshaw, B. E., Tarlowski, C. Z., 1998. The tectono-stratigraphic history of the northern Lawn Hill Platform, Australia: an integrated intracontinental basin analysis. *Tectonophysics*, 300, 329–358.
- Scott, D.L., Rawlings, D.J., Page, R.W., Tarlowski, C.Z., Idnurm, M., Jackson, M.J., Southgate, P.N., 2000. Basement framework and geodynamic evolution of the Palaeoproterozoic superbasins of north central Australia: an integrated review of geochemical, geochronological and geophysical data. *Australian Journal of Earth Sciences* 47, 341-380.
- Sharpe, R., Gemmell, J.B., 2002. The Archaean Cu-Zn Magnetite-Rich Gossan Hill Volcanic-Hosted Massive Sulphide Deposit, Western Australia: Genesis of a Multistage Hydrothermal System. *Economic Geology*, 97, 517-541.
- Sibson, R., 1981. A brief description of natural neighbour interpolation. *Interpolating multivariate data*, Barnett, V. (Ed), John Wiley, 21-36.
- Sibson, R.H., 1985. Short Notes. A Note on Fault Reactivation. *Journal of Structural Geology*, 7, 6, 751-754.
- Sibson, R.H., 1987. Earthquake rupturing as a hydrothermal mineralising agent. *Geology* 15, 701-704.
- Sibson, R.H., 1992. Implications for fault-valve behaviour for rupture nucleation and recurrence. *Tectonophysics*, 211, 283-293.
- Sibson, R.H., 1994. Crustal stress, faulting and fluid flow. In: Parnell, J. (Ed) *Geofluids: Origin, Migration and Evolution of Fluids in Sedimentary Basins: Geological Society of London, Special Publication*, 78, 69-84.
- Sibson, R.H., 1996. Structural permeability of fluid-driven fault-fracture meshes. *Journal of Structural Geology*, 18, 8, 1031-1042.
- Sibson, R.H., 1998. Brittle failure mode plots for compressional and extensional tectonic regimes. *Journal of Structural Geology*, 20, 655-660.
- Sibson, R.H., Robert, F., Poulsen, K.H., 1988. High-angle reverse faults, fluid pressure cycling, and mesothermal gold-quartz deposits. *Geology*, 16, 551-555.

- Sibson, R.H., Moore, J., Rankin, A.H., 1995. Seismic pumping – a hydrothermal fluid transport mechanism. *Journal of the Geological Society of London*, 131, 653-659.
- Sillitoe, R.H., 1993. Giant and Bonanza Gold Deposits in the Epithermal Environment: Assessment of Potential Genetic Factors. In: Whiting, B.H., Hodgson, C.J. and Mason, R. (Eds.) *Giant Ore Deposits*, Special Publication Number 2, Society of Economic Geologists, 125-156.
- Simms, M.A., Garven, G., 2004. Thermal Convection in faulted extensional sedimentary basins: theoretical results from finite-element modelling. *Geofluids*, 4, 109-130.
- Smith, W.D., 1969. Penecontemporaneous faulting and its likely significance in relation to Mount Isa ore deposition. *Special Publications of the Geological Society of Australia*, 2, 225-235.
- Snow, D.T., 1968. Rock fracture spacings, openings and porosities. *J. Soil Mechanics., Found. Div., Proc. Am. Soc. Civil Engrs.*, 94, 73-91.
- Southgate, P. N., Bradshaw, B. E., Domagala, J. and others, 2000. Chronostratigraphic basin framework for Palaeoproterozoic rocks (1730–1575 Ma) in northern Australia and implications for base-metal mineralisation. *Australian Journal of Earth Sciences*, 47, 461–483.
- Spencer, J. E., Welty, J. W., 1986. Possible controls of base- and precious-metal mineralization associated with Tertiary detachment faults in the lower Colorado River trough, Arizona and California: *Geology*, 14, 195-198.
- Stephens, J. R., 2003. Structural, mechanical and P-T evolution of intrusion-related gold mineralization at Clear Creek and Dublin Gulch, Yukon, Canada. Unpublished PhD thesis, James Cook University, Australia.
- Stewart, A.J., Blake, D.H., 1992. Detailed studies of the Mount Isa Inlier: Australian Bureau of Mineral Research Bulletin, 243, pp. 374.
- Stober, I., Bucher, K., 2004. Fluid sinks within the earth's crust. *Geofluids*, 4, 2, 143-151.
- Sun, S.S., Page, R.W., Carr, G., 1994. Lead-isotope-based stratigraphic correlations and ages of Proterozoic sediment-hosted Pb-Zn deposits in the Mount Isa Inlier. *AGSO Bulletin*, 20, 1-2.

- Sweet, I. P., Mock, C. M., Mitchell, J. E., 1981. Seigal (Northern Territory) and Hedleys Creek (Queensland) 1:100 000 Geological Map Commentary. Bureau of Mineral Resources, Canberra.
- Sweet, I. P., Hutton, L. J., 1982. Lawn Hill Region 1: 100 000 geological map commentary. Bureau of Mineral Resources, Canberra.
- Tadakuza, U., Akira, I., Yu, Y., 2001. Horizontal Strain Rate in Relation to Vein Formation of the Hishikari Gold Deposits, Southern Kyushu, Japan. *Resource Geology*, 51, 1, 7-18.
- Taylor, D., Dalstra, H.J., Harding, A.E., Broadbent, G.C., Barley, M.E., 2001. Genesis of High-Grade Orebodies of the Hamersley Province, Western Australia. *Economic Geology* 96, 837-873.
- Taylor, D., Dalstra, H.J., Harding, A.E., 2002. Genesis of High-Grade Hematite Ore Bodies of the Hamersley Province, Western Australia – A Reply. *Economic Geology*, 97, 179-183.
- Terzaghi, K., 1925. *Erdaumechanik auf Bodenphysikalischer Grundlage*. Deutike, Leipzig.
- Terzaghi, K., 1943. *Theoretical Soil Mechanics*. John Wiley & Sons, New York.
- Terzaghi, K., 1945. Stress Conditions for the Failure of Saturated Concrete and Rock, *Proc. Am. Soc. Test. Mater.*, 45, 777-801.
- Tóth, J., 1962. A Theory of Groundwater Motion in Small Drainage basins in Central Alberta, Canada. *Journal of Geophysical Research*, 67, 11, 4375-4387.
- Tóth, J., 1963. A Theoretical Analysis of Groundwater Flow in Small Drainage Basins. *Journal of Geophysical Research*, 68, 16, 4795-4812.
- Trendall, A.F., Blockley, J.G., 1970. The iron formations of the Precambrian Hamersley Group, Western Australia, with special reference to the associated Crocidolite. *Geological Survey, Western Australian Bulletin*, 119, 365.
- Tresca, H., 1868. Mémoire sur l'écoulement des corps solides. *Mém. Prés. Div. Sav. Acad. Sci., Inst. Fr.* 18, 733-799.
- Turcotte, D.L., Schubert, G., 2002. *Geodynamics*, 2nd Edition, Cambridge University Press, U.K.

- Tyler, I.M., 1991. The geology of the Sylvania Inlier and southeastern Hamersley Basin. Geological Survey, Western Australian Bulletin, 138, 108.
- Tyler, I.M., Thorne, A.M., 1990. The northern margin of the Capricorn Orogen, Western Australia – an example of an Early Proterozoic collision zone. *Journal of Structural Geology*, 12, 685-701.
- Upton, P., 1998. Modelling Localization of deformation and Fluid Flow in a Compressional Orogen: Implications for the Southern Alps of New Zealand. *American Journal of Science*, 298, 296-323.
- Upton, P., Baxter, K., O'Brien, G.W., 1998. Coupled Mechanical / Fluid Flow Models of Trap Integrity and Fault Reactivation: Application to the North West Shelf of Australia. *Australian Petroleum Production and Exploration Association Journal* 1998, 488-499.
- Upton, P., Koons, P.O., Chamberlain, C.P., 1995. Penetration of deformation-driven meteoric water into ductile rocks: isotopic and model observations from the Southern Alps, New Zealand. *New Zealand Journal of Geology and Geophysics* 38, 535-543.
- Valenta, R.K., 1994. Syntectonic discordant copper mineralisation in the Hilton Mine, Mount Isa. *Economic Geology*, v89, pp. 1031-1052.
- Vermeer, P.A., de Borst, R., 1984. Non-associated plasticity for soils, concrete and rock. *Heron*. 29, 1-62.
- Waltho, A.E., Andrews, S.J., 1993. The Century Zinc-Lead Deposit, Northwest Queensland. *Proceedings of the Australasian Institute of Mining and Metallurgy Centenary Conference*, Adelaide, 41-61.
- Wang, S., Williams, P.J., 2001. Geochemistry and origin of Proterozoic skarns at the Mount Elliott Cu-Au(-Co-Ni) deposit, Cloncurry district, NW Queensland, Australia. *Mineralium Deposita*, 36, 109-124.
- Webb, A.D., Dickens, G.R., Oliver, N.H.S., 2003. From banded iron-formation to iron ore: geochemical and mineralogical constraints from across the Hamersley Province, Western Australia. *Chemical Geology*, 197, 215-251.
- Wernicke, B., 1981. Low angle normal faults in the Basin and Range province: nappe tectonics in an extending orogen: *Nature*, 291, 645-648.

- Wickham, S. M., Taylor, H. P. J., 1985. Stable isotopic evidence for large-scale seawater infiltration into a regional metamorphic terrane; the Trois Seigneurs Massif, Pyrenees, France: *Contrib. Mineral. Petrol.*, 91, 122-137.
- Williams, P.J., 1998. Metalliferous economic geology of the Mount Isa Eastern Succession, Queensland. *Australian Journal of Earth Sciences*, 45, 329-341.
- Williams, P. J., Barton, M. D., Fontboté, L., deHaller, A., Johnson, D. A., Mark, G., Marschik, R., Oliver, N. H. S., 2005. Iron oxide-copper-gold deposits: Geology, space-time distribution and possible modes of origin: *Econ. Geol.* (in press).
- Zengqian, H., Liquean, W., 2003. Post-collisional crustal extension setting and VHMS mineralization in the Jinshajiang orogenic belt, southwestern China: *Ore Geology Reviews*, 22, 177-199.
- Zhang, X., Sanderson, D.J., 2002. *Numerical Modelling and Analysis of Fluid Flow and Deformation of Fractured Rock Masses*. Pergamon, Elsevier, Oxford U.K.
- Zhang, Y., Hobbs, B.E., Ord, A., Muhlhaus, H-B., 1996a. Computer simulation of single-layer buckling. *Journal of Structural Geology*, 18, 643-655.
- Zhang, Y., Scheibner, E., Ord, A., Hobbs, B.E., 1996b. Numerical modelling of crustal stresses in the eastern Australian passive margin. *Australian Journal of Earth Sciences*, 43, 161-175.
- Zhang, Y., Hobbs, B.E., Ord, A., Barnicoat, A., Zhao, C., Walshe, J.L., Ge Lin, 2003. The influence of faulting on host-rock permeability, fluid flow and ore genesis of gold deposits: a theoretical 2D numerical model. *Journal of Geochemical Exploration - Conference Proceedings for GEOFLUIDS IV*, Vol. 78-79, 279-284.
- Zienkiewicz, O.C., Taylor, R.L., 1989. *The Finite Element Method*. McGraw-Hill, London.

Section B

Appendices

Appendix 1 – FLAC code

Appendix 2 – UDEC code

Appendix 1

FLAC numerical code

HM Hamersley Models

HM.1 Model 1 – Static mountain range

```

;
title
FLAC Modelling Input File
;
config extra 4 gw
grid 120 60
gen 0.00e0,-3.00e3 0.00e0,0.00e0 1.20e4,0.00e0 1.20e4,-3.00e3 i=1,121 j=1,61
gen 0.00e0,-3.00e3 0.00e0,0.00e0 1.50e3,0.00e0 1.50e3,-3.00e3 i=1,16 j=1,61
gen 1.50e3,-3.00e3 1.50e3,0.00e3 4.00e3,1.00e3 4.00e3,-3.00e3 i=16,41 j=1,61
gen 4.00e3,-3.00e3 4.00e3,1.00e3 8.00e3,1.00e3 8.00e3,-3.00e3 i=41,81 j=1,61
gen 8.00e3,-3.00e3 8.00e3,1.00e3 1.05e4,0.00e0 1.05e4,-3.00e3 i=81,106 j=1,61
gen 1.05e4,-3.00e3 1.05e4,0.00e0 1.20e4,0.00e0 1.20e4,-3.00e3 i=106,121 j=1,61

mark i=1
mark j=1
mark i = 121
mark j = 61
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3
set nmech 1 ngw 1 flow off
*****
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 77 , 16
pro coh=1.00e7 tens=1.00e6 reg= 77 , 16
pro fric=30 dil= 3 reg= 77 , 16
pro perm=1.00e-15 porosity=0.2 reg= 77 , 16

;
def hydro_pp
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa + 1e5
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*

ini sat 1
fix sat
fix pp i=1,121 j=61
set gravity=9.8
set large

;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=60 j=30
hist 3 pp i=60 j=5
hist 4 pp i=60 j=15
hist 5 pp i=60 j=30
hist 6 pp i=60 j=40
fix x i=1
fix x i=121

```

```

fix y j=1

plot pp fill
sav finoext1_ini.sav

plot pp fill
movie on file finoext1.dcx step 500

;RUN TO GRAVITY SETTLING
STEP 1500
;SET FLUID FLOW ON AND RUN TO EQUILIBRIUM
set flow on
;apply discharge 1e-10 i=41,81 j=61

pl pp fi fl bl
sav finoext1_grav.sav
step 1500

sav finoext1_flow.sav
;
free x
free y
fix x i=1
fix x i=121
fix y j=1

step 2500
save finoext1_1.sav;
step 2500
save finoext1_2.sav;
step 2500
save finoext1_3.sav;
step 2500
save finoext1_4.sav;

```

HM.2 Model 2 – Mountain range extension

```

;
title
FLAC Modelling Input File
;
config extra 4 gw
grid 120 60
gen 0.00e0,-3.00e3 0.00e0,0.00e0 1.20e4,0.00e0 1.20e4,-3.00e3 i=1,121 j=1,61
gen 0.00e0,-3.00e3 0.00e0,0.00e0 1.50e3,0.00e0 1.50e3,-3.00e3 i=1,16 j=1,61
gen 1.50e3,-3.00e3 1.50e3,0.00e3 4.00e3,1.00e3 4.00e3,-3.00e3 i=16,41 j=1,61
gen 4.00e3,-3.00e3 4.00e3,1.00e3 8.00e3,1.00e3 8.00e3,-3.00e3 i=41,81 j=1,61
gen 8.00e3,-3.00e3 8.00e3,1.00e3 1.05e4,0.00e0 1.05e4,-3.00e3 i=81,106 j=1,61
gen 1.05e4,-3.00e3 1.05e4,0.00e0 1.20e4,0.00e0 1.20e4,-3.00e3 i=106,121 j=1,61

mark i=1
mark j=1
mark i = 121
mark j = 61
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3
set nmech 1 ngw 1 flow off
*****
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 77 , 16
pro coh=1.00e7 tens=1.00e6 reg= 77 , 16
pro fric=30 dil= 3 reg= 77 , 16
pro perm=1.00e-15 porosity=0.2 reg= 77 , 16

;
def hydro_pp
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then

```

```
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa + 1e5
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
ini sat 1
fix sat
fix pp i=1,121 j=61
set gravity=9.8
set large

;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=60 j=30
hist 3 pp i=60 j=5
hist 4 pp i=60 j=15
hist 5 pp i=60 j=30
hist 6 pp i=60 j=40
fix x i=1
fix x i=121
fix y j=1

plot pp fill
sav finoext2_ini.sav

plot pp fill
movie on file finoext2.dcx step 500

;RUN TO GRAVITY SETTLING
STEP 1500
;SET FLUID FLOW ON AND RUN TO EQUILIBRIUM
set flow on
;apply discharge 1e-10 i=41,81 j=61

pl pp fi fl bl
sav finoext2_grav.sav
step 1500

sav finoext2_flow.sav
;
free x
free y
fix x i=1
fix x i=121
;fix y j=61
fix y j=1

ini xvel -0.024 var= 0.048 ,0 i=1, 121 j=1, 61

step 2500
save finext2_1.sav; 1 % deformation
step 2500
save finext2_2.sav; 2 % deformation
step 2500
save finext2_3.sav; 3 % deformation
step 2500
save finext2_4.sav; 4 % deformation
step 2500
save finext2_5.sav; 5 % deformation
step 2500
save finext2_6.sav; 6 % deformation
step 2500
save finext2_7.sav; 7 % deformation
step 2500
save finext2_8.sav; 8 % deformation
step 2500
save finext2_9.sav; 9 % deformation
step 2500
```

```

save finext2_10.sav; 10 % deformation
step 2500
save finext2_11.sav; 11 % deformation
step 2500
save finext2_12.sav; 12 % deformation
step 2500
save finext2_13.sav; 13 % deformation
step 2500
save finext2_14.sav; 14 % deformation
step 2500
save finext2_15.sav; 15 % deformation
step 2500
save finext2_16.sav; 16 % deformation
step 2500
save finext2_17.sav; 17 % deformation
step 2500
save finext2_18.sav; 18 % deformation
step 2500
save finext2_19.sav; 19 % deformation
step 2500
save finext2_20.sav; 20 % deformation
return
stop

```

HM.3 Model 3 – Mountain range extension with shear zone

```

;
tit
FLAC Modelling Input File
;
config extra 4 gw
grid 120 60
gen 0.00e0,-3.00e3 0.00e0,0.00e0 1.20e4,0.00e0 1.20e4,-3.00e3 i=1,121 j=1,61
gen 0.00e0,-3.00e3 0.00e0,0.00e0 1.50e3,0.00e0 1.50e3,-3.00e3 i=1,16 j=1,61
gen 1.50e3,-3.00e3 1.50e3,0.00e3 4.00e3,1.00e3 4.00e3,-3.00e3 i=16,41 j=1,61
gen 4.00e3,-3.00e3 4.00e3,1.00e3 8.00e3,1.00e3 8.00e3,-3.00e3 i=41,81 j=1,61
gen 8.00e3,-3.00e3 8.00e3,1.00e3 1.05e4,0.00e0 1.05e4,-3.00e3 i=81,106 j=1,61
gen 1.05e4,-3.00e3 1.05e4,0.00e0 1.20e4,0.00e0 1.20e4,-3.00e3 i=106,121 j=1,61

mark i=1
mark j=1
mark i = 121
mark j = 61
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3
set nmech 1 ngw 1 flow off
*****
tab 1 0 , -2506.14 12000 , -2506.14
tab 2 1000 , -3000 10300 , 1000 10900 , 1000
tab 2 1600 , -3000
;
tab 3 0 , -2006.43 3324.46 , -2006.43
;
tab 4 3885.76 , -2006.43 4197.59 , -2068.89 4484.48 , -2106.37
tab 4 5045.78 , -2093.88 5619.56 , -2031.41 6068.6 , -1968.95
tab 4 6542.59 , -1881.5 6979.16 , -1756.57 7503.04 , -1644.13
tab 4 7977.02 , -1619.15 8488.43 , -1669.12 8875.11 , -1781.56
tab 4 9286.73 , -1906.48 9673.4 , -2043.9 10134.92 , -2131.35
tab 4 10746.11 , -2143.85 11245.05 , -2081.38 11656.67 , -1993.93
tab 4 12000 , -1881.5
;
;
tab 5 4384.69 , -1794.05 4609.21 , -1831.53 4896.1 , -1844.02
tab 5 5257.83 , -1794.05 5669.45 , -1756.57 6068.6 , -1694.1
tab 5 6455.27 , -1594.16 6929.26 , -1481.73 7415.72 , -1381.79
tab 5 7814.87 , -1331.81 8201.55 , -1356.8 8638.11 , -1444.25
tab 5 9049.74 , -1556.68 9448.88 , -1694.1 9823.08 , -1819.03
tab 5 10234.71 , -1869 10733.64 , -1906.48 11220.1 , -1844.02
tab 5 11656.68 , -1706.6 12000 , -1569.18

```

```

:
:
tab 6 4883.63,-1569.18 5207.94,-1531.7 5482.35,-1494.22
tab 6 6031.18,-1394.28 6592.48,-1244.36 7041.52,-1131.93
tab 6 7552.93,-1044.48 8076.81,-994.51 8600.69,-1094.45
tab 6 9062.21,-1219.38 9548.67,-1381.79 10060.08,-1544.19
tab 6 10608.91,-1606.66 11070.42,-1556.68 11506.99,-1444.25
tab 6 12000,-1256.86
:
:
tab 7 5719.34,-1194.39 6118.49,-1119.44 6442.8,-1044.48
tab 7 6729.69,-982.02 7141.31,-869.58 7665.19,-757.15
tab 7 8201.55,-744.65 8737.9,-832.1 9286.73,-1031.99
tab 7 9723.3,-1169.41 10184.81,-1294.34 10571.49,-1331.81
tab 7 11020.53,-1306.83 11494.52,-1181.9 11793.88,-1069.46
tab 7 12000,-994.51
:
:
tab 8 4409.64,-1569.18 3835.86,-1331.81 3374.35,-1194.39
tab 8 2862.94,-1119.44 2301.64,-1119.44 1815.18,-1219.38
tab 8 1353.66,-1356.8 904.62,-1481.73 418.16,-1519.21
tab 8 0,-1481.73
:
:
tab 9 4758.89,-1394.28 4097.81,-1119.44 3673.71,-994.51
tab 9 3137.36,-882.07 2625.95,-869.58 2027.23,-919.55
tab 9 1490.87,-1044.48 966.99,-1194.39 555.37,-1269.35
tab 9 181.17,-1281.84 0,-1256.86
:
:
tab 10 5095.68,-1231.87 4472.01,-957.03 3823.39,-744.65
tab 10 3174.78,-644.71 2501.21,-607.23 1952.38,-657.2
tab 10 1416.03,-782.13 954.51,-907.06 443.11,-1007
tab 10 0,-994.51 0,-982.02
:
:
tab 11 5382.56,-1081.96 4634.16,-719.67 4147.7,-569.75
tab 11 3361.88,-419.84 2813.05,-382.36 2102.07,-407.35
tab 11 1353.66,-569.75 817.31,-694.68 293.43,-757.14
tab 11 0,-732.16
:
:gen tab 1
:gen tab 2
:gen tab 3
:gen tab 4
:gen tab 5
:gen tab 6
:gen tab 7
:gen tab 8
:gen tab 9
:gen tab 10
:gen tab 11

; Properties for each sub-regions:
:
; Fault
pro dens= 2400 bulk=2.33e8 shear=3.00e7 reg= 64 , 44
pro coh=2.00e2 tens=2.00e2 reg= 64 , 44
pro fric=30 dil= 4 reg= 64 , 44
pro perm=1.00e-13 porosity=0.3 reg= 64 , 44
; Fault
pro dens= 2400 bulk=2.33e8 shear=3.00e7 reg= 24 , 10
pro coh=2.00e2 tens=2.00e2 reg= 24 , 10
pro fric=30 dil= 4 reg= 24 , 10
pro perm=1.00e-13 porosity=0.3 reg= 24 , 10
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 6 , 55
pro coh=1.00e7 tens=1.00e6 reg= 6 , 55
pro fric=30 dil= 4 reg= 6 , 55
pro perm=1.00e-15 porosity=0.2 reg= 6 , 55
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 64 , 30
pro coh=1.00e7 tens=1.00e6 reg= 64 , 30
pro fric=30 dil= 3 reg= 64 , 30
pro perm=1.00e-15 porosity=0.2 reg= 64 , 30

```

```

; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 24 , 27
pro coh=1.00e7 tens=1.00e6 reg= 24 , 27
pro fric=30 dil= 3 reg= 24 , 27
pro perm=1.00e-15 porosity=0.2 reg= 24 , 27
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 106 , 50
pro coh=1.00e7 tens=1.00e6 reg= 106 , 50
pro fric=30 dil= 3 reg= 106 , 50
pro perm=1.00e-15 porosity=0.2 reg= 106 , 50
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 77 , 16
pro coh=1.00e7 tens=1.00e6 reg= 77 , 16
pro fric=30 dil= 3 reg= 77 , 16
pro perm=1.00e-15 porosity=0.2 reg= 77 , 16
;
*****
;
def hydro_pp
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa + 1e5
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
;
ini sat 1
fix sat
;fix pp i=1,121 j=61
set gravity=9.8
;
set large

;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=60 j=30
hist 3 pp i=60 j=5; basement
hist 4 pp i=60 j=15; footwall
hist 5 pp i=60 j=30; fault
hist 6 pp i=60 j=40; hangingwall

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTling
fix x i=1
fix x i=121
fix y j=1
apply syy -7.5e7 j=1

plot pp fill
sav finext3_ini.sav

;Create Movie files every 500 steps
plot pp fill
movie on file finext3.dcx step 500
;

;RUN TO GRAVITY SETTling
STEP 1500

;SET FLUID FLOW ON AND RUN TO EQUILIBRIUM
set flow on
apply discharge 1e-10 i=41,81 j=61

pl pp fi fl bl
sav finext3_grav.sav
step 1500

sav finext3_flow.sav

```



```

;
free x
free y
ini xvel -0.024 var= 0.048 ,0 i=1, 121 j=1, 61
fix x i=1
fix x i=121
;fix y j=61
fix y i=17,121 j=1 ; this fixes base on footwall side only, stress is applied to all to prevent drop on hangingwall
apply syy -7.5e7 j=1

step 2500
save finext3_1.sav; 1 % deformation
step 2500
save finext3_2.sav; 2 % deformation
step 2500
save finext3_3.sav; 3 % deformation
step 2500
save finext3_4.sav; 4 % deformation
step 2500
save finext3_5.sav; 5 % deformation
step 2500
save finext3_6.sav; 6 % deformation
step 2500
save finext3_7.sav; 7 % deformation
step 2500
save finext3_8.sav; 8 % deformation
step 2500
save finext3_9.sav; 9 % deformation
step 2500
save finext3_10.sav; 10 % deformation
step 2500
save finext3_11.sav; 11 % deformation
step 2500
save finext3_12.sav; 12 % deformation
step 2500
save finext3_13.sav; 13 % deformation
step 2500
save finext3_14.sav; 14 % deformation
step 2500
save finext3_15.sav; 15 % deformation
step 2500
save finext3_16.sav; 16 % deformation
step 2500
save finext3_17.sav; 17 % deformation
step 2500
save finext3_18.sav; 18 % deformation
step 2500
save finext3_19.sav; 19 % deformation
step 2500
save finext3_20.sav; 20 % deformation
return
stop

```

HM.4 Model 4 – Low permeability basement

```

;
tit
FLAC Modelling Input File
;
config extra 4 gw
grid 120 60
gen 0.00e0,-3.00e3 0.00e0,0.00e0 1.20e4,0.00e0 1.20e4,-3.00e3 i=1,121 j=1,61
gen 0.00e0,-3.00e3 0.00e0,0.00e0 1.50e3,0.00e0 1.50e3,-3.00e3 i=1,16 j=1,61
gen 1.50e3,-3.00e3 1.50e3,0.00e3 4.00e3,1.00e3 4.00e3,-3.00e3 i=16,41 j=1,61
gen 4.00e3,-3.00e3 4.00e3,1.00e3 8.00e3,1.00e3 8.00e3,-3.00e3 i=41,81 j=1,61
gen 8.00e3,-3.00e3 8.00e3,1.00e3 1.05e4,0.00e0 1.05e4,-3.00e3 i=81,106 j=1,61
gen 1.05e4,-3.00e3 1.05e4,0.00e0 1.20e4,0.00e0 1.20e4,-3.00e3 i=106,121 j=1,61

mark i=1
mark j=1

```

```

mark i = 121
mark j = 61
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3
set nmech 1 ngw 1 flow off
*****
;
tab 1 0,-2506.14 12000,-2506.14

;
tab 2 2139.49,-2500.29 10300,1000 10900,1000
tab 2 2738.21,-2500.29
tab 3 0,-2006.43 3324.46,-2006.43
;
;
tab 4 3885.76,-2006.43 4197.59,-2068.89 4484.48,-2106.37
tab 4 5045.78,-2093.88 5619.56,-2031.41 6068.6,-1968.95
tab 4 6542.59,-1881.5 6979.16,-1756.57 7503.04,-1644.13
tab 4 7977.02,-1619.15 8488.43,-1669.12 8875.11,-1781.56
tab 4 9286.73,-1906.48 9673.4,-2043.9 10134.92,-2131.35
tab 4 10746.11,-2143.85 11245.05,-2081.38 11656.67,-1993.93
tab 4 12000,-1881.5
;
;
tab 5 4384.69,-1794.05 4609.21,-1831.53 4896.1,-1844.02
tab 5 5257.83,-1794.05 5669.45,-1756.57 6068.6,-1694.1
tab 5 6455.27,-1594.16 6929.26,-1481.73 7415.72,-1381.79
tab 5 7814.87,-1331.81 8201.55,-1356.8 8638.11,-1444.25
tab 5 9049.74,-1556.68 9448.88,-1694.1 9823.08,-1819.03
tab 5 10234.71,-1869 10733.64,-1906.48 11220.1,-1844.02
tab 5 11656.68,-1706.6 12000,-1569.18
;
;
tab 6 4883.63,-1569.18 5207.94,-1531.7 5482.35,-1494.22
tab 6 6031.18,-1394.28 6592.48,-1244.36 7041.52,-1131.93
tab 6 7552.93,-1044.48 8076.81,-994.51 8600.69,-1094.45
tab 6 9062.21,-1219.38 9548.67,-1381.79 10060.08,-1544.19
tab 6 10608.91,-1606.66 11070.42,-1556.68 11506.99,-1444.25
tab 6 12000,-1256.86
;
;
tab 7 5719.34,-1194.39 6118.49,-1119.44 6442.8,-1044.48
tab 7 6729.69,-982.02 7141.31,-869.58 7665.19,-757.15
tab 7 8201.55,-744.65 8737.9,-832.1 9286.73,-1031.99
tab 7 9723.3,-1169.41 10184.81,-1294.34 10571.49,-1331.81
tab 7 11020.53,-1306.83 11494.52,-1181.9 11793.88,-1069.46
tab 7 12000,-994.51
;
;
tab 8 4409.64,-1569.18 3835.86,-1331.81 3374.35,-1194.39
tab 8 2862.94,-1119.44 2301.64,-1119.44 1815.18,-1219.38
tab 8 1353.66,-1356.8 904.62,-1481.73 418.16,-1519.21
tab 8 0,-1481.73
;
;
tab 9 4758.89,-1394.28 4097.81,-1119.44 3673.71,-994.51
tab 9 3137.36,-882.07 2625.95,-869.58 2027.23,-919.55
tab 9 1490.87,-1044.48 966.99,-1194.39 555.37,-1269.35
tab 9 181.17,-1281.84 0,-1256.86
;
;
tab 10 5095.68,-1231.87 4472.01,-957.03 3823.39,-744.65
tab 10 3174.78,-644.71 2501.21,-607.23 1952.38,-657.2
tab 10 1416.03,-782.13 954.51,-907.06 443.11,-1007
tab 10 0,-994.51 0,-982.02
;
;
tab 11 5382.56,-1081.96 4634.16,-719.67 4147.7,-569.75
tab 11 3361.88,-419.84 2813.05,-382.36 2102.07,-407.35
tab 11 1353.66,-569.75 817.31,-694.68 293.43,-757.14
tab 11 0,-732.16
;
gen tab 1
gen tab 2
gen tab 3
;gen tab 4
;gen tab 5
;gen tab 6
;gen tab 7
;gen tab 8

```

```

;gen tab 9
;gen tab 10
;gen tab 11
;
;
; Properties for each sub-regions:
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 92 , 4
pro coh=4.00e6 tens=4.00e5 reg= 92 , 4
pro fric=30 dil= 3 reg= 92 , 4
pro perm=2.00e-16 porosity=0.3 reg= 92 , 4
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 9 , 14
pro coh=4.00e6 tens=4.00e5 reg= 9 , 14
pro fric=30 dil= 3 reg= 9 , 14
pro perm=2.00e-16 porosity=0.3 reg= 9 , 14
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 7 , 4
pro coh=4.00e6 tens=4.00e5 reg= 7 , 4
pro fric=30 dil= 3 reg= 7 , 4
pro perm=2.00e-16 porosity=0.3 reg= 7 , 4
; Fault
pro dens= 2400 bulk=2.33e8 shear=3.00e7 reg= 64 , 44
pro coh=2.00e2 tens=2.00e2 reg= 64 , 44
pro fric=30 dil= 4 reg= 64 , 44
pro perm=1.00e-13 porosity=0.3 reg= 64 , 44
; Fault
pro dens= 2400 bulk=2.33e8 shear=3.00e7 reg= 24 , 10
pro coh=2.00e2 tens=2.00e2 reg= 24 , 10
pro fric=30 dil= 4 reg= 24 , 10
pro perm=1.00e-13 porosity=0.3 reg= 24 , 10
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 6 , 55
pro coh=1.00e7 tens=1.00e6 reg= 6 , 55
pro fric=30 dil= 4 reg= 6 , 55
pro perm=1.00e-15 porosity=0.2 reg= 6 , 55
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 64 , 30
pro coh=1.00e7 tens=1.00e6 reg= 64 , 30
pro fric=30 dil= 3 reg= 64 , 30
pro perm=1.00e-15 porosity=0.2 reg= 64 , 30
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 24 , 27
pro coh=1.00e7 tens=1.00e6 reg= 24 , 27
pro fric=30 dil= 3 reg= 24 , 27
pro perm=1.00e-15 porosity=0.2 reg= 24 , 27
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 106 , 50
pro coh=1.00e7 tens=1.00e6 reg= 106 , 50
pro fric=30 dil= 3 reg= 106 , 50
pro perm=1.00e-15 porosity=0.2 reg= 106 , 50
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 77 , 16
pro coh=1.00e7 tens=1.00e6 reg= 77 , 16
pro fric=30 dil= 3 reg= 77 , 16
pro perm=1.00e-15 porosity=0.2 reg= 77 , 16
;
def hydro_pp
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa + 1e5
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
```

```

; Set PP at Lithostatic in basement
;
def litho_pp
loop i (1,igp)
loop j (1,21)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 2650 * 9.8 * aaa + 1e5
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
litho_pp
*
;
ini sat 1
fix sat
;fix pp i=1,121 j=61

set gravity=9.8
set large

;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=60 j=30
hist 3 pp i=60 j=5; basement
hist 4 pp i=60 j=15; footwall
hist 5 pp i=60 j=30; fault
hist 6 pp i=60 j=40; hangingwall

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTLING
fix x i=1
fix x i=121
fix y j=1
apply syy -7.5e7 j=1

plot pp fill
sav finext4_ini.sav

;Create Movie files every 500 steps
plot pp fill
movie on file finext4.dcx step 500
;
;RUN TO GRAVITY SETTLING
STEP 1500
;SET FLUID FLOW ON AND RUN TO EQUILIBRIUM
set flow on
apply discharge 1e-10 i=41,81 j=61

pl pp fi fl bl
sav finext4_grav.sav
step 1500
sav finext4_flow.sav

free x
free y
ini xvel -0.024 var= 0.048 ,0 i=1, 121 j=1, 61
fix x i=1
fix x i=121
;fix y j=61
fix y i=26,121 j=1 ; this fixes base on footwall side only, stress is applied to all to prevent drop on hangingwall
apply syy -7.5e7 j=1

step 2500
save finext4_1.sav; 1 % deformation
step 2500
save finext4_2.sav; 2 % deformation
step 2500
save finext4_3.sav; 3 % deformation
step 2500
save finext4_4.sav; 4 % deformation

```

```

step 2500
save finext4_5.sav; 5 % deformation
step 2500
save finext4_6.sav; 6 % deformation
step 2500
save finext4_7.sav; 7 % deformation
step 2500
save finext4_8.sav; 8 % deformation
step 2500
save finext4_9.sav; 9 % deformation
step 2500
save finext4_10.sav; 10 % deformation
step 2500
save finext4_11.sav; 11 % deformation
step 2500
save finext4_12.sav; 12 % deformation
step 2500
save finext4_13.sav; 13 % deformation
step 2500
save finext4_14.sav; 14 % deformation
step 2500
save finext4_15.sav; 15 % deformation
step 2500
save finext4_16.sav; 16 % deformation
step 2500
save finext4_17.sav; 17 % deformation
step 2500
save finext4_18.sav; 18 % deformation
step 2500
save finext4_19.sav; 19 % deformation
step 2500
save finext4_20.sav; 20 % deformation
return
stop

```

HM.5 Model 5 – Hamersley Model

```

;
tit
FLAC Modelling Input File
;
config extra 4 gw
grid 120 60
gen 0.00e0,-3.00e3 0.00e0,0.00e0 1.20e4,0.00e0 1.20e4,-3.00e3 i=1,121 j=1,61
gen 0.00e0,-3.00e3 0.00e0,0.00e0 1.50e3,0.00e0 1.50e3,-3.00e3 i=1,16 j=1,61
gen 1.50e3,-3.00e3 1.50e3,0.00e3 4.00e3,1.00e3 4.00e3,-3.00e3 i=16,41 j=1,61
gen 4.00e3,-3.00e3 4.00e3,1.00e3 8.00e3,1.00e3 8.00e3,-3.00e3 i=41,81 j=1,61
gen 8.00e3,-3.00e3 8.00e3,1.00e3 1.05e4,0.00e0 1.05e4,-3.00e3 i=81,106 j=1,61
gen 1.05e4,-3.00e3 1.05e4,0.00e0 1.20e4,0.00e0 1.20e4,-3.00e3 i=106,121 j=1,61

mark i=1
mark j=1
mark i = 121
mark j = 61
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3
set nmech 1 ngw 1 flow off
*****
tab 1 0,-2506.14 12000,-2506.14
tab 2 2139.49,-2500.29 10300,1000 10900,1000
tab 2 2738.21,-2500.29
tab 3 0,-2006.43 3324.46,-2006.43
tab 4 3885.76,-2006.43 4197.59,-2068.89 4484.48,-2106.37
tab 4 5045.78,-2093.88 5619.56,-2031.41 6068.6,-1968.95
tab 4 6542.59,-1881.5 6979.16,-1756.57 7503.04,-1644.13
tab 4 7977.02,-1619.15 8488.43,-1669.12 8875.11,-1781.56
tab 4 9286.73,-1906.48 9673.4,-2043.9 10134.92,-2131.35
tab 4 10746.11,-2143.85 11245.05,-2081.38 11656.67,-1993.93

```

```

tab 4 12000 ,-1881.5
;
tab 5 4384.69 ,-1794.05 4609.21 ,-1831.53 4896.1 ,-1844.02
tab 5 5257.83 ,-1794.05 5669.45 ,-1756.57 6068.6 ,-1694.1
tab 5 6455.27 ,-1594.16 6929.26 ,-1481.73 7415.72 ,-1381.79
tab 5 7814.87 ,-1331.81 8201.55 ,-1356.8 8638.11 ,-1444.25
tab 5 9049.74 ,-1556.68 9448.88 ,-1694.1 9823.08 ,-1819.03
tab 5 10234.71 ,-1869 10733.64 ,-1906.48 11220.1 ,-1844.02
tab 5 11656.68 ,-1706.6 12000 ,-1569.18
;
tab 6 4883.63 ,-1569.18 5207.94 ,-1531.7 5482.35 ,-1494.22
tab 6 6031.18 ,-1394.28 6592.48 ,-1244.36 7041.52 ,-1131.93
tab 6 7552.93 ,-1044.48 8076.81 ,-994.51 8600.69 ,-1094.45
tab 6 9062.21 ,-1219.38 9548.67 ,-1381.79 10060.08 ,-1544.19
tab 6 10608.91 ,-1606.66 11070.42 ,-1556.68 11506.99 ,-1444.25
tab 6 12000 ,-1256.86
;
tab 7 5719.34 ,-1194.39 6118.49 ,-1119.44 6442.8 ,-1044.48
tab 7 6729.69 ,-982.02 7141.31 ,-869.58 7665.19 ,-757.15
tab 7 8201.55 ,-744.65 8737.9 ,-832.1 9286.73 ,-1031.99
tab 7 9723.3 ,-1169.41 10184.81 ,-1294.34 10571.49 ,-1331.81
tab 7 11020.53 ,-1306.83 11494.52 ,-1181.9 11793.88 ,-1069.46
tab 7 12000 ,-994.51
;
tab 8 4409.64 ,-1569.18 3835.86 ,-1331.81 3374.35 ,-1194.39
tab 8 2862.94 ,-1119.44 2301.64 ,-1119.44 1815.18 ,-1219.38
tab 8 1353.66 ,-1356.8 904.62 ,-1481.73 418.16 ,-1519.21
tab 8 0 ,-1481.73
;
tab 9 4758.89 ,-1394.28 4097.81 ,-1119.44 3673.71 ,-994.51
tab 9 3137.36 ,-882.07 2625.95 ,-869.58 2027.23 ,-919.55
tab 9 1490.87 ,-1044.48 966.99 ,-1194.39 555.37 ,-1269.35
tab 9 181.17 ,-1281.84 0 ,-1256.86
;
tab 10 5095.68 ,-1231.87 4472.01 ,-957.03 3823.39 ,-744.65
tab 10 3174.78 ,-644.71 2501.21 ,-607.23 1952.38 ,-657.2
tab 10 1416.03 ,-782.13 954.51 ,-907.06 443.11 ,-1007
tab 10 0 ,-994.51 0 ,-982.02
;
tab 11 5382.56 ,-1081.96 4634.16 ,-719.67 4147.7 ,-569.75
tab 11 3361.88 ,-419.84 2813.05 ,-382.36 2102.07 ,-407.35
tab 11 1353.66 ,-569.75 817.31 ,-694.68 293.43 ,-757.14
tab 11 0 ,-732.16
;
gen tab 1
gen tab 2
gen tab 3
gen tab 4
gen tab 5
gen tab 6
gen tab 7
gen tab 8
gen tab 9
gen tab 10
gen tab 11
;
; Properties for each sub-regions:
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 92 , 4
pro coh=4.00e6 tens=4.00e5 reg= 92 , 4
pro fric=30 dil= 3 reg= 92 , 4
pro perm=2.00e-16 porosity=0.3 reg= 92 , 4
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 9 , 14
pro coh=4.00e6 tens=4.00e5 reg= 9 , 14
pro fric=30 dil= 3 reg= 9 , 14
pro perm=2.00e-16 porosity=0.3 reg= 9 , 14
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 7 , 4
pro coh=4.00e6 tens=4.00e5 reg= 7 , 4
pro fric=30 dil= 3 reg= 7 , 4
pro perm=2.00e-16 porosity=0.3 reg= 7 , 4
; Fault
pro dens= 2400 bulk=2.33e8 shear=3.00e7 reg= 64 , 44
pro coh=2.00e2 tens=2.00e2 reg= 64 , 44

```

pro fric=30 dil= 4 reg= 64 , 44
pro perm=1.00e-13 porosity=0.3 reg= 64 , 44
; Fault
pro dens= 2400 bulk=2.33e8 shear=3.00e7 reg= 24 , 10
pro coh=2.00e2 tens=2.00e2 reg= 24 , 10
pro fric=30 dil= 4 reg= 24 , 10
pro perm=1.00e-13 porosity=0.3 reg= 24 , 10
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 24 , 35
pro coh=3.01e6 tens=1.50e6 reg= 24 , 35
pro fric=30 dil= 4 reg= 24 , 35
pro perm=1.00e-14 porosity=0.3 reg= 24 , 35
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 24 , 44
pro coh=3.01e6 tens=1.50e6 reg= 24 , 44
pro fric=30 dil= 4 reg= 24 , 44
pro perm=1.00e-14 porosity=0.3 reg= 24 , 44
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 45 , 14
pro coh=3.01e6 tens=3.00e5 reg= 45 , 14
pro fric=30 dil= 4 reg= 45 , 14
pro perm=1.00e-14 porosity=0.3 reg= 45 , 14
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 42 , 23
pro coh=3.01e6 tens=3.00e5 reg= 42 , 23
pro fric=30 dil= 4 reg= 42 , 23
pro perm=1.00e-14 porosity=0.3 reg= 42 , 23
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 43 , 23
pro coh=3.01e6 tens=3.00e5 reg= 43 , 23
pro fric=30 dil= 4 reg= 43 , 23
pro perm=1.00e-14 porosity=0.3 reg= 43 , 23
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 53 , 23
pro coh=3.01e6 tens=3.00e5 reg= 53 , 23
pro fric=30 dil= 4 reg= 53 , 23
pro perm=1.00e-14 porosity=0.3 reg= 53 , 23
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 55 , 24
pro coh=3.01e6 tens=3.00e5 reg= 55 , 24
pro fric=30 dil= 4 reg= 55 , 24
pro perm=1.00e-14 porosity=0.3 reg= 55 , 24
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 22 , 50
pro coh=3.01e6 tens=3.00e5 reg= 22 , 50
pro fric=30 dil= 4 reg= 22 , 50
pro perm=1.00e-14 porosity=0.3 reg= 22 , 50
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 84 , 42
pro coh=3.01e6 tens=3.00e5 reg= 84 , 42
pro fric=30 dil= 4 reg= 84 , 42
pro perm=1.00e-14 porosity=0.3 reg= 84 , 42
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 82 , 28
pro coh=3.01e6 tens=3.00e5 reg= 82 , 28
pro fric=30 dil= 4 reg= 82 , 28
pro perm=1.00e-14 porosity=0.3 reg= 82 , 28
; Shale
pro dens= 2500 bulk=2.81e10 shear=6.69e9 reg= 24 , 39
pro coh=3.00e6 tens=3.0e5 reg= 24 , 39
pro fric=30 dil= 4 reg= 24 , 39
pro perm=1.00e-19 porosity=0.3 reg= 24 , 39
; Shale
pro dens= 2500 bulk=2.81e10 shear=6.69e9 reg= 80 , 28
pro coh=3.00e6 tens=3.0e5 reg= 80 , 28
pro fric=30 dil= 4 reg= 80 , 28
pro perm=1.00e-19 porosity=0.3 reg= 80 , 28
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 6 , 55
pro coh=1.00e7 tens=1.00e6 reg= 6 , 55
pro fric=30 dil= 4 reg= 6 , 55
pro perm=1.00e-15 porosity=0.2 reg= 6 , 55
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 64 , 30
pro coh=1.00e7 tens=1.00e6 reg= 64 , 30

```

pro fric=30 dil= 3 reg= 64 , 30
pro perm=1.00e-15 porosity=0.2 reg= 64 , 30
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 24 , 27
pro coh=1.00e7 tens=1.00e6 reg= 24 , 27
pro fric=30 dil= 3 reg= 24 , 27
pro perm=1.00e-15 porosity=0.2 reg= 24 , 27
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 106 , 50
pro coh=1.00e7 tens=1.00e6 reg= 106 , 50
pro fric=30 dil= 3 reg= 106 , 50
pro perm=1.00e-15 porosity=0.2 reg= 106 , 50
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 77 , 16
pro coh=1.00e7 tens=1.00e6 reg= 77 , 16
pro fric=30 dil= 3 reg= 77 , 16
pro perm=1.00e-15 porosity=0.2 reg= 77 , 16
;
*****
;
def hydro_pp
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa + 1e5
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*

; Set PP at Lithostatic in basement
;
def litho_pp
loop i (1,igp)
loop j (1,21)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 2650 * 9.8 * aaa + 1e5
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
litho_pp
*

ini sat 1
fix sat
fix pp j=61

set gravity=9.8
set large

;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=60 j=30
hist 3 pp i=60 j=5; basement
hist 4 pp i=60 j=15; footwall
hist 5 pp i=60 j=30; fault
hist 6 pp i=60 j=40; hangingwall

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTLING
fix x i=1
fix x i=121
fix y j=1
apply syy -7.5e7 j=1

```



```
plot pp fill
sav finext5_ini.sav

;Create Movie files every 500 steps
plot pp fill
movie on file finext5.dcx step 500
;

;RUN TO GRAVITY SETTling
STEP 1500
;SET FLUID FLOW ON AND RUN TO EQUILIBRIUM
set flow on
apply discharge 1e-10 i=41,81 j=61

pl pp fi fl bl
sav finext5_grav.sav
step 1500
sav finext5_flow.sav
;
free x
free y
ini xvel -0.024 var= 0.048 ,0 i=1, 121 j=1, 61
fix x i=1
fix x i=121
;fix y j=61
fix y i=26,121 j=1 ; this fixes base on footwall side only, stress is applied to all to prevent drop on hangingwall
apply syy -7.5e7 j=1

step 2500
save finext5_1.sav; 1 % deformation
step 2500
save finext5_2.sav; 2 % deformation
step 2500
save finext5_3.sav; 3 % deformation
step 2500
save finext5_4.sav; 4 % deformation
step 2500
save finext5_5.sav; 5 % deformation
step 2500
save finext5_6.sav; 6 % deformation
step 2500
save finext5_7.sav; 7 % deformation
step 2500
save finext5_8.sav; 8 % deformation
step 2500
save finext5_9.sav; 9 % deformation
step 2500
save finext5_10.sav; 10 % deformation
step 2500
save finext5_11.sav; 11 % deformation
step 2500
save finext5_12.sav; 12 % deformation
step 2500
save finext5_13.sav; 13 % deformation
step 2500
save finext5_14.sav; 14 % deformation
step 2500
save finext5_15.sav; 15 % deformation
step 2500
save finext5_16.sav; 16 % deformation
step 2500
save finext5_17.sav; 17 % deformation
step 2500
save finext5_18.sav; 18 % deformation
step 2500
save finext5_19.sav; 19 % deformation
step 2500
save finext5_20.sav; 20 % deformation
return
stop
```

HM.6 Model 5 – Hamersley Model with silica dissolution

```

;
tit
FLAC Modelling Input File
;
config extra 4 gw
grid 120 60
gen 0.00e0,-3.00e3 0.00e0,0.00e0 1.20e4,0.00e0 1.20e4,-3.00e3 i=1,121 j=1,61
gen 0.00e0,-3.00e3 0.00e0,0.00e0 1.50e3,0.00e0 1.50e3,-3.00e3 i=1,16 j=1,61
gen 1.50e3,-3.00e3 1.50e3,0.00e3 4.00e3,1.00e3 4.00e3,-3.00e3 i=16,41 j=1,61
gen 4.00e3,-3.00e3 4.00e3,1.00e3 8.00e3,1.00e3 8.00e3,-3.00e3 i=41,81 j=1,61
gen 8.00e3,-3.00e3 8.00e3,1.00e3 1.05e4,0.00e0 1.05e4,-3.00e3 i=81,106 j=1,61
gen 1.05e4,-3.00e3 1.05e4,0.00e0 1.20e4,0.00e0 1.20e4,-3.00e3 i=106,121 j=1,61

;
mark i=1
mark j=1
mark i = 121
mark j = 61
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3
set nmech 1 ngw 1 flow off
*****
tab 1 0 ,-2506.14 12000 ,-2506.14
;
tab 2 2139.49 ,-2500.29 10300 , 1000 10900 , 1000
tab 2 2738.21 ,-2500.29
;
tab 3 0 ,-2006.43 3324.46 ,-2006.43
;
tab 4 3885.76 ,-2006.43 4197.59 ,-2068.89 4484.48 ,-2106.37
tab 4 5045.78 ,-2093.88 5619.56 ,-2031.41 6068.6 ,-1968.95
tab 4 6542.59 ,-1881.5 6979.16 ,-1756.57 7503.04 ,-1644.13
tab 4 7977.02 ,-1619.15 8488.43 ,-1669.12 8875.11 ,-1781.56
tab 4 9286.73 ,-1906.48 9673.4 ,-2043.9 10134.92 ,-2131.35
tab 4 10746.11 ,-2143.85 11245.05 ,-2081.38 11656.67 ,-1993.93
tab 4 12000 ,-1881.5
;
tab 5 4384.69 ,-1794.05 4609.21 ,-1831.53 4896.1 ,-1844.02
tab 5 5257.83 ,-1794.05 5669.45 ,-1756.57 6068.6 ,-1694.1
tab 5 6455.27 ,-1594.16 6929.26 ,-1481.73 7415.72 ,-1381.79
tab 5 7814.87 ,-1331.81 8201.55 ,-1356.8 8638.11 ,-1444.25
tab 5 9049.74 ,-1556.68 9448.88 ,-1694.1 9823.08 ,-1819.03
tab 5 10234.71 ,-1869 10733.64 ,-1906.48 11220.1 ,-1844.02
tab 5 11656.68 ,-1706.6 12000 ,-1569.18
;
tab 6 4883.63 ,-1569.18 5207.94 ,-1531.7 5482.35 ,-1494.22
tab 6 6031.18 ,-1394.28 6592.48 ,-1244.36 7041.52 ,-1131.93
tab 6 7552.93 ,-1044.48 8076.81 ,-994.51 8600.69 ,-1094.45
tab 6 9062.21 ,-1219.38 9548.67 ,-1381.79 10060.08 ,-1544.19
tab 6 10608.91 ,-1606.66 11070.42 ,-1556.68 11506.99 ,-1444.25
tab 6 12000 ,-1256.86
;
tab 7 5719.34 ,-1194.39 6118.49 ,-1119.44 6442.8 ,-1044.48
tab 7 6729.69 ,-982.02 7141.31 ,-869.58 7665.19 ,-757.15
tab 7 8201.55 ,-744.65 8737.9 ,-832.1 9286.73 ,-1031.99
tab 7 9723.3 ,-1169.41 10184.81 ,-1294.34 10571.49 ,-1331.81
tab 7 11020.53 ,-1306.83 11494.52 ,-1181.9 11793.88 ,-1069.46
tab 7 12000 ,-994.51
;
tab 8 4409.64 ,-1569.18 3835.86 ,-1331.81 3374.35 ,-1194.39
tab 8 2862.94 ,-1119.44 2301.64 ,-1119.44 1815.18 ,-1219.38
tab 8 1353.66 ,-1356.8 904.62 ,-1481.73 418.16 ,-1519.21
tab 8 0 ,-1481.73
;
tab 9 4758.89 ,-1394.28 4097.81 ,-1119.44 3673.71 ,-994.51
tab 9 3137.36 ,-882.07 2625.95 ,-869.58 2027.23 ,-919.55
tab 9 1490.87 ,-1044.48 966.99 ,-1194.39 555.37 ,-1269.35
tab 9 181.17 ,-1281.84 0 ,-1256.86
;

```

```

;
tab 10 5095.68 ,-1231.87 4472.01 ,-957.03 3823.39 ,-744.65
tab 10 3174.78 ,-644.71 2501.21 ,-607.23 1952.38 ,-657.2
tab 10 1416.03 ,-782.13 954.51 ,-907.06 443.11 ,-1007
tab 10 0 ,-994.51 0 ,-982.02
;
tab 11 5382.56 ,-1081.96 4634.16 ,-719.67 4147.7 ,-569.75
tab 11 3361.88 ,-419.84 2813.05 ,-382.36 2102.07 ,-407.35
tab 11 1353.66 ,-569.75 817.31 ,-694.68 293.43 ,-757.14
tab 11 0 ,-732.16
;
gen tab 1
gen tab 2
gen tab 3
gen tab 4
gen tab 5
gen tab 6
gen tab 7
gen tab 8
gen tab 9
gen tab 10
gen tab 11
;
;
; Properties for each sub-regions:
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 92 , 4
pro coh=4.00e6 tens=4.00e5 reg= 92 , 4
pro fric=30 dil= 3 reg= 92 , 4
pro perm=2.00e-16 porosity=0.3 reg= 92 , 4
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 9 , 14
pro coh=4.00e6 tens=4.00e5 reg= 9 , 14
pro fric=30 dil= 3 reg= 9 , 14
pro perm=2.00e-16 porosity=0.3 reg= 9 , 14
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 7 , 4
pro coh=4.00e6 tens=4.00e5 reg= 7 , 4
pro fric=30 dil= 3 reg= 7 , 4
pro perm=2.00e-16 porosity=0.3 reg= 7 , 4
; Fault
pro dens= 2400 bulk=2.33e8 shear=3.00e7 reg= 64 , 44
pro coh=2.00e2 tens=2.00e2 reg= 64 , 44
pro fric=30 dil= 4 reg= 64 , 44
pro perm=1.00e-13 porosity=0.3 reg= 64 , 44
; Fault
pro dens= 2400 bulk=2.33e8 shear=3.00e7 reg= 24 , 10
pro coh=2.00e2 tens=2.00e2 reg= 24 , 10
pro fric=30 dil= 4 reg= 24 , 10
pro perm=1.00e-13 porosity=0.3 reg= 24 , 10
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 24 , 35
pro coh=3.01e6 tens=1.50e6 reg= 24 , 35
pro fric=30 dil= 4 reg= 24 , 35
pro perm=1.00e-14 porosity=0.3 reg= 24 , 35
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 24 , 44
pro coh=3.01e6 tens=1.50e6 reg= 24 , 44
pro fric=30 dil= 4 reg= 24 , 44
pro perm=1.00e-14 porosity=0.3 reg= 24 , 44
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 45 , 14
pro coh=3.01e6 tens=3.00e5 reg= 45 , 14
pro fric=30 dil= 4 reg= 45 , 14
pro perm=1.00e-14 porosity=0.3 reg= 45 , 14
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 42 , 23
pro coh=3.01e6 tens=3.00e5 reg= 42 , 23
pro fric=30 dil= 4 reg= 42 , 23
pro perm=1.00e-14 porosity=0.3 reg= 42 , 23
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 43 , 23
pro coh=3.01e6 tens=3.00e5 reg= 43 , 23
pro fric=30 dil= 4 reg= 43 , 23
pro perm=1.00e-14 porosity=0.3 reg= 43 , 23

```

```

; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 53 , 23
pro coh=3.01e6 tens=3.00e5 reg= 53 , 23
pro fric=30 dil= 4 reg= 53 , 23
pro perm=1.00e-14 porosity=0.3 reg= 53 , 23
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 55 , 24
pro coh=3.01e6 tens=3.00e5 reg= 55 , 24
pro fric=30 dil= 4 reg= 55 , 24
pro perm=1.00e-14 porosity=0.3 reg= 55 , 24
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 22 , 50
pro coh=3.01e6 tens=3.00e5 reg= 22 , 50
pro fric=30 dil= 4 reg= 22 , 50
pro perm=1.00e-14 porosity=0.3 reg= 22 , 50
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 84 , 42
pro coh=3.01e6 tens=3.00e5 reg= 84 , 42
pro fric=30 dil= 4 reg= 84 , 42
pro perm=1.00e-14 porosity=0.3 reg= 84 , 42
; Bif
pro dens= 2800 bulk=3.21e10 shear=4.0e9 reg= 82 , 28
pro coh=3.01e6 tens=3.00e5 reg= 82 , 28
pro fric=30 dil= 4 reg= 82 , 28
pro perm=1.00e-14 porosity=0.3 reg= 82 , 28
; Shale
pro dens= 2500 bulk=2.81e10 shear=6.69e9 reg= 24 , 39
pro coh=3.00e6 tens=3.0e5 reg= 24 , 39
pro fric=30 dil= 4 reg= 24 , 39
pro perm=1.00e-19 porosity=0.3 reg= 24 , 39
; Shale
pro dens= 2500 bulk=2.81e10 shear=6.69e9 reg= 80 , 28
pro coh=3.00e6 tens=3.0e5 reg= 80 , 28
pro fric=30 dil= 4 reg= 80 , 28
pro perm=1.00e-19 porosity=0.3 reg= 80 , 28
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 6 , 55
pro coh=1.00e7 tens=1.00e6 reg= 6 , 55
pro fric=30 dil= 4 reg= 6 , 55
pro perm=1.00e-15 porosity=0.2 reg= 6 , 55
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 64 , 30
pro coh=1.00e7 tens=1.00e6 reg= 64 , 30
pro fric=30 dil= 3 reg= 64 , 30
pro perm=1.00e-15 porosity=0.2 reg= 64 , 30
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 24 , 27
pro coh=1.00e7 tens=1.00e6 reg= 24 , 27
pro fric=30 dil= 3 reg= 24 , 27
pro perm=1.00e-15 porosity=0.2 reg= 24 , 27
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 106 , 50
pro coh=1.00e7 tens=1.00e6 reg= 106 , 50
pro fric=30 dil= 3 reg= 106 , 50
pro perm=1.00e-15 porosity=0.2 reg= 106 , 50
; Upper Crust
pro dens= 2700 bulk=2.33e10 shear=6.40e9 reg= 77 , 16
pro coh=1.00e7 tens=1.00e6 reg= 77 , 16
pro fric=30 dil= 3 reg= 77 , 16
pro perm=1.00e-15 porosity=0.2 reg= 77 , 16
;
;
def hydro_pp
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa + 1e5
end_if
gpp(i, j) = sss2
end_loop
end_loop

```

```

end
hydro_pp
*

; Set PP at Lithostatic in basement

def litho_pp
loop i (1,igp)
loop j (1,21)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 2650 * 9.8 * aaa + 1e5
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
litho_pp
*
;
ini sat 1
fix sat
fix pp j=61

set gravity=9.8
set large

;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=60 j=30
hist 3 pp i=60 j=5; basement
hist 4 pp i=60 j=15; footwall
hist 5 pp i=60 j=30; fault
hist 6 pp i=60 j=40; hangingwall

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTling
fix x i=1
fix x i=121
fix y j=1
apply syy -7.5e7 j=1

plot pp fill
sav finext5_rep_ini.sav

;Create Movie files every 500 steps
plot pp fill
movie on file finext5_rep.dcx step 500
;

;RUN TO GRAVITY SETTling
STEP 1500
;SET FLUID FLOW ON AND RUN TO EQUILIBRIUM
set flow on
apply discharge 1e-10 i=41,81 j=61

pl pp fi fl bl
sav finext5_rep_grav.sav
step 1500

sav finext5_rep_flow.sav
;
;Reaction enhanced permeability function

table 5 0,1e-15 1e-20,1e-15 1e-15,1e-15 1e-14,1e-14
table 5 1e-13,1e-14 1e-12,1e-14 1e-11,9e-13
table 5 9e-10,9e-13 8e-10,8e-13
table 5 7e-10,7e-13 6e-10,6e-13 5e-10,5e-13 4e-10,4e-13
table 5 3e-10,3e-13 2e-10,2e-13 1e-10,1e-13 1e-8,1e-13; maxflow,perm (start with 0,original perm)

def incr_perm2
while_stepping

```

```
loop i (1, izones)
loop j (1, jzones)
ex_2(i,j)=sqrt((xflow(i,j)^2)+(yflow(i,j)^2)) ; puts flow rate into an extra variable
if cohesion(i,j) = 3.01e6 then
k11(i,j)=table(5,ex_2(i,j))
k22(i,j)=k11(i,j)
k12(i,j)=0
;end_if
end_if
end_loop
end_loop
end
incr_perm2

free x
free y
ini xvel -0.024 var= 0.048 ,0 i=1, 121 j=1, 61
fix x i=1
;fix x i=121
;fix y j=61
fix y i=26,121 j=1 ; this fixes base on footwall side only, stress is applied to all to prevent drop on hangingwall
apply sy -7.5e7 j=1

step 2500
save finext5_rep_1.sav; 1 % deformation
step 2500
save finext5_rep_2.sav; 2 % deformation
step 2500
save finext5_rep_3.sav; 3 % deformation
step 2500
save finext5_rep_4.sav; 4 % deformation
step 2500
save finext5_rep_5.sav; 5 % deformation
step 2500
save finext5_rep_6.sav; 6 % deformation
step 2500
save finext5_rep_7.sav; 7 % deformation
step 2500
save finext5_rep_8.sav; 8 % deformation
step 2500
save finext5_rep_9.sav; 9 % deformation
step 2500
save finext5_rep_10.sav; 10 % deformation
step 2500
save finext5_rep_11.sav; 11 % deformation
step 2500
save finext5_rep_12.sav; 12 % deformation
step 2500
save finext5_rep_13.sav; 13 % deformation
step 2500
save finext5_rep_14.sav; 14 % deformation
step 2500
save finext5_rep_15.sav; 15 % deformation
step 2500
save finext5_rep_16.sav; 16 % deformation
step 2500
save finext5_rep_17.sav; 17 % deformation
step 2500
save finext5_rep_18.sav; 18 % deformation
step 2500
save finext5_rep_19.sav; 19 % deformation
step 2500
save finext5_rep_20.sav; 20 % deformation
return
stop
```

C Century Models

C.1 Model 1a

```

;
tit
Century Model 1 - Extension
;
config extra 4 gw
grid 80 80
gen 0.00e0,-2.40e3 0.00e0,-2.00e3 4.00e2,-2.00e3 4.00e2,-2.40e3 i=1,81 j=1,81
mark i=1
mark j=1
mark i = 81
mark j = 81
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3 ; to be elaborated below
;; 1 mech step = 1 fluid step; modify if necessary!!!
set nmech 1 ngw 1 flow off
*****
tab 1 0 , -2175.03 205.11 , -2175.03
;
tab 2 221.48 , -2155.5 400 , -2155.5
;
tab 3 0 , -2271.87 155.99 , -2271.87
;
tab 4 173.92 , -2250.78 400 , -2250.78
;
tab 5 0 , -2321.85 131.03 , -2321.85
;
tab 6 148.97 , -2301.54 400 , -2301.54
;
tab 7 0 , -2289.05 148.19 , -2289.05
;
tab 8 164.56 , -2268.74 400 , -2268.74
;
tab 9 0 , -2297.64 143.51 , -2297.64
;
tab 10 159.88 , -2278.12 400 , -2278.12
;
tab 11 155.99 , -2286.71 400 , -2286.71
;
tab 12 137.27 , -2308.57 0 , -2307.79
;
tab 13 292.44 , -2000 91.27 , -2400
;
tab 14 100.62 , -2400 300.24 , -2000
;
gen tab 1
gen tab 2
gen tab 3
gen tab 4
gen tab 5
gen tab 6
gen tab 7
gen tab 8
gen tab 9
gen tab 10
gen tab 11
gen tab 12
gen tab 13
gen tab 14
;
; Moving the gridpoints i=20 j=1 at base
; Moving i=60 j=80 at top of fault to straighten it out
ini x add -3 i=20 j=1
ini x add -2 i=21 j=1

```

```

ini x add -3 i=22 j=1

ini x add 3 i=59 j=81
ini x add 2 i=60 j=81

ini y add 3 i=60 j=80

; Properties for each sub-regions:
; Sand
pro dens= 1600 bulk=8.33e6 shear=1.88e7 reg= 22 , 61
pro coh= 3.0e3 tens= 1.0e3 reg= 22 , 61
pro fric=30 dil= 5 reg= 22 , 61
pro perm=1.00e-12 porosity=0.4 reg= 22 , 61
; Sand
pro dens= 1600 bulk=8.33e6 shear=1.88e7 reg= 66 , 60
pro coh= 3.0e3 tens= 1.0e3 reg= 66 , 60
pro fric=30 dil= 5 reg= 66 , 60
pro perm=1.00e-12 porosity=0.4 reg= 66 , 60
; Silt
pro dens= 1700 bulk=3.00e6 shear=7.5e6 reg= 17 , 34
pro coh= 3.0e3 tens= 1.0e3 reg= 17 , 34
pro fric=25 dil= 5 reg= 17 , 34
pro perm=1.00e-13 porosity=0.4 reg= 17 , 34
; Silt
pro dens= 1700 bulk=3.00e6 shear=7.5e6 reg= 60 , 38
pro coh= 1.0e4 tens= 1.0e3 reg= 60 , 38
pro fric=25 dil= 5 reg= 60 , 38
pro perm=1.00e-13 porosity=0.4 reg= 60 , 38
; Shale (clay layers)
pro dens= 1800 bulk=3.01e6 shear=5e6 reg= 11 , 8
pro coh= 1.0e3 tens= 1.0e2 reg= 11 , 8
pro fric=20 dil= 2 reg= 11 , 8
pro perm=1.00e-14 porosity=0.3 reg= 11 , 8
; Shale
pro dens= 1800 bulk=3.01e6 shear=5.01e6 reg= 57 , 8
pro coh= 1.0e3 tens= 1.0e2 reg= 57 , 8
pro fric=20 dil= 2 reg= 57 , 8
pro perm=1.00e-14 porosity=0.3 reg= 57 , 8

; ORE ZONE
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 reg= 5 , 24
pro coh= 2.0e3 tens= 5.0e2 reg= 5 , 24
pro fric=22 dil= 3 reg= 5 , 24
pro perm=5.00e-13 porosity=0.35 reg= 5 , 24
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 reg= 55 , 28
pro coh= 2.0e3 tens= 5.0e2 reg= 55 , 28
pro fric=22 dil= 3 reg= 55 , 28
pro perm=5.00e-13 porosity=0.35 reg= 55 , 28
; Shale
pro dens= 1800 bulk=3.01e6 shear=5.01e6 reg= 3 , 21
pro coh= 1.0e3 tens= 1.0e2 reg= 3 , 21
pro fric=20 dil= 2 reg= 3 , 21
pro perm=1.00e-14 porosity=0.3 reg= 3 , 21
; Shale
pro dens= 1800 bulk=3.01e6 shear=5.01e6 reg= 75 , 25
pro coh= 1.0e3 tens= 1.0e2 reg= 75 , 25
pro fric=20 dil= 2 reg= 75 , 25
pro perm=1.00e-14 porosity=0.3 reg= 75 , 25
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 reg= 12 , 19
pro coh= 2.0e3 tens= 5.0e2 reg= 12 , 19
pro fric=22 dil= 3 reg= 12 , 19
pro perm=5.00e-13 porosity=0.35 reg= 12 , 19
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 reg= 32 , 23
pro coh= 2.0e3 tens= 5.0e2 reg= 32 , 23
pro fric=22 dil= 3 reg= 32 , 23
pro perm=5.00e-13 porosity=0.35 reg= 32 , 23
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 i= 34 j= 24
pro coh= 2.0e3 tens= 5.0e2 i= 34 j= 24
pro fric=22 dil= 3 i= 34 j= 24

```



```

pro perm=5.00e-13 porosity=0.35 i= 34 j= 24

; Silt / Mud -as silt/shale prop (silt & clay)
pro dens= 1750 bulk=8.0e5 shear=9.5e5 reg= 5 , 17
pro coh= 2.0e3 tens= 5.0e2 reg= 5 , 17
pro fric=22 dil= 3 reg= 5 , 17
pro perm=2.00e-14 porosity=0.35 reg= 5 , 17
; Silt / Mud
pro dens= 1750 bulk=8.0e5 shear=9.5e5 reg= 55 , 21
pro coh= 2.0e3 tens= 5.0e2 reg= 55 , 21
pro fric=22 dil= 3 reg= 55 , 21
pro perm=2.00e-14 porosity=0.35 reg= 55 , 21
;END ORE ZONE

pro dens= 1600 bulk=3.33e5 shear=7.00e4 reg= 58 , 78
pro coh= 1.0e3 tens= 1.0e2 reg= 58 , 78
pro fric=20 dil= 5 reg= 58 , 78
pro perm=1.00e-12 porosity=0.6 reg= 58 , 78
; Fault
pro dens= 1600 bulk=3.33e5 shear=7.00e4 reg= 21 , 3
pro coh= 1.0e3 tens= 1.0e2 reg= 21 , 3
pro fric=20 dil= 5 reg= 21 , 3
pro perm=1.00e-12 porosity=0.6 reg= 21 , 3
; Fault
pro dens= 1600 bulk=3.33e5 shear=7.00e4 reg= 21 , 1
pro coh= 1.0e3 tens= 1.0e2 reg= 21 , 1
pro fric=20 dil= 5 reg= 21 , 1
pro perm=1.00e-12 porosity=0.6 reg= 21 , 1
; Fault
pro dens= 1600 bulk=3.33e5 shear=7.00e4 reg= 21 , 2
pro coh= 1.0e3 tens= 1.0e2 reg= 21 , 2
pro fric=20 dil= 5 reg= 21 , 2
pro perm=1.00e-12 porosity=0.6 reg= 21 , 2
; Fault
pro dens= 1600 bulk=3.33e5 shear=7.00e4 reg= 20 , 1
pro coh= 1.0e3 tens= 1.0e2 reg= 20 , 1
pro fric=20 dil= 5 reg= 20 , 1
pro perm=1.00e-12 porosity=0.6 reg= 20 , 1
; Fault
pro dens= 1600 bulk=3.33e5 shear=7.00e4 reg= 21 , 2
pro coh= 1.0e3 tens= 1.0e2 reg= 21 , 2
pro fric=20 dil= 5 reg= 21 , 2
pro perm=1.00e-12 porosity=0.6 reg= 21 , 2

;ORE ZONE
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 i= 33,80 j= 24
pro coh= 2.0e3 tens= 5.0e2 i= 33,80 j= 24
pro fric=22 dil= 3 i= 33,80 j= 24
pro perm=5.00e-13 porosity=0.35 i= 33,80 j= 24
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 i= 34 j= 27
pro coh= 2.0e3 tens= 5.0e2 i= 34 j= 27
pro fric=22 dil= 3 i= 34 j= 27
pro perm=5.00e-13 porosity=0.35 i= 34 j= 27
;END ORE ZONE

; Silt
pro dens= 1700 bulk=3.00e6 shear=7.5e6 i= 36 j= 31
pro coh= 3.0e3 tens= 1.0e3 i=36 j= 31
pro fric=25 dil= 5 i= 36 j= 31
pro perm=1.00e-13 porosity=0.4 i=36 j= 31
; Silt
pro dens= 1700 bulk=3.00e6 shear=7.5e6 i= 41 j= 45
pro coh= 3.0e3 tens= 1.0e4 i=41 j= 45
pro fric=25 dil= 5 i= 41 j= 45
pro perm=1.00e-13 porosity=0.4 i=41 j= 45

;ORE ZONE
; Silt / Mud
pro dens= 1750 bulk=8.0e5 shear=9.5e5 i= 31 j= 21
pro coh= 2.0e3 tens= 5.0e2 i= 31 j= 21
pro fric=22 dil= 3 i= 31 j= 21
pro perm=2.00e-14 porosity=0.35 i= 31 j= 21

```

```

; Shale
pro dens= 1800 bulk=3.01e6 shear=5.01e6 i=33 j=25
pro coh= 1.0e3 tens= 1.0e2 i=33 j=25
pro fric=20 dil= 2 i=33 j=25
pro perm=1.00e-14 porosity=0.3 i=33 j=25
;END ORE ZONE

;-----END OF PROPERTIES-----

def ini_stress
hh1 = 0.5*abs(y(1,2) - y(1,1))
surf_load = -2.0e3*9.8*2500
str_add = hh1*9.8*2700
bot_str = (-1.0)*(2.4e3*9.8*2500 - str_add)
top_str = (-1.0)*(2.0e3*9.8*2500 + str_add)

str_var = top_str - bot_str

command
ini sxx bot_str var=0,str_var i=1,80 j=1,80
ini syy bot_str var=0,str_var i=1,80 j=1,80
ini szz bot_str var=0,str_var i=1,80 j=1,80
ini sxy = 0.0
end_command

end
ini_stress

apply ns surf_load i=1,81 j=81

def hydro_pp

surf_pp = 2.5e3*9.8*1000 + 1e5 ;pp (2.0km) + pp (atmospheric loading)

loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
;sss2 = 0
sss2 = surf_pp

else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa + surf_pp
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
;
;
ini sat 1
fix sat
fix pp j=81
;
set gravity=9.8
;
set large
;
;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=40 j=40
hist 3 pp i=40 j=40

;Movie every 500 steps
plot pp fill
sav sm1a_ini.sav
movie on file sm1a.dcx step 500

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTLING
fix x i=1
fix x i=81
fix y j=1

```

```
; Gravity settling
STEP 1500

;Set fluid on run to equilibrium
set flow on
pl pp fi fl bl
STEP 1500

free x
free y

ini xvel -0.0008 var = 0.0016 ,0 i=1, 81 j=1, 81
fix x i=1
fix x i= 81
fix y j=1

sav sm1a_def.sav

step 5000
save sm1a_1.sav; 1%
step 5000
save sm1a_2.sav;
step 5000
save sm1a_3.sav;
step 5000
save sm1a_4.sav;
step 5000
save sm1a_5.sav;

step 5000
save sm1a_6.sav;
step 5000
save sm1a_7.sav;
step 5000
save sm1a_8.sav;
step 5000
save sm1a_9.sav;
step 5000
save sm1a_10.sav;

step 5000
save sm1a_11.sav;
step 5000
save sm1a_12.sav;
step 5000
save sm1a_13.sav;
step 5000
save sm1a_14.sav;
step 5000
save sm1a_15.sav;

step 5000
save sm1a_16.sav;
step 5000
save sm1a_17.sav;
step 5000
save sm1a_18.sav;
step 5000
save sm1a_19.sav;
step 5000
save sm1a_20.sav;

return
stop
```

C.2 Model 1b

```

;
tit
Century Model 1 - Extension
;
config extra 4 gw
grid 80 80
gen 0.00e0,-2.40e3 0.00e0,-2.00e3 4.00e2,-2.00e3 4.00e2,-2.40e3 i=1,81 j=1,81
mark i=1
mark j=1
mark i = 81
mark j = 81
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3 ; to be elaborated below
;; 1 mech step = 10 fluid step; modify if necessary!!!
set nmech 1 ngw 1 flow off
*****
;
GEOMETRY AS PREVIOUS MODEL
; Properties for each sub-regions:
; Sand
pro dens= 1600 bulk=8.33e6 shear=1.88e7 reg= 22 , 61
pro coh= 3.0e3 tens= 1.0e3 reg= 22 , 61
pro fric=30 dil= 5 reg= 22 , 61
pro perm=1.00e-12 porosity=0.4 reg= 22 , 61
; Sand
pro dens= 1600 bulk=8.33e6 shear=1.88e7 reg= 66 , 60
pro coh= 3.0e3 tens= 1.0e3 reg= 66 , 60
pro fric=30 dil= 5 reg= 66 , 60
pro perm=1.00e-12 porosity=0.4 reg= 66 , 60
; Silt
pro dens= 1700 bulk=3.00e6 shear=7.5e6 reg= 17 , 34
pro coh= 3.0e3 tens= 1.0e3 reg= 17 , 34
pro fric=25 dil= 5 reg= 17 , 34
pro perm=1.00e-13 porosity=0.4 reg= 17 , 34
; Silt
pro dens= 1700 bulk=3.00e6 shear=7.5e6 reg= 60 , 38
pro coh= 1.0e4 tens= 1.0e3 reg= 60 , 38
pro fric=25 dil= 5 reg= 60 , 38
pro perm=1.00e-13 porosity=0.4 reg= 60 , 38
; Shale (clay layers)
pro dens= 1800 bulk=3.01e6 shear=5e6 reg= 11 , 8
pro coh= 1.0e3 tens= 1.0e2 reg= 11 , 8
pro fric=20 dil= 2 reg= 11 , 8
pro perm=1.00e-14 porosity=0.3 reg= 11 , 8
; Shale
pro dens= 1800 bulk=3.01e6 shear=5.01e6 reg= 57 , 8
pro coh= 1.0e3 tens= 1.0e2 reg= 57 , 8
pro fric=20 dil= 2 reg= 57 , 8
pro perm=1.00e-14 porosity=0.3 reg= 57 , 8
; ORE ZONE
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 reg= 5 , 24
pro coh= 2.0e3 tens= 5.0e2 reg= 5 , 24
pro fric=22 dil= 3 reg= 5 , 24
pro perm=5.00e-13 porosity=0.35 reg= 5 , 24
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 reg= 55 , 28
pro coh= 2.0e3 tens= 5.0e2 reg= 55 , 28
pro fric=22 dil= 3 reg= 55 , 28
pro perm=5.00e-13 porosity=0.35 reg= 55 , 28
; Shale
pro dens= 1800 bulk=3.01e6 shear=5.01e6 reg= 3 , 21
pro coh= 1.0e3 tens= 1.0e2 reg= 3 , 21
pro fric=20 dil= 2 reg= 3 , 21

```

```

pro perm=1.00e-12 porosity=0.3 reg= 3 , 21
; Shale
pro dens= 1800 bulk=3.01e6 shear=5.01e6 reg= 75 , 25
pro coh= 1.0e3 tens= 1.0e2 reg= 75 , 25
pro fric=20 dil= 2 reg= 75 , 25
pro perm=1.00e-12 porosity=0.3 reg= 75 , 25
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 reg= 12 , 19
pro coh= 2.0e3 tens= 5.0e2 reg= 12 , 19
pro fric=22 dil= 3 reg= 12 , 19
pro perm=5.00e-13 porosity=0.35 reg= 12 , 19
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 reg= 32 , 23
pro coh= 2.0e3 tens= 5.0e2 reg= 32 , 23
pro fric=22 dil= 3 reg= 32 , 23
pro perm=5.00e-13 porosity=0.35 reg= 32 , 23
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 i= 34 j= 24
pro coh= 2.0e3 tens= 5.0e2 i= 34 j= 24
pro fric=22 dil= 3 i= 34 j= 24
pro perm=5.00e-13 porosity=0.35 i= 34 j= 24
; Silt / Mud -as silt/shale prop (silt & clay)
pro dens= 1750 bulk=8.0e5 shear=9.5e5 reg= 5 , 17
pro coh= 2.0e3 tens= 5.0e2 reg= 5 , 17
pro fric=22 dil= 3 reg= 5 , 17
pro perm=2.00e-14 porosity=0.35 reg= 5 , 17
; Silt / Mud
pro dens= 1750 bulk=8.0e5 shear=9.5e5 reg= 55 , 21
pro coh= 2.0e3 tens= 5.0e2 reg= 55 , 21
pro fric=22 dil= 3 reg= 55 , 21
pro perm=2.00e-14 porosity=0.35 reg= 55 , 21
;END ORE ZONE

```

```

; Fault
pro dens= 1600 bulk=3.33e5 shear=7.00e4 reg= 58 , 78
pro coh= 1.0e3 tens= 1.0e2 reg= 58 , 78
pro fric=20 dil= 5 reg= 58 , 78
pro perm=1.00e-12 porosity=0.6 reg= 58 , 78
; Fault
pro dens= 1600 bulk=3.33e5 shear=7.00e4 reg= 21 , 3
pro coh= 1.0e3 tens= 1.0e2 reg= 21 , 3
pro fric=20 dil= 5 reg= 21 , 3
pro perm=1.00e-12 porosity=0.6 reg= 21 , 3
; Fault
pro dens= 1600 bulk=3.33e5 shear=7.00e4 reg= 21 , 1
pro coh= 1.0e3 tens= 1.0e2 reg= 21 , 1
pro fric=20 dil= 5 reg= 21 , 1
pro perm=1.00e-12 porosity=0.6 reg= 21 , 1
; Fault
pro dens= 1600 bulk=3.33e5 shear=7.00e4 reg= 21 , 2
pro coh= 1.0e3 tens= 1.0e2 reg= 21 , 2
pro fric=20 dil= 5 reg= 21 , 2
pro perm=1.00e-12 porosity=0.6 reg= 21 , 2
; Fault
pro dens= 1600 bulk=3.33e5 shear=7.00e4 reg= 20 , 1
pro coh= 1.0e3 tens= 1.0e2 reg= 20 , 1
pro fric=20 dil= 5 reg= 20 , 1
pro perm=1.00e-12 porosity=0.6 reg= 20 , 1
; Fault
pro dens= 1600 bulk=3.33e5 shear=7.00e4 reg= 21 , 2
pro coh= 1.0e3 tens= 1.0e2 reg= 21 , 2
pro fric=20 dil= 5 reg= 21 , 2
pro perm=1.00e-12 porosity=0.6 reg= 21 , 2

```

```

;ORE ZONE
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 i= 33,80 j= 24
pro coh= 2.0e3 tens= 5.0e2 i= 33,80 j= 24
pro fric=22 dil= 3 i= 33,80 j= 24
pro perm=5.00e-13 porosity=0.35 i= 33,80 j= 24
; Silt / Shale
pro dens= 1750 bulk=8.0e5 shear=7.00e6 i= 34 j= 27
pro coh= 2.0e3 tens= 5.0e2 i= 34 j= 27
pro fric=22 dil= 3 i= 34 j= 27

```

```

pro perm=5.00e-13 porosity=0.35 i= 34 j= 27
;END ORE ZONE

; Silt
pro dens= 1700 bulk=3.00e6 shear=7.5e6 i= 36 j= 31
pro coh= 3.0e3 tens= 1.0e3 i=36 j= 31
pro fric=25 dil= 5 i= 36 j= 31
pro perm=1.00e-13 porosity=0.4 i=36 j= 31
; Silt
pro dens= 1700 bulk=3.00e6 shear=7.5e6 i= 41 j= 45
pro coh= 3.0e3 tens= 1.0e4 i=41 j= 45
pro fric=25 dil= 5 i= 41 j= 45
pro perm=1.00e-13 porosity=0.4 i=41 j= 45

;ORE ZONE
; Silt / Mud
pro dens= 1750 bulk=8.0e5 shear=9.5e5 i= 31 j= 21
pro coh= 2.0e3 tens= 5.0e2 i= 31 j= 21
pro fric=22 dil= 3 i= 31 j= 21
pro perm=2.00e-14 porosity=0.35 i= 31 j= 21
; Shale
pro dens= 1800 bulk=3.01e6 shear=5.01e6 i=33 j=25
pro coh= 1.0e3 tens= 1.0e2 i=33 j=25
pro fric=20 dil= 2 i=33 j=25
pro perm=1.00e-12 porosity=0.3 i=33 j=25
;END ORE ZONE

;-----END OF PROPERTIES-----

def ini_stress
hh1 = 0.5*abs(y(1,2) - y(1,1))
surf_load = -2.0e3*9.8*2500
str_add = hh1*9.8*2700
bot_str = (-1.0)*(2.4e3*9.8*2500 - str_add)
top_str = (-1.0)*(2.0e3*9.8*2500 + str_add)

str_var = top_str - bot_str

command
ini sxx bot_str var=0,str_var i=1,80 j=1,80
ini syy bot_str var=0,str_var i=1,80 j=1,80
ini szz bot_str var=0,str_var i=1,80 j=1,80
ini sxy = 0.0
end_command

end
ini_stress

apply ns surf_load i=1,81 j=81

def hydro_pp

surf_pp = 2.5e3*9.8*1000 + 1e5 ;pp (2.0km) + pp (atmospheric loading)

loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
;sss2 = 0
sss2 = surf_pp

else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa + surf_pp
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
;
;
ini sat 1
fix sat

```

```

fix pp j=81
;
set gravity=9.8
;
set large
;
;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=40 j=40
hist 3 pp i=40 j=40

;Movie every 500 steps
plot pp fill
sav sm1b_100_ini.sav
movie on file sm1b_100.dcx step 500

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTLING
fix x i=1
fix x i=81
fix y j=1

; Gravity settling
STEP 1500

;Set fluid on run to equilibrium
set flow on
pl pp fi fl bl
STEP 1500

free x
free y

ini xvel -0.0008 var = 0.0016 ,0 i=1, 81 j=1, 81
fix x i=1
fix x i= 81
fix y j=1

sav sm1b_100_def.sav

step 5000
save sm1b_100_1.sav; 1%
step 5000
save sm1b_100_2.sav;
step 5000
save sm1b_100_3.sav;
step 5000
save sm1b_100_4.sav;
step 5000
save sm1b_100_5.sav; 5% deformation

return
stop

```

C.3 Model 2a

```

tit
Century Model 2 - Compression
;
config extra 9 gw
grid 80 80
gen 0.00e0,-2.90e3 0.00e0,-2.50e3 4.00e2,-2.50e3 4.00e2,-2.90e3 i=1,81 j=1,81
mark i=1
mark j=1
mark i = 81
mark j = 81
;
*****
model mohr
water bulk 2e9 dens 1000

```

```

prop poro=0.3 ; to be elaborated below
;; 1 mech step = 1 fluid step;
set nmech 1 ngw 1 flow off
*****
tab 1 0 ,-2675.03 205.11 ,-2675.03
;
tab 2 219.15 ,-2655.5 400 ,-2655.5
;
tab 3 0 ,-2771.87 155.99 ,-2771.87
;
tab 4 172.36 ,-2750.78 400 ,-2750.78
;
tab 5 0 ,-2821.85 131.03 ,-2821.85
;
tab 6 146.63 ,-2801.54 400 ,-2801.54
;
tab 7 0 ,-2789.05 148.19 ,-2789.05
;
tab 8 163 ,-2768.74 400 ,-2768.74
;
tab 9 0 ,-2797.64 143.51 ,-2797.64
;
tab 10 158.32 ,-2778.12 400 ,-2778.12
;
tab 11 154.43 ,-2786.71 400 ,-2786.71
;
tab 12 137.27 ,-2808.57 0 ,-2807.79
;
tab 13 291 ,-2500 91 ,-2900
;
tab 14 99 ,-2900 299 ,-2500
;
tab 15 60.85 ,-2500 117 ,-2852.31 123.24 ,-2839.03
tab 15 67.87 ,-2500
;
tab 16 139.61 ,-2500 180.16 ,-2727.35 186.4 ,-2714.86
tab 16 146.63 ,-2500
;
gen tab 1
gen tab 2
gen tab 3
gen tab 4
gen tab 5
gen tab 6
gen tab 7
gen tab 8
gen tab 9
gen tab 10
gen tab 11
gen tab 12
gen tab 13
gen tab 14
gen tab 15
gen tab 16
;
; Moving the gridpoints i=20 j=1 at base i=60 j=80 at top of fault to straighten it out
ini x add -4 i=20 j=1
ini x add 3 i=60 j=81

; Properties for each sub-regions:
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 21 , 62
pro coh=2.7e7 tens=2.00e6 reg= 21 , 62
pro fric=27 dil= 4 reg= 21 , 62
pro perm=1.00e-15 porosity=0.3 reg= 21 , 62
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 65 , 62
pro coh=2.7e7 tens=2.00e6 reg= 65 , 62
pro fric=27 dil= 4 reg= 65 , 62
pro perm=1.00e-15 porosity=0.3 reg= 65 , 62
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 8 , 36
pro coh=3.47e7 tens=2.00e6 reg= 8 , 36
pro fric=32 dil= 4 reg= 8 , 36

```


pro perm=1.00e-16 porosity=0.3 reg= 8 , 36
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 60 , 38
pro coh=3.47e7 tens=2.00e6 reg= 60 , 38
pro fric=32 dil= 4 reg= 60 , 38
pro perm=1.00e-16 porosity=0.3 reg= 60 , 38
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 11 , 8
pro coh=3.84e7 tens=8.00e5 reg= 11 , 8
pro fric=14 dil= 1 reg= 11 , 8
pro perm=1.00e-19 porosity=0.2 reg= 11 , 8
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 57 , 8
pro coh=3.84e7 tens=8.00e5 reg= 57 , 8
pro fric=14 dil= 1 reg= 57 , 8
pro perm=1.00e-19 porosity=0.2 reg= 57 , 8
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 5 , 24
pro coh=3.6e7 tens=8.00e5 reg= 5 , 24
pro fric=23 dil= 2 reg= 5 , 24
pro perm=5.00e-16 porosity=0.3 reg= 5 , 24
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 55 , 28
pro coh=3.6e7 tens=8.00e5 reg= 55 , 28
pro fric=23 dil= 2 reg= 55 , 28
pro perm=5.00e-16 porosity=0.3 reg= 55 , 28
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 3 , 21
pro coh=3.84e7 tens=8.00e5 reg= 3 , 21
pro fric=14 dil= 1 reg= 3 , 21
pro perm=1.00e-19 porosity=0.2 reg= 3 , 21
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 75 , 25
pro coh=3.84e7 tens=8.00e5 reg= 75 , 25
pro fric=14 dil= 1 reg= 75 , 25
pro perm=1.00e-19 porosity=0.2 reg= 75 , 25
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 12 , 19
pro coh=3.6e7 tens=8.00e5 reg= 12 , 19
pro fric=23 dil= 2 reg= 12 , 19
pro perm=5.00e-16 porosity=0.3 reg= 12 , 19
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 32 , 23
pro coh=3.6e7 tens=8.00e5 reg= 32 , 23
pro fric=23 dil= 2 reg= 32 , 23
pro perm=5.00e-16 porosity=0.3 reg= 32 , 23
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 reg= 5 , 17
pro coh=3.6e7 tens=8.00e5 reg= 5 , 17
pro fric=23 dil= 2 reg= 5 , 17
pro perm=1.00e-18 porosity=0.2 reg= 5 , 17
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 reg= 55 , 21
pro coh=3.6e7 tens=8.00e5 reg= 55 , 21
pro fric=23 dil= 2 reg= 55 , 21
pro perm=1.00e-18 porosity=0.2 reg= 55 , 21
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 27 , 36
pro coh=3.47e7 tens=2.00e6 reg= 27 , 36
pro fric=32 dil= 4 reg= 27 , 36
pro perm=1.00e-16 porosity=0.3 reg= 27 , 36
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 38 , 43
pro coh=3.47e7 tens=2.00e6 reg= 38 , 43
pro fric=32 dil= 4 reg= 38 , 43
pro perm=1.00e-16 porosity=0.3 reg= 38 , 43
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 24 , 24
pro coh=3.6e7 tens=8.00e5 reg= 24 , 24
pro fric=23 dil= 2 reg= 24 , 24
pro perm=5.00e-16 porosity=0.3 reg= 24 , 24
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 25 , 19
pro coh=3.6e7 tens=8.00e5 reg= 25 , 19
pro fric=23 dil= 2 reg= 25 , 19

pro perm=5.00e-16 porosity=0.3 reg= 25 , 19
 ; Shale
 pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 25 , 21
 pro coh=3.84e7 tens=8.00e5 reg= 25 , 21
 pro fric=14 dil= 1 reg= 25 , 21
 pro perm=1.00e-19 porosity=0.2 reg= 25 , 21
 ; Siltstone / Mudstone
 pro dens= 2600 bulk=1.0e10 shear=7.5e9 reg= 25 , 17
 pro coh=3.6e7 tens=8.00e5 reg= 25 , 17
 pro fric=23 dil= 2 reg= 25 , 17
 pro perm=1.00e-18 porosity=0.2 reg= 25 , 17
 ; Sandstone
 pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 4 , 56
 pro coh=2.7e7 tens=2.00e6 reg= 4 , 56
 pro fric=27 dil= 4 reg= 4 , 56
 pro perm=1.00e-15 porosity=0.3 reg= 4 , 56
 ; Sandstone
 pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 38 , 63
 pro coh=2.7e7 tens=2.00e6 reg= 38 , 63
 pro fric=27 dil= 4 reg= 38 , 63
 pro perm=1.00e-15 porosity=0.3 reg= 38 , 63
 ;
 ; Fault
 pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 14 , 79
 pro coh=8.00e5 tens=8.00e5 reg= 14 , 79
 pro fric=30 dil= 5 reg= 14 , 79
 pro perm=1.00e-14 porosity=0.3 reg= 14 , 79
 ; Fault
 pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 14 , 74
 pro coh=8.00e5 tens=8.00e5 reg= 14 , 74
 pro fric=30 dil= 5 reg= 14 , 74
 pro perm=1.00e-14 porosity=0.3 reg= 14 , 74
 ; Fault
 pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 15 , 68
 pro coh=8.00e5 tens=8.00e5 reg= 15 , 68
 pro fric=30 dil= 5 reg= 15 , 68
 pro perm=1.00e-14 porosity=0.3 reg= 15 , 68

 ; LEFT Fault
 pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 16 , 62
 pro coh=8.00e5 tens=8.00e5 reg= 16 , 62
 pro fric=30 dil= 5 reg= 16 , 62
 pro perm=1.00e-14 porosity=0.3 reg= 16 , 62
 ; Fault
 pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 17 , 56
 pro coh=8.00e5 tens=8.00e5 reg= 17 , 56
 pro fric=30 dil= 5 reg= 17 , 56
 pro perm=1.00e-14 porosity=0.3 reg= 17 , 56
 ; Fault
 pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 18 , 50
 pro coh=8.00e5 tens=8.00e5 reg= 18 , 50
 pro fric=30 dil= 5 reg= 18 , 50
 pro perm=1.00e-14 porosity=0.3 reg= 18 , 50
 ; Fault
 pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 19 , 44
 pro coh=8.00e5 tens=8.00e5 reg= 19 , 44
 pro fric=30 dil= 5 reg= 19 , 44
 pro perm=1.00e-14 porosity=0.3 reg= 19 , 44
 ; Fault
 pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 20 , 38
 pro coh=8.00e5 tens=8.00e5 reg= 20 , 38
 pro fric=30 dil= 5 reg= 20 , 38
 pro perm=1.00e-14 porosity=0.3 reg= 20 , 38
 ; Fault
 pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 21 , 32
 pro coh=8.00e5 tens=8.00e5 reg= 21 , 32
 pro fric=30 dil= 5 reg= 21 , 32
 pro perm=1.00e-14 porosity=0.3 reg= 21 , 32
 ; Fault
 pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 21 , 31
 pro coh=8.00e5 tens=8.00e5 reg= 21 , 31
 pro fric=30 dil= 5 reg= 21 , 31
 pro perm=1.00e-14 porosity=0.3 reg= 21 , 31
 ; Fault
 pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 22 , 25

```
pro coh=8.00e5 tens=8.00e5 reg= 22 , 25
pro fric=30 dil= 5 reg= 22 , 25
pro perm=1.00e-14 porosity=0.3 reg= 22 , 25
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 23 , 18
pro coh=8.00e5 tens=8.00e5 reg= 23 , 18
pro fric=30 dil= 5 reg= 23 , 18
pro perm=1.00e-14 porosity=0.3 reg= 23 , 18
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 23 , 16
pro coh=8.00e5 tens=8.00e5 reg= 23 , 16
pro fric=30 dil= 5 reg= 23 , 16
pro perm=1.00e-14 porosity=0.3 reg= 23 , 16

;MID Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 29 , 80
pro coh=8.00e5 tens=8.00e5 reg= 29 , 80
pro fric=30 dil= 5 reg= 29 , 80
pro perm=1.00e-14 porosity=0.3 reg= 29 , 80
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 30 , 74
pro coh=8.00e5 tens=8.00e5 reg= 30 , 74
pro fric=30 dil= 5 reg= 30 , 74
pro perm=1.00e-14 porosity=0.3 reg= 30 , 74
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 31 , 68
pro coh=8.00e5 tens=8.00e5 reg= 31 , 68
pro fric=30 dil= 5 reg= 31 , 68
pro perm=1.00e-14 porosity=0.3 reg= 31 , 68
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 33 , 61
pro coh=8.00e5 tens=8.00e5 reg= 33 , 61
pro fric=30 dil= 5 reg= 33 , 61
pro perm=1.00e-14 porosity=0.3 reg= 33 , 61
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 33 , 57
pro coh=8.00e5 tens=8.00e5 reg= 33 , 57
pro fric=30 dil= 5 reg= 33 , 57
pro perm=1.00e-14 porosity=0.3 reg= 33 , 57
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 34 , 53
pro coh=8.00e5 tens=8.00e5 reg= 34 , 53
pro fric=30 dil= 5 reg= 34 , 53
pro perm=1.00e-14 porosity=0.3 reg= 34 , 53
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 34 , 51
pro coh=8.00e5 tens=8.00e5 reg= 34 , 51
pro fric=30 dil= 5 reg= 34 , 51
pro perm=1.00e-14 porosity=0.3 reg= 34 , 51
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 35 , 47
pro coh=8.00e5 tens=8.00e5 reg= 35 , 47
pro fric=30 dil= 5 reg= 35 , 47
pro perm=1.00e-14 porosity=0.3 reg= 35 , 47
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 36 , 45
pro coh=8.00e5 tens=8.00e5 reg= 36 , 45
pro fric=30 dil= 5 reg= 36 , 45
pro perm=1.00e-14 porosity=0.3 reg= 36 , 45
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 36 , 43
pro coh=8.00e5 tens=8.00e5 reg= 36 , 43
pro fric=30 dil= 5 reg= 36 , 43
pro perm=1.00e-14 porosity=0.3 reg= 36 , 43
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 36 , 40
pro coh=8.00e5 tens=8.00e5 reg= 36 , 40
pro fric=30 dil= 5 reg= 36 , 40
pro perm=1.00e-14 porosity=0.3 reg= 36 , 40

; RIGHT Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 59 , 80
pro coh=8.00e5 tens=8.00e5 reg= 59 , 80
pro fric=30 dil= 5 reg= 59 , 80
pro perm=1.00e-14 porosity=0.3 reg= 59 , 80
```

```
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 59 , 79
pro coh=8.00e5 tens=8.00e5 reg= 59 , 79
pro fric=30 dil= 5 reg= 59 , 79
pro perm=1.00e-14 porosity=0.3 reg= 59 , 79
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 58 , 77
pro coh=8.00e5 tens=8.00e5 reg= 58 , 77
pro fric=30 dil= 5 reg= 58 , 77
pro perm=1.00e-14 porosity=0.3 reg= 58 , 77
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 57 , 75
pro coh=8.00e5 tens=8.00e5 reg= 57 , 75
pro fric=30 dil= 5 reg= 57 , 75
pro perm=1.00e-14 porosity=0.3 reg= 57 , 75
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 55 , 71
pro coh=8.00e5 tens=8.00e5 reg= 55 , 71
pro fric=30 dil= 5 reg= 55 , 71
pro perm=1.00e-14 porosity=0.3 reg= 55 , 71
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 56 , 73
pro coh=8.00e5 tens=8.00e5 reg= 56 , 73
pro fric=30 dil= 5 reg= 56 , 73
pro perm=1.00e-14 porosity=0.3 reg= 56 , 73
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 53 , 68
pro coh=8.00e5 tens=8.00e5 reg= 53 , 68
pro fric=30 dil= 5 reg= 53 , 68
pro perm=1.00e-14 porosity=0.3 reg= 53 , 68
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 52 , 66
pro coh=8.00e5 tens=8.00e5 reg= 52 , 66
pro fric=30 dil= 5 reg= 52 , 66
pro perm=1.00e-14 porosity=0.3 reg= 52 , 66
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 52 , 65
pro coh=8.00e5 tens=8.00e5 reg= 52 , 65
pro fric=30 dil= 5 reg= 52 , 65
pro perm=1.00e-14 porosity=0.3 reg= 52 , 65
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 50 , 61
pro coh=8.00e5 tens=8.00e5 reg= 50 , 61
pro fric=30 dil= 5 reg= 50 , 61
pro perm=1.00e-14 porosity=0.3 reg= 50 , 61
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 47 , 56
pro coh=8.00e5 tens=8.00e5 reg= 47 , 56
pro fric=30 dil= 5 reg= 47 , 56
pro perm=1.00e-14 porosity=0.3 reg= 47 , 56
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=51 j=62,63
pro coh=8.00e5 tens=8.00e5 i=51 j=62,63
pro fric=30 dil= 5 i=51 j=62,63
pro perm=1.00e-14 porosity=0.3 i=51 j=62,63
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=49 j=58,59
pro coh=8.00e5 tens=8.00e5 i=49 j=58,59
pro fric=30 dil= 5 i=49 j=58,59
pro perm=1.00e-14 porosity=0.3 i=49 j=58,59
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=50 j=62,63
pro coh=8.00e5 tens=8.00e5 i=50 j=62,63
pro fric=30 dil= 5 i=50 j=62,63
pro perm=1.00e-14 porosity=0.3 i=50 j=62,63
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=48 j=58,59
pro coh=8.00e5 tens=8.00e5 i=48 j=58,59
pro fric=30 dil= 5 i=48 j=58,59
pro perm=1.00e-14 porosity=0.3 i=48 j=58,59
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=47 j=54,55
pro coh=8.00e5 tens=8.00e5 i=47 j=54,55
pro fric=30 dil= 5 i=47 j=54,55
pro perm=1.00e-14 porosity=0.3 i=47 j=54,55
```

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=46 j=52,53
pro coh=8.00e5 tens=8.00e5 i=46 j=52,53
pro fric=30 dil= 5 i=46 j=52,53
pro perm=1.00e-14 porosity=0.3 i=46 j=52,53
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 45 , 51
pro coh=8.00e5 tens=8.00e5 reg= 45 , 51
pro fric=30 dil= 5 reg= 45 , 51
pro perm=1.00e-14 porosity=0.3 reg= 45 , 51
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 44 , 50
pro coh=8.00e5 tens=8.00e5 reg= 44 , 50
pro fric=30 dil= 5 reg= 44 , 50
pro perm=1.00e-14 porosity=0.3 reg= 44 , 50
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 44 , 49
pro coh=8.00e5 tens=8.00e5 reg= 44 , 49
pro fric=30 dil= 5 reg= 44 , 49
pro perm=1.00e-14 porosity=0.3 reg= 44 , 49
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 43 , 48
pro coh=8.00e5 tens=8.00e5 reg= 43 , 48
pro fric=30 dil= 5 reg= 43 , 48
pro perm=1.00e-14 porosity=0.3 reg= 43 , 48
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=46 j=54,55
pro coh=8.00e5 tens=8.00e5 i=46 j=54,55
pro fric=30 dil= 5 i=46 j=54,55
pro perm=1.00e-14 porosity=0.3 i=46 j=54,55
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=45 j=52,53
pro coh=8.00e5 tens=8.00e5 i=45 j=52,53
pro fric=30 dil= 5 i=45 j=52,53
pro perm=1.00e-14 porosity=0.3 i=45 j=52,53
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=43 j=46,47
pro coh=8.00e5 tens=8.00e5 i=43 j=46,47
pro fric=30 dil= 5 i=43 j=46,47
pro perm=1.00e-14 porosity=0.3 i=43 j=46,47
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=42 j=44,45
pro coh=8.00e5 tens=8.00e5 i=42 j=44,45
pro fric=30 dil= 5 i=42 j=44,45
pro perm=1.00e-14 porosity=0.3 i=42 j=44,45
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=41 j=42,43
pro coh=8.00e5 tens=8.00e5 i=41 j=42,43
pro fric=30 dil= 5 i=41 j=42,43
pro perm=1.00e-14 porosity=0.3 i=41 j=42,43
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=40 j=40,41
pro coh=8.00e5 tens=8.00e5 i=40 j=40,41
pro fric=30 dil= 5 i=40 j=40,41
pro perm=1.00e-14 porosity=0.3 i=40 j=40,41
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=42 j=46,47
pro coh=8.00e5 tens=8.00e5 i=42 j=46,47
pro fric=30 dil= 5 i=42 j=46,47
pro perm=1.00e-14 porosity=0.3 i=42 j=46,47
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 41 , 44
pro coh=8.00e5 tens=8.00e5 reg= 41 , 44
pro fric=30 dil= 5 reg= 41 , 44
pro perm=1.00e-14 porosity=0.3 reg= 41 , 44
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=40 j=42,43
pro coh=8.00e5 tens=8.00e5 i=40 j=42,43
pro fric=30 dil= 5 i=40 j=42,43
pro perm=1.00e-14 porosity=0.3 i=40 j=42,43
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=39 j=38,41
pro coh=8.00e5 tens=8.00e5 i=39 j=38,41
pro fric=30 dil= 5 i=39 j=38,41

pro perm=1.00e-14 porosity=0.3 i=39 j=38,41
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=38 j=38,39
pro coh=8.00e5 tens=8.00e5 i=38 j=38,39
pro fric=30 dil= 5 i=38 j=38,39
pro perm=1.00e-14 porosity=0.3 i=38 j=38,39
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=36,37 j=35
pro coh=8.00e5 tens=8.00e5 i=36,37 j=35
pro fric=30 dil= 5 i=36,37 j=35
pro perm=1.00e-14 porosity=0.3 i=36,37 j=35
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 37 , 34
pro coh=8.00e5 tens=8.00e5 reg= 37 , 34
pro fric=30 dil= 5 reg= 37 , 34
pro perm=1.00e-14 porosity=0.3 reg= 37 , 34
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 35 , 32
pro coh=8.00e5 tens=8.00e5 reg= 35 , 32
pro fric=30 dil= 5 reg= 35 , 32
pro perm=1.00e-14 porosity=0.3 reg= 35 , 32
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=35 j=30,31
pro coh=8.00e5 tens=8.00e5 i=35 j=30,31
pro fric=30 dil= 5 i=35 j=30,31
pro perm=1.00e-14 porosity=0.3 i=35 j=30,31
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=34 j=28,31
pro coh=8.00e5 tens=8.00e5 i=34 j=28,31
pro fric=30 dil= 5 i=34 j=28,31
pro perm=1.00e-14 porosity=0.3 i=34 j=28,31
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=33 j=26,29
pro coh=8.00e5 tens=8.00e5 i=33 j=26,29
pro fric=30 dil= 5 i=33 j=26,29
pro perm=1.00e-14 porosity=0.3 i=33 j=26,29
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=32 j=25,27
pro coh=8.00e5 tens=8.00e5 i=32 j=25,27
pro fric=30 dil= 5 i=32 j=25,27
pro perm=1.00e-14 porosity=0.3 i=32 j=25,27
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=31 j=24,25
pro coh=8.00e5 tens=8.00e5 i=31 j=24,25
pro fric=30 dil= 5 i=31 j=24,25
pro perm=1.00e-14 porosity=0.3 i=31 j=24,25
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=31 j=22,25
pro coh=8.00e5 tens=8.00e5 i=31 j=22,25
pro fric=30 dil= 5 i=31 j=22,25
pro perm=1.00e-14 porosity=0.3 i=31 j=22,25
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 29 , 20
pro coh=8.00e5 tens=8.00e5 reg= 29 , 20
pro fric=30 dil= 5 reg= 29 , 20
pro perm=1.00e-14 porosity=0.3 reg= 29 , 20
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=30 j=20,23
pro coh=8.00e5 tens=8.00e5 i=30 j=20,23
pro fric=30 dil= 5 i=30 j=20,23
pro perm=1.00e-14 porosity=0.3 i=30 j=20,23
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 28 , 18
pro coh=8.00e5 tens=8.00e5 reg= 28 , 18
pro fric=30 dil= 5 reg= 28 , 18
pro perm=1.00e-14 porosity=0.3 reg= 28 , 18
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 28 , 17
pro coh=8.00e5 tens=8.00e5 reg= 28 , 17
pro fric=30 dil= 5 reg= 28 , 17
pro perm=1.00e-14 porosity=0.3 reg= 28 , 17
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 26 , 13
pro coh=8.00e5 tens=8.00e5 reg= 26 , 13
pro fric=30 dil= 5 reg= 26 , 13

```

pro perm=1.00e-14 porosity=0.3 reg= 26 , 13
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 25 , 12
pro coh=8.00e5 tens=8.00e5 reg= 25 , 12
pro fric=30 dil= 5 reg= 25 , 12
pro perm=1.00e-14 porosity=0.3 reg= 25 , 12
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 26 , 15
pro coh=8.00e5 tens=8.00e5 reg= 26 , 15
pro fric=30 dil= 5 reg= 26 , 15
pro perm=1.00e-14 porosity=0.3 reg= 26 , 15
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 25 , 11
pro coh=8.00e5 tens=8.00e5 reg= 25 , 11
pro fric=30 dil= 5 reg= 25 , 11
pro perm=1.00e-14 porosity=0.3 reg= 25 , 11
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 24 , 10
pro coh=8.00e5 tens=8.00e5 reg= 24 , 10
pro fric=30 dil= 5 reg= 24 , 10
pro perm=1.00e-14 porosity=0.3 reg= 24 , 10
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 24 , 9
pro coh=8.00e5 tens=8.00e5 reg= 24 , 9
pro fric=30 dil= 5 reg= 24 , 9
pro perm=1.00e-14 porosity=0.3 reg= 24 , 9
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 23 , 7
pro coh=8.00e5 tens=8.00e5 reg= 23 , 7
pro fric=30 dil= 5 reg= 23 , 7
pro perm=1.00e-14 porosity=0.3 reg= 23 , 7
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 22 , 5
pro coh=8.00e5 tens=8.00e5 reg= 22 , 5
pro fric=30 dil= 5 reg= 22 , 5
pro perm=1.00e-14 porosity=0.3 reg= 22 , 5
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 21 , 3
pro coh=8.00e5 tens=8.00e5 reg= 21 , 3
pro fric=30 dil= 5 reg= 21 , 3
pro perm=1.00e-14 porosity=0.3 reg= 21 , 3
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 20 , 1
pro coh=8.00e5 tens=8.00e5 reg= 20 , 1
pro fric=30 dil= 5 reg= 20 , 1
pro perm=1.00e-14 porosity=0.3 reg= 20 , 1

; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 i=45 j=50
pro coh=2.7e7 tens=2.00e6 i=45 j=50
pro fric=27 dil= 4 i=45 j=50
pro perm=1.00e-15 porosity=0.3 i=45 j=50
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 i=58 j=80
pro coh=2.7e7 tens=2.00e6 i=58 j=80
pro fric=27 dil= 4 i=58 j=80
pro perm=1.00e-15 porosity=0.3 i=58 j=80
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=38 j=40,41
pro coh=3.47e7 tens=2.00e6 i=38 j=40,41
pro fric=32 dil= 4 i=38 j=40,41
pro perm=1.00e-16 porosity=0.3 i=38 j=40,41
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=41 j=45
pro coh=3.47e7 tens=2.00e6 i=41 j=45
pro fric=32 dil= 4 i=41 j=45
pro perm=1.00e-16 porosity=0.3 i=41 j=45
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=36 j=31
pro coh=3.47e7 tens=2.00e6 i=36 j=31
pro fric=32 dil= 4 i=36 j=31
pro perm=1.00e-16 porosity=0.3 i=36 j=31
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=20 j=45
pro coh=3.47e7 tens=2.00e6 i=20 j=45

```

```

pro fric=32 dil= 4 i=20 j=45
pro perm=1.00e-16 porosity=0.3 i=20 j=45
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 25 , j=14,16
pro coh=3.84e7 tens=8.00e5 i= 25 , j=14,16
pro fric=14 dil= 1 i= 25 , j=14,16
pro perm=1.00e-19 porosity=0.2 i= 25 , j=14,16
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 26 , j=16
pro coh=3.84e7 tens=8.00e5 i= 26 , j=16
pro fric=14 dil= 1 i= 26 , j=16
pro perm=1.00e-19 porosity=0.2 i= 26 , j=16
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 22 , j=21
pro coh=3.84e7 tens=8.00e5 i= 22 , j=21
pro fric=14 dil= 1 i= 22 , j=21
pro perm=1.00e-19 porosity=0.2 i= 22 , j=21
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 33 , j=25
pro coh=3.84e7 tens=8.00e5 i= 33 , j=25
pro fric=14 dil= 1 i= 33 , j=25
pro perm=1.00e-19 porosity=0.2 i= 33 , j=25
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 29 , j=22
pro coh=3.84e7 tens=8.00e5 i= 29 , j=22
pro fric=14 dil= 1 i= 29 , j=22
pro perm=1.00e-19 porosity=0.2 i= 29 , j=22
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 21 , j=1
pro coh=3.84e7 tens=8.00e5 i= 21 , j=1
pro fric=14 dil= 1 i= 21 , j=1
pro perm=1.00e-19 porosity=0.2 i= 21 , j=1
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 i=24,28 j=20
pro coh=3.6e7 tens=8.00e5 i=24,28 j=20
pro fric=23 dil= 2 i=24,28 j=20
pro perm=5.00e-16 porosity=0.3 i=24,28 j=20
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 i=34 , j=27
pro coh=3.6e7 tens=8.00e5 i=34 , j=27
pro fric=23 dil= 2 reg= i=34 , j=27
pro perm=5.00e-16 porosity=0.3 i=34 , j=27
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 i=31 , j=21
pro coh=3.6e7 tens=8.00e5 i=31 , j=21
pro fric=23 dil= 2 i=31 , j=21
pro perm=1.00e-18 porosity=0.2 i=31 , j=21
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 i=27 , j=18
pro coh=3.6e7 tens=8.00e5 i=27 , j=18
pro fric=23 dil= 2 i=27 , j=18
pro perm=1.00e-18 porosity=0.2 i=27 , j=18

```

```
;------END OF PROPERTIES-----
```

```

def ini_stress
hh1 = 0.5*abs(y(1,2) - y(1,1))
surf_load = -2.5e3*9.8*2500
str_add = hh1*9.8*2700
bot_str = (-1.0)*(2.9e3*9.8*2500 - str_add)
top_str = (-1.0)*(2.5e3*9.8*2500 + str_add)

```

```
str_var = top_str - bot_str
```

```

command
ini sxx bot_str var=0,str_var i=1,80 j=1,80
ini syy bot_str var=0,str_var i=1,80 j=1,80
ini szz bot_str var=0,str_var i=1,80 j=1,80
ini sxy = 0.0
end_command

```

```

end
ini_stress

```

```
apply ns surf_load i=1,81 j=81
```



```

def hydro_pp
surf_pp = 2.5e3*9.8*1000 + 1e5 ;pp (2.5km) + pp (atmospheric loading)
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
;sss2 = 0
sss2 = surf_pp
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa + surf_pp
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*

ini sat 1
fix sat

;fix pp j=81
set gravity=9.8
set large
;
;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=40 j=40
;hist 3 pp i=40 j=40

hist 3 pp i=10 j=18;sst/mud
hist 4 pp i=10 j=20;lower sst/sh
hist 5 pp i=10 j=22;shale
hist 6 pp i=10 j=26;higher sst/sh
hist 7 pp i=10 j=28;sst cap

;Movie every 500 steps
plot pp fill
sav m2a_ini.sav
movie on file m2a.dcx step 500

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTLING
fix x i=1
fix x i=81
fix y j=1

; Gravity settling
STEP 1500
;Set fluid on run to equilibrium
set flow on
pl pp fi fl bl
STEP 1500

free x
free y

;Compression
ini xvel 0.0008 var=-0.0016 ,0 i=1, 81 j=1, 81
fix x i=1
fix x i= 81
fix y j=1
;
step 2500
save m2a_1.sav ; 1 % compression
step 2500
save m2a_2.sav ; 2 % compression
step 2500
save m2a_3.sav ; 3 % compression
step 2500
save m2a_4.sav ; 4 % compression
step 2500
save m2a_5.sav ; 5 % compression
step 2500
save m2a_6.sav ; 6 % compression
step 2500

```

```

save m2a_7.sav ; 7 % compression
step 2500
save m2a_8.sav ; 8 % compression
step 2500
save m2a_9.sav ; 9 % compression
step 2500
save m2a_10.sav ; 10 % compression
step 2500
save m2a_11.sav ; 11 % compression
step 2500
save m2a_12.sav ; 12 % compression

return
stop

```

C.4 Model 2b

```

;
tit
Century Model 2 - Compression
;
config extra 9 gw
grid 80 80
gen 0.00e0,-2.90e3 0.00e0,-2.50e3 4.00e2,-2.50e3 4.00e2,-2.90e3 i=1,81 j=1,81
mark i=1
mark j=1
mark i = 81
mark j = 81
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3 ; to be elaborated below
;; 1 mech step = 1 fluid step; modify if necessary!!!
set nmech 1 ngw 1 flow off
*****

```

GEOMETRY AS PREVIOUS MODEL

```

; Properties for each sub-regions:
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 21 , 62
pro coh=2.7e7 tens=2.00e6 reg= 21 , 62
pro fric=27 dil= 4 reg= 21 , 62
pro perm=1.00e-19 porosity=0.3 reg= 21 , 62
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 65 , 62
pro coh=2.7e7 tens=2.00e6 reg= 65 , 62
pro fric=27 dil= 4 reg= 65 , 62
pro perm=1.00e-19 porosity=0.3 reg= 65 , 62
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 8 , 36
pro coh=3.47e7 tens=2.00e6 reg= 8 , 36
pro fric=32 dil= 4 reg= 8 , 36
pro perm=1.00e-16 porosity=0.3 reg= 8 , 36
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 60 , 38
pro coh=3.47e7 tens=2.00e6 reg= 60 , 38
pro fric=32 dil= 4 reg= 60 , 38
pro perm=1.00e-16 porosity=0.3 reg= 60 , 38
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 11 , 8
pro coh=3.84e7 tens=8.00e5 reg= 11 , 8
pro fric=14 dil= 1 reg= 11 , 8
pro perm=1.00e-19 porosity=0.2 reg= 11 , 8
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 57 , 8
pro coh=3.84e7 tens=8.00e5 reg= 57 , 8
pro fric=14 dil= 1 reg= 57 , 8
pro perm=1.00e-19 porosity=0.2 reg= 57 , 8
; Siltstone / Shale

```

pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 5 , 24
pro coh=3.6e7 tens=8.00e5 reg= 5 , 24
pro fric=23 dil= 2 reg= 5 , 24
pro perm=5.00e-16 porosity=0.3 reg= 5 , 24
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 55 , 28
pro coh=3.6e7 tens=8.00e5 reg= 55 , 28
pro fric=23 dil= 2 reg= 55 , 28
pro perm=5.00e-16 porosity=0.3 reg= 55 , 28
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 3 , 21
pro coh=3.84e7 tens=8.00e5 reg= 3 , 21
pro fric=14 dil= 1 reg= 3 , 21
pro perm=1.00e-19 porosity=0.2 reg= 3 , 21
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 75 , 25
pro coh=3.84e7 tens=8.00e5 reg= 75 , 25
pro fric=14 dil= 1 reg= 75 , 25
pro perm=1.00e-19 porosity=0.2 reg= 75 , 25
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 12 , 19
pro coh=3.6e7 tens=8.00e5 reg= 12 , 19
pro fric=23 dil= 2 reg= 12 , 19
pro perm=5.00e-16 porosity=0.3 reg= 12 , 19
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 32 , 23
pro coh=3.6e7 tens=8.00e5 reg= 32 , 23
pro fric=23 dil= 2 reg= 32 , 23
pro perm=5.00e-16 porosity=0.3 reg= 32 , 23
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 reg= 5 , 17
pro coh=3.6e7 tens=8.00e5 reg= 5 , 17
pro fric=23 dil= 2 reg= 5 , 17
pro perm=1.00e-18 porosity=0.2 reg= 5 , 17
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 reg= 55 , 21
pro coh=3.6e7 tens=8.00e5 reg= 55 , 21
pro fric=23 dil= 2 reg= 55 , 21
pro perm=1.00e-18 porosity=0.2 reg= 55 , 21
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 27 , 36
pro coh=3.47e7 tens=2.00e6 reg= 27 , 36
pro fric=32 dil= 4 reg= 27 , 36
pro perm=1.00e-16 porosity=0.3 reg= 27 , 36
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 38 , 43
pro coh=3.47e7 tens=2.00e6 reg= 38 , 43
pro fric=32 dil= 4 reg= 38 , 43
pro perm=1.00e-16 porosity=0.3 reg= 38 , 43
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 24 , 24
pro coh=3.6e7 tens=8.00e5 reg= 24 , 24
pro fric=23 dil= 2 reg= 24 , 24
pro perm=5.00e-16 porosity=0.3 reg= 24 , 24
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 25 , 19
pro coh=3.6e7 tens=8.00e5 reg= 25 , 19
pro fric=23 dil= 2 reg= 25 , 19
pro perm=5.00e-16 porosity=0.3 reg= 25 , 19
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 25 , 21
pro coh=3.84e7 tens=8.00e5 reg= 25 , 21
pro fric=14 dil= 1 reg= 25 , 21
pro perm=1.00e-19 porosity=0.2 reg= 25 , 21
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 reg= 25 , 17
pro coh=3.6e7 tens=8.00e5 reg= 25 , 17
pro fric=23 dil= 2 reg= 25 , 17
pro perm=1.00e-18 porosity=0.2 reg= 25 , 17
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 4 , 56
pro coh=2.7e7 tens=2.00e6 reg= 4 , 56
pro fric=27 dil= 4 reg= 4 , 56
pro perm=1.00e-19 porosity=0.3 reg= 4 , 56
; Sandstone

pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 38 , 63
pro coh=2.7e7 tens=2.00e6 reg= 38 , 63
pro fric=27 dil= 4 reg= 38 , 63
pro perm=1.00e-19 porosity=0.3 reg= 38 , 63
;
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 14 , 79
pro coh=8.00e5 tens=8.00e5 reg= 14 , 79
pro fric=30 dil= 5 reg= 14 , 79
pro perm=1.00e-14 porosity=0.3 reg= 14 , 79
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 14 , 74
pro coh=8.00e5 tens=8.00e5 reg= 14 , 74
pro fric=30 dil= 5 reg= 14 , 74
pro perm=1.00e-14 porosity=0.3 reg= 14 , 74
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 15 , 68
pro coh=8.00e5 tens=8.00e5 reg= 15 , 68
pro fric=30 dil= 5 reg= 15 , 68
pro perm=1.00e-14 porosity=0.3 reg= 15 , 68

; LEFT Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 16 , 62
pro coh=8.00e5 tens=8.00e5 reg= 16 , 62
pro fric=30 dil= 5 reg= 16 , 62
pro perm=1.00e-14 porosity=0.3 reg= 16 , 62
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 17 , 56
pro coh=8.00e5 tens=8.00e5 reg= 17 , 56
pro fric=30 dil= 5 reg= 17 , 56
pro perm=1.00e-14 porosity=0.3 reg= 17 , 56
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 18 , 50
pro coh=8.00e5 tens=8.00e5 reg= 18 , 50
pro fric=30 dil= 5 reg= 18 , 50
pro perm=1.00e-14 porosity=0.3 reg= 18 , 50
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 19 , 44
pro coh=8.00e5 tens=8.00e5 reg= 19 , 44
pro fric=30 dil= 5 reg= 19 , 44
pro perm=1.00e-14 porosity=0.3 reg= 19 , 44
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 20 , 38
pro coh=8.00e5 tens=8.00e5 reg= 20 , 38
pro fric=30 dil= 5 reg= 20 , 38
pro perm=1.00e-14 porosity=0.3 reg= 20 , 38
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 21 , 32
pro coh=8.00e5 tens=8.00e5 reg= 21 , 32
pro fric=30 dil= 5 reg= 21 , 32
pro perm=1.00e-14 porosity=0.3 reg= 21 , 32
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 21 , 31
pro coh=8.00e5 tens=8.00e5 reg= 21 , 31
pro fric=30 dil= 5 reg= 21 , 31
pro perm=1.00e-14 porosity=0.3 reg= 21 , 31
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 22 , 25
pro coh=8.00e5 tens=8.00e5 reg= 22 , 25
pro fric=30 dil= 5 reg= 22 , 25
pro perm=1.00e-14 porosity=0.3 reg= 22 , 25
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 23 , 18
pro coh=8.00e5 tens=8.00e5 reg= 23 , 18
pro fric=30 dil= 5 reg= 23 , 18
pro perm=1.00e-14 porosity=0.3 reg= 23 , 18
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 23 , 16
pro coh=8.00e5 tens=8.00e5 reg= 23 , 16
pro fric=30 dil= 5 reg= 23 , 16
pro perm=1.00e-14 porosity=0.3 reg= 23 , 16

;MID Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 29 , 80
pro coh=8.00e5 tens=8.00e5 reg= 29 , 80

pro fric=30 dil= 5 reg= 29 , 80
pro perm=1.00e-14 porosity=0.3 reg= 29 , 80
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 30 , 74
pro coh=8.00e5 tens=8.00e5 reg= 30 , 74
pro fric=30 dil= 5 reg= 30 , 74
pro perm=1.00e-14 porosity=0.3 reg= 30 , 74
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 31 , 68
pro coh=8.00e5 tens=8.00e5 reg= 31 , 68
pro fric=30 dil= 5 reg= 31 , 68
pro perm=1.00e-14 porosity=0.3 reg= 31 , 68
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 33 , 61
pro coh=8.00e5 tens=8.00e5 reg= 33 , 61
pro fric=30 dil= 5 reg= 33 , 61
pro perm=1.00e-14 porosity=0.3 reg= 33 , 61
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 33 , 57
pro coh=8.00e5 tens=8.00e5 reg= 33 , 57
pro fric=30 dil= 5 reg= 33 , 57
pro perm=1.00e-14 porosity=0.3 reg= 33 , 57
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 34 , 53
pro coh=8.00e5 tens=8.00e5 reg= 34 , 53
pro fric=30 dil= 5 reg= 34 , 53
pro perm=1.00e-14 porosity=0.3 reg= 34 , 53
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 34 , 51
pro coh=8.00e5 tens=8.00e5 reg= 34 , 51
pro fric=30 dil= 5 reg= 34 , 51
pro perm=1.00e-14 porosity=0.3 reg= 34 , 51
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 35 , 47
pro coh=8.00e5 tens=8.00e5 reg= 35 , 47
pro fric=30 dil= 5 reg= 35 , 47
pro perm=1.00e-14 porosity=0.3 reg= 35 , 47
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 36 , 45
pro coh=8.00e5 tens=8.00e5 reg= 36 , 45
pro fric=30 dil= 5 reg= 36 , 45
pro perm=1.00e-14 porosity=0.3 reg= 36 , 45
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 36 , 43
pro coh=8.00e5 tens=8.00e5 reg= 36 , 43
pro fric=30 dil= 5 reg= 36 , 43
pro perm=1.00e-14 porosity=0.3 reg= 36 , 43
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 36 , 40
pro coh=8.00e5 tens=8.00e5 reg= 36 , 40
pro fric=30 dil= 5 reg= 36 , 40
pro perm=1.00e-14 porosity=0.3 reg= 36 , 40

; RIGHT Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 59 , 80
pro coh=8.00e5 tens=8.00e5 reg= 59 , 80
pro fric=30 dil= 5 reg= 59 , 80
pro perm=1.00e-14 porosity=0.3 reg= 59 , 80
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 59 , 79
pro coh=8.00e5 tens=8.00e5 reg= 59 , 79
pro fric=30 dil= 5 reg= 59 , 79
pro perm=1.00e-14 porosity=0.3 reg= 59 , 79
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 58 , 77
pro coh=8.00e5 tens=8.00e5 reg= 58 , 77
pro fric=30 dil= 5 reg= 58 , 77
pro perm=1.00e-14 porosity=0.3 reg= 58 , 77
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 57 , 75
pro coh=8.00e5 tens=8.00e5 reg= 57 , 75
pro fric=30 dil= 5 reg= 57 , 75
pro perm=1.00e-14 porosity=0.3 reg= 57 , 75
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 55 , 71

pro coh=8.00e5 tens=8.00e5 reg= 55 , 71
pro fric=30 dil= 5 reg= 55 , 71
pro perm=1.00e-14 porosity=0.3 reg= 55 , 71
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 56 , 73
pro coh=8.00e5 tens=8.00e5 reg= 56 , 73
pro fric=30 dil= 5 reg= 56 , 73
pro perm=1.00e-14 porosity=0.3 reg= 56 , 73
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 53 , 68
pro coh=8.00e5 tens=8.00e5 reg= 53 , 68
pro fric=30 dil= 5 reg= 53 , 68
pro perm=1.00e-14 porosity=0.3 reg= 53 , 68
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 52 , 66
pro coh=8.00e5 tens=8.00e5 reg= 52 , 66
pro fric=30 dil= 5 reg= 52 , 66
pro perm=1.00e-14 porosity=0.3 reg= 52 , 66
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 52 , 65
pro coh=8.00e5 tens=8.00e5 reg= 52 , 65
pro fric=30 dil= 5 reg= 52 , 65
pro perm=1.00e-14 porosity=0.3 reg= 52 , 65
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 50 , 61
pro coh=8.00e5 tens=8.00e5 reg= 50 , 61
pro fric=30 dil= 5 reg= 50 , 61
pro perm=1.00e-14 porosity=0.3 reg= 50 , 61
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 47 , 56
pro coh=8.00e5 tens=8.00e5 reg= 47 , 56
pro fric=30 dil= 5 reg= 47 , 56
pro perm=1.00e-14 porosity=0.3 reg= 47 , 56
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=51 j=62,63
pro coh=8.00e5 tens=8.00e5 i=51 j=62,63
pro fric=30 dil= 5 i=51 j=62,63
pro perm=1.00e-14 porosity=0.3 i=51 j=62,63
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=49 j=58,59
pro coh=8.00e5 tens=8.00e5 i=49 j=58,59
pro fric=30 dil= 5 i=49 j=58,59
pro perm=1.00e-14 porosity=0.3 i=49 j=58,59
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=50 j=62,63
pro coh=8.00e5 tens=8.00e5 i=50 j=62,63
pro fric=30 dil= 5 i=50 j=62,63
pro perm=1.00e-14 porosity=0.3 i=50 j=62,63
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=48 j=58,59
pro coh=8.00e5 tens=8.00e5 i=48 j=58,59
pro fric=30 dil= 5 i=48 j=58,59
pro perm=1.00e-14 porosity=0.3 i=48 j=58,59
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=47 j=54,55
pro coh=8.00e5 tens=8.00e5 i=47 j=54,55
pro fric=30 dil= 5 i=47 j=54,55
pro perm=1.00e-14 porosity=0.3 i=47 j=54,55
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=46 j=52,53
pro coh=8.00e5 tens=8.00e5 i=46 j=52,53
pro fric=30 dil= 5 i=46 j=52,53
pro perm=1.00e-14 porosity=0.3 i=46 j=52,53
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 45 , 51
pro coh=8.00e5 tens=8.00e5 reg= 45 , 51
pro fric=30 dil= 5 reg= 45 , 51
pro perm=1.00e-14 porosity=0.3 reg= 45 , 51
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 44 , 50
pro coh=8.00e5 tens=8.00e5 reg= 44 , 50
pro fric=30 dil= 5 reg= 44 , 50
pro perm=1.00e-14 porosity=0.3 reg= 44 , 50
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 44 , 49

pro coh=8.00e5 tens=8.00e5 reg= 44 , 49
pro fric=30 dil= 5 reg= 44 , 49
pro perm=1.00e-14 porosity=0.3 reg= 44 , 49
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 43 , 48
pro coh=8.00e5 tens=8.00e5 reg= 43 , 48
pro fric=30 dil= 5 reg= 43 , 48
pro perm=1.00e-14 porosity=0.3 reg= 43 , 48
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=46 j=54,55
pro coh=8.00e5 tens=8.00e5 i=46 j=54,55
pro fric=30 dil= 5 i=46 j=54,55
pro perm=1.00e-14 porosity=0.3 i=46 j=54,55
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=45 j=52,53
pro coh=8.00e5 tens=8.00e5 i=45 j=52,53
pro fric=30 dil= 5 i=45 j=52,53
pro perm=1.00e-14 porosity=0.3 i=45 j=52,53
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=43 j=46,47
pro coh=8.00e5 tens=8.00e5 i=43 j=46,47
pro fric=30 dil= 5 i=43 j=46,47
pro perm=1.00e-14 porosity=0.3 i=43 j=46,47
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=42 j=44,45
pro coh=8.00e5 tens=8.00e5 i=42 j=44,45
pro fric=30 dil= 5 i=42 j=44,45
pro perm=1.00e-14 porosity=0.3 i=42 j=44,45
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=41 j=42,43
pro coh=8.00e5 tens=8.00e5 i=41 j=42,43
pro fric=30 dil= 5 i=41 j=42,43
pro perm=1.00e-14 porosity=0.3 i=41 j=42,43
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=40 j=40,41
pro coh=8.00e5 tens=8.00e5 i=40 j=40,41
pro fric=30 dil= 5 i=40 j=40,41
pro perm=1.00e-14 porosity=0.3 i=40 j=40,41
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=42 j=46,47
pro coh=8.00e5 tens=8.00e5 i=42 j=46,47
pro fric=30 dil= 5 i=42 j=46,47
pro perm=1.00e-14 porosity=0.3 i=42 j=46,47
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 41 , 44
pro coh=8.00e5 tens=8.00e5 reg= 41 , 44
pro fric=30 dil= 5 reg= 41 , 44
pro perm=1.00e-14 porosity=0.3 reg= 41 , 44
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=40 j=42,43
pro coh=8.00e5 tens=8.00e5 i=40 j=42,43
pro fric=30 dil= 5 i=40 j=42,43
pro perm=1.00e-14 porosity=0.3 i=40 j=42,43
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=39 j=38,41
pro coh=8.00e5 tens=8.00e5 i=39 j=38,41
pro fric=30 dil= 5 i=39 j=38,41
pro perm=1.00e-14 porosity=0.3 i=39 j=38,41
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=38 j=38,39
pro coh=8.00e5 tens=8.00e5 i=38 j=38,39
pro fric=30 dil= 5 i=38 j=38,39
pro perm=1.00e-14 porosity=0.3 i=38 j=38,39
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=36,37 j=35
pro coh=8.00e5 tens=8.00e5 i=36,37 j=35
pro fric=30 dil= 5 i=36,37 j=35
pro perm=1.00e-14 porosity=0.3 i=36,37 j=35
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 37 , 34
pro coh=8.00e5 tens=8.00e5 reg= 37 , 34
pro fric=30 dil= 5 reg= 37 , 34
pro perm=1.00e-14 porosity=0.3 reg= 37 , 34
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 35 , 32

pro coh=8.00e5 tens=8.00e5 reg= 35 , 32
pro fric=30 dil= 5 reg= 35 , 32
pro perm=1.00e-14 porosity=0.3 reg= 35 , 32
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=35 j=30,31
pro coh=8.00e5 tens=8.00e5 i=35 j=30,31
pro fric=30 dil= 5 i=35 j=30,31
pro perm=1.00e-14 porosity=0.3 i=35 j=30,31
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=34 j=28,31
pro coh=8.00e5 tens=8.00e5 i=34 j=28,31
pro fric=30 dil= 5 i=34 j=28,31
pro perm=1.00e-14 porosity=0.3 i=34 j=28,31
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=33 j=26,29
pro coh=8.00e5 tens=8.00e5 i=33 j=26,29
pro fric=30 dil= 5 i=33 j=26,29
pro perm=1.00e-14 porosity=0.3 i=33 j=26,29
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=32 j=25,27
pro coh=8.00e5 tens=8.00e5 i=32 j=25,27
pro fric=30 dil= 5 i=32 j=25,27
pro perm=1.00e-14 porosity=0.3 i=32 j=25,27
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=31 j=24,25
pro coh=8.00e5 tens=8.00e5 i=31 j=24,25
pro fric=30 dil= 5 i=31 j=24,25
pro perm=1.00e-14 porosity=0.3 i=31 j=24,25
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=31 j=22,25
pro coh=8.00e5 tens=8.00e5 i=31 j=22,25
pro fric=30 dil= 5 i=31 j=22,25
pro perm=1.00e-14 porosity=0.3 i=31 j=22,25
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 29 , 20
pro coh=8.00e5 tens=8.00e5 reg= 29 , 20
pro fric=30 dil= 5 reg= 29 , 20
pro perm=1.00e-14 porosity=0.3 reg= 29 , 20
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=30 j=20,23
pro coh=8.00e5 tens=8.00e5 i=30 j=20,23
pro fric=30 dil= 5 i=30 j=20,23
pro perm=1.00e-14 porosity=0.3 i=30 j=20,23
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 28 , 18
pro coh=8.00e5 tens=8.00e5 reg= 28 , 18
pro fric=30 dil= 5 reg= 28 , 18
pro perm=1.00e-14 porosity=0.3 reg= 28 , 18
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 28 , 17
pro coh=8.00e5 tens=8.00e5 reg= 28 , 17
pro fric=30 dil= 5 reg= 28 , 17
pro perm=1.00e-14 porosity=0.3 reg= 28 , 17
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 26 , 13
pro coh=8.00e5 tens=8.00e5 reg= 26 , 13
pro fric=30 dil= 5 reg= 26 , 13
pro perm=1.00e-14 porosity=0.3 reg= 26 , 13
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 25 , 12
pro coh=8.00e5 tens=8.00e5 reg= 25 , 12
pro fric=30 dil= 5 reg= 25 , 12
pro perm=1.00e-14 porosity=0.3 reg= 25 , 12
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 26 , 15
pro coh=8.00e5 tens=8.00e5 reg= 26 , 15
pro fric=30 dil= 5 reg= 26 , 15
pro perm=1.00e-14 porosity=0.3 reg= 26 , 15
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 25 , 11
pro coh=8.00e5 tens=8.00e5 reg= 25 , 11
pro fric=30 dil= 5 reg= 25 , 11
pro perm=1.00e-14 porosity=0.3 reg= 25 , 11
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 24 , 10


```

pro coh=8.00e5 tens=8.00e5 reg= 24 , 10
pro fric=30 dil= 5 reg= 24 , 10
pro perm=1.00e-14 porosity=0.3 reg= 24 , 10
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 24 , 9
pro coh=8.00e5 tens=8.00e5 reg= 24 , 9
pro fric=30 dil= 5 reg= 24 , 9
pro perm=1.00e-14 porosity=0.3 reg= 24 , 9
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 23 , 7
pro coh=8.00e5 tens=8.00e5 reg= 23 , 7
pro fric=30 dil= 5 reg= 23 , 7
pro perm=1.00e-14 porosity=0.3 reg= 23 , 7
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 22 , 5
pro coh=8.00e5 tens=8.00e5 reg= 22 , 5
pro fric=30 dil= 5 reg= 22 , 5
pro perm=1.00e-14 porosity=0.3 reg= 22 , 5
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 21 , 3
pro coh=8.00e5 tens=8.00e5 reg= 21 , 3
pro fric=30 dil= 5 reg= 21 , 3
pro perm=1.00e-14 porosity=0.3 reg= 21 , 3
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 20 , 1
pro coh=8.00e5 tens=8.00e5 reg= 20 , 1
pro fric=30 dil= 5 reg= 20 , 1
pro perm=1.00e-14 porosity=0.3 reg= 20 , 1

; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 i=45 j=50
pro coh=2.7e7 tens=2.00e6 i=45 j=50
pro fric=27 dil= 4 i=45 j=50
pro perm=1.00e-19 porosity=0.3 i=45 j=50
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 i=58 j=80
pro coh=2.7e7 tens=2.00e6 i=58 j=80
pro fric=27 dil= 4 i=58 j=80
pro perm=1.00e-19 porosity=0.3 i=58 j=80
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=38 j=40,41
pro coh=3.47e7 tens=2.00e6 i=38 j=40,41
pro fric=32 dil= 4 i=38 j=40,41
pro perm=1.00e-16 porosity=0.3 i=38 j=40,41
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=41 j=45
pro coh=3.47e7 tens=2.00e6 i=41 j=45
pro fric=32 dil= 4 i=41 j=45
pro perm=1.00e-16 porosity=0.3 i=41 j=45
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=36 j=31
pro coh=3.47e7 tens=2.00e6 i=36 j=31
pro fric=32 dil= 4 i=36 j=31
pro perm=1.00e-16 porosity=0.3 i=36 j=31
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=20 j=45
pro coh=3.47e7 tens=2.00e6 i=20 j=45
pro fric=32 dil= 4 i=20 j=45
pro perm=1.00e-16 porosity=0.3 i=20 j=45
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 25 , j=14,16
pro coh=3.84e7 tens=8.00e5 i= 25 , j=14,16
pro fric=14 dil= 1 i= 25 , j=14,16
pro perm=1.00e-19 porosity=0.2 i= 25 , j=14,16
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 26 , j=16
pro coh=3.84e7 tens=8.00e5 i= 26 , j=16
pro fric=14 dil= 1 i= 26 , j=16
pro perm=1.00e-19 porosity=0.2 i= 26 , j=16
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 22 , j=21
pro coh=3.84e7 tens=8.00e5 i= 22 , j=21
pro fric=14 dil= 1 i= 22 , j=21
pro perm=1.00e-19 porosity=0.2 i= 22 , j=21
; Shale

```

```

pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 33 , j=25
pro coh=3.84e7 tens=8.00e5 i= 33 , j=25
pro fric=14 dil= 1 i= 33 , j=25
pro perm=1.00e-19 porosity=0.2 i= 33 , j=25
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 29 , j=22
pro coh=3.84e7 tens=8.00e5 i= 29 , j=22
pro fric=14 dil= 1 i= 29 , j=22
pro perm=1.00e-19 porosity=0.2 i= 29 , j=22
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 21 , j=1
pro coh=3.84e7 tens=8.00e5 i= 21 , j=1
pro fric=14 dil= 1 i= 21 , j=1
pro perm=1.00e-19 porosity=0.2 i= 21 , j=1
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 i=24,28 j=20
pro coh=3.6e7 tens=8.00e5 i=24,28 j=20
pro fric=23 dil= 2 i=24,28 j=20
pro perm=5.00e-16 porosity=0.3 i=24,28 j=20
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 i=34 , j=27
pro coh=3.6e7 tens=8.00e5 i=34 , j=27
pro fric=23 dil= 2 reg= i=34 , j=27
pro perm=5.00e-16 porosity=0.3 i=34 , j=27
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 i=31 , j=21
pro coh=3.6e7 tens=8.00e5 i=31 , j=21
pro fric=23 dil= 2 i=31 , j=21
pro perm=1.00e-18 porosity=0.2 i=31 , j=21
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 i=27 , j=18
pro coh=3.6e7 tens=8.00e5 i=27 , j=18
pro fric=23 dil= 2 i=27 , j=18
pro perm=1.00e-18 porosity=0.2 i=27 , j=18
;-----END OF PROPERTIES-----

def ini_stress
hh1 = 0.5*abs(y(1,2) - y(1,1))
surf_load = -2.5e3*9.8*2500
str_add = hh1*9.8*2700
bot_str = (-1.0)*(2.9e3*9.8*2500 - str_add)
top_str = (-1.0)*(2.5e3*9.8*2500 + str_add)

str_var = top_str - bot_str

command
ini sxx bot_str var=0,str_var i=1,80 j=1,80
ini syy bot_str var=0,str_var i=1,80 j=1,80
ini szz bot_str var=0,str_var i=1,80 j=1,80
ini sxy = 0.0
end_command

end
ini_stress

apply ns surf_load i=1,81 j=81
def hydro_pp
surf_pp = 2.5e3*9.8*1000 + 1e5 ;pp (2.5km) + pp (atmospheric loading)
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
;sss2 = 0
sss2 = surf_pp
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa + surf_pp
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
;

```

```

;
ini sat 1
fix sat

;fix pp j=81
;
set gravity=9.8
;
set large
;
;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=40 j=40
;hist 3 pp i=40 j=40

hist 3 pp i=10 j=18;sst/mud
hist 4 pp i=10 j=20;lower sst/sh
hist 5 pp i=10 j=22;shale
hist 6 pp i=10 j=26;higher sst/sh
hist 7 pp i=10 j=28;sst cap

;Movie every 500 steps
plot pp fill
sav m2b_ini.sav
movie on file m2b.dcx step 500

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTLING
fix x i=1
fix x i=81
fix y j=1

; Gravity settling
STEP 1500

;Set fluid on run to equilibrium
set flow on
pl pp fi fl bl
STEP 1500

;***Fish function to set overpressure from j=45 to j=1****
def overpress_pp
surf_pp = 3.0e3*9.8*2700 + 1e5 ;pp (3km) + pp (atmospheric loading)
loop i (1,igp)
loop j (1,45)
if j < 45 Then
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 2700 * 9.8 * aaa + surf_pp
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
overpress_pp
*
;
sav m2b_overpress.sav

free x
free y

;Compression
ini xvel 0.0008 var=-0.0016 ,0 i=1, 81 j=1, 81
fix x i=1
fix x i= 81
fix y j=1
;

step 2500
save m2b_1.sav ; 1 % compression
step 2500
save m2b_2.sav ; 2 % compression
step 2500
save m2b_3.sav ; 3 % compression
step 2500

```

```

save m2b_4.sav ; 4 % compression
step 2500
save m2b_5.sav ; 5 % compression
step 2500
save m2b_6.sav ; 6 % compression
step 2500
save m2b_7.sav ; 7 % compression
step 2500
save m2b_8.sav ; 8 % compression
step 2500
save m2b_9.sav ; 9 % compression
step 2500
save m2b_10.sav ; 10 % compression

return
stop

```

C.5 Model 2c

```

;
tit
Century Model 2 - Compression
;
config extra 9 gw
grid 80 80
gen 0.00e0,-2.90e3 0.00e0,-2.50e3 4.00e2,-2.50e3 4.00e2,-2.90e3 i=1,81 j=1,81
mark i=1
mark j=1
mark i = 81
mark j = 81
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3 ; to be elaborated below
;; 1 mech step = 1 fluid step; modify if necessary!!!
set nmech 1 ngw 1 flow off
*****

```

GEOMETRY AS PREVIOUS MODEL

```

; Properties for each sub-regions:
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 21 , 62
pro coh=2.7e7 tens=2.00e6 reg= 21 , 62
pro fric=27 dil= 4 reg= 21 , 62
pro perm=1.00e-19 porosity=0.3 reg= 21 , 62
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 65 , 62
pro coh=2.7e7 tens=2.00e6 reg= 65 , 62
pro fric=27 dil= 4 reg= 65 , 62
pro perm=1.00e-19 porosity=0.3 reg= 65 , 62
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 8 , 36
pro coh=3.47e7 tens=2.00e6 reg= 8 , 36
pro fric=32 dil= 4 reg= 8 , 36
pro perm=1.00e-16 porosity=0.3 reg= 8 , 36
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 60 , 38
pro coh=3.47e7 tens=2.00e6 reg= 60 , 38
pro fric=32 dil= 4 reg= 60 , 38
pro perm=1.00e-16 porosity=0.3 reg= 60 , 38
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 11 , 8
pro coh=3.84e7 tens=8.00e5 reg= 11 , 8
pro fric=14 dil= 1 reg= 11 , 8
pro perm=1.00e-19 porosity=0.2 reg= 11 , 8
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 57 , 8
pro coh=3.84e7 tens=8.00e5 reg= 57 , 8
pro fric=14 dil= 1 reg= 57 , 8

```

pro perm=1.00e-19 porosity=0.2 reg= 57 , 8
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 5 , 24
pro coh=3.6e7 tens=8.00e5 reg= 5 , 24
pro fric=23 dil= 2 reg= 5 , 24
pro perm=5.00e-16 porosity=0.3 reg= 5 , 24
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 55 , 28
pro coh=3.6e7 tens=8.00e5 reg= 55 , 28
pro fric=23 dil= 2 reg= 55 , 28
pro perm=5.00e-16 porosity=0.3 reg= 55 , 28
; Shale (ore zone)
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 3 , 21
pro coh=3.84e7 tens=8.00e5 reg= 3 , 21
pro fric=14 dil= 5 reg= 3 , 21
pro perm=5.00e-15 porosity=0.2 reg= 3 , 21
; Shale (ore zone)
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 75 , 25
pro coh=3.84e7 tens=8.00e5 reg= 75 , 25
pro fric=14 dil= 5 reg= 75 , 25
pro perm=5.00e-15 porosity=0.2 reg= 75 , 25
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 12 , 19
pro coh=3.6e7 tens=8.00e5 reg= 12 , 19
pro fric=23 dil= 2 reg= 12 , 19
pro perm=5.00e-16 porosity=0.3 reg= 12 , 19
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 32 , 23
pro coh=3.6e7 tens=8.00e5 reg= 32 , 23
pro fric=23 dil= 2 reg= 32 , 23
pro perm=5.00e-16 porosity=0.3 reg= 32 , 23
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 reg= 5 , 17
pro coh=3.6e7 tens=8.00e5 reg= 5 , 17
pro fric=23 dil= 2 reg= 5 , 17
pro perm=1.00e-18 porosity=0.2 reg= 5 , 17
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 reg= 55 , 21
pro coh=3.6e7 tens=8.00e5 reg= 55 , 21
pro fric=23 dil= 2 reg= 55 , 21
pro perm=1.00e-18 porosity=0.2 reg= 55 , 21

; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 27 , 36
pro coh=3.47e7 tens=2.00e6 reg= 27 , 36
pro fric=32 dil= 4 reg= 27 , 36
pro perm=1.00e-16 porosity=0.3 reg= 27 , 36
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 38 , 43
pro coh=3.47e7 tens=2.00e6 reg= 38 , 43
pro fric=32 dil= 4 reg= 38 , 43
pro perm=1.00e-16 porosity=0.3 reg= 38 , 43
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 24 , 24
pro coh=3.6e7 tens=8.00e5 reg= 24 , 24
pro fric=23 dil= 2 reg= 24 , 24
pro perm=5.00e-16 porosity=0.3 reg= 24 , 24
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 25 , 19
pro coh=3.6e7 tens=8.00e5 reg= 25 , 19
pro fric=23 dil= 2 reg= 25 , 19
pro perm=5.00e-16 porosity=0.3 reg= 25 , 19
; Shale (ore zone)
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 25 , 21
pro coh=3.84e7 tens=8.00e5 reg= 25 , 21
pro fric=14 dil= 5 reg= 25 , 21
pro perm=5.00e-15 porosity=0.2 reg= 25 , 21
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 reg= 25 , 17
pro coh=3.6e7 tens=8.00e5 reg= 25 , 17
pro fric=23 dil= 2 reg= 25 , 17
pro perm=1.00e-18 porosity=0.2 reg= 25 , 17
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 4 , 56
pro coh=2.7e7 tens=2.00e6 reg= 4 , 56

pro fric=27 dil= 4 reg= 4 , 56
pro perm=1.00e-19 porosity=0.3 reg= 4 , 56
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 38 , 63
pro coh=2.7e7 tens=2.00e6 reg= 38 , 63
pro fric=27 dil= 4 reg= 38 , 63
pro perm=1.00e-19 porosity=0.3 reg= 38 , 63
;
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 14 , 79
pro coh=8.00e5 tens=8.00e5 reg= 14 , 79
pro fric=30 dil= 5 reg= 14 , 79
pro perm=1.00e-14 porosity=0.3 reg= 14 , 79
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 14 , 74
pro coh=8.00e5 tens=8.00e5 reg= 14 , 74
pro fric=30 dil= 5 reg= 14 , 74
pro perm=1.00e-14 porosity=0.3 reg= 14 , 74
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 15 , 68
pro coh=8.00e5 tens=8.00e5 reg= 15 , 68
pro fric=30 dil= 5 reg= 15 , 68
pro perm=1.00e-14 porosity=0.3 reg= 15 , 68

; LEFT Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 16 , 62
pro coh=8.00e5 tens=8.00e5 reg= 16 , 62
pro fric=30 dil= 5 reg= 16 , 62
pro perm=1.00e-14 porosity=0.3 reg= 16 , 62
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 17 , 56
pro coh=8.00e5 tens=8.00e5 reg= 17 , 56
pro fric=30 dil= 5 reg= 17 , 56
pro perm=1.00e-14 porosity=0.3 reg= 17 , 56
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 18 , 50
pro coh=8.00e5 tens=8.00e5 reg= 18 , 50
pro fric=30 dil= 5 reg= 18 , 50
pro perm=1.00e-14 porosity=0.3 reg= 18 , 50
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 19 , 44
pro coh=8.00e5 tens=8.00e5 reg= 19 , 44
pro fric=30 dil= 5 reg= 19 , 44
pro perm=1.00e-14 porosity=0.3 reg= 19 , 44
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 20 , 38
pro coh=8.00e5 tens=8.00e5 reg= 20 , 38
pro fric=30 dil= 5 reg= 20 , 38
pro perm=1.00e-14 porosity=0.3 reg= 20 , 38
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 21 , 32
pro coh=8.00e5 tens=8.00e5 reg= 21 , 32
pro fric=30 dil= 5 reg= 21 , 32
pro perm=1.00e-14 porosity=0.3 reg= 21 , 32
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 21 , 31
pro coh=8.00e5 tens=8.00e5 reg= 21 , 31
pro fric=30 dil= 5 reg= 21 , 31
pro perm=1.00e-14 porosity=0.3 reg= 21 , 31
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 22 , 25
pro coh=8.00e5 tens=8.00e5 reg= 22 , 25
pro fric=30 dil= 5 reg= 22 , 25
pro perm=1.00e-14 porosity=0.3 reg= 22 , 25
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 23 , 18
pro coh=8.00e5 tens=8.00e5 reg= 23 , 18
pro fric=30 dil= 5 reg= 23 , 18
pro perm=1.00e-14 porosity=0.3 reg= 23 , 18
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 23 , 16
pro coh=8.00e5 tens=8.00e5 reg= 23 , 16
pro fric=30 dil= 5 reg= 23 , 16
pro perm=1.00e-14 porosity=0.3 reg= 23 , 16

```
;MID Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 29 , 80
pro coh=8.00e5 tens=8.00e5 reg= 29 , 80
pro fric=30 dil= 5 reg= 29 , 80
pro perm=1.00e-14 porosity=0.3 reg= 29 , 80
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 30 , 74
pro coh=8.00e5 tens=8.00e5 reg= 30 , 74
pro fric=30 dil= 5 reg= 30 , 74
pro perm=1.00e-14 porosity=0.3 reg= 30 , 74
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 31 , 68
pro coh=8.00e5 tens=8.00e5 reg= 31 , 68
pro fric=30 dil= 5 reg= 31 , 68
pro perm=1.00e-14 porosity=0.3 reg= 31 , 68
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 33 , 61
pro coh=8.00e5 tens=8.00e5 reg= 33 , 61
pro fric=30 dil= 5 reg= 33 , 61
pro perm=1.00e-14 porosity=0.3 reg= 33 , 61
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 33 , 57
pro coh=8.00e5 tens=8.00e5 reg= 33 , 57
pro fric=30 dil= 5 reg= 33 , 57
pro perm=1.00e-14 porosity=0.3 reg= 33 , 57
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 34 , 53
pro coh=8.00e5 tens=8.00e5 reg= 34 , 53
pro fric=30 dil= 5 reg= 34 , 53
pro perm=1.00e-14 porosity=0.3 reg= 34 , 53
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 34 , 51
pro coh=8.00e5 tens=8.00e5 reg= 34 , 51
pro fric=30 dil= 5 reg= 34 , 51
pro perm=1.00e-14 porosity=0.3 reg= 34 , 51
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 35 , 47
pro coh=8.00e5 tens=8.00e5 reg= 35 , 47
pro fric=30 dil= 5 reg= 35 , 47
pro perm=1.00e-14 porosity=0.3 reg= 35 , 47
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 36 , 45
pro coh=8.00e5 tens=8.00e5 reg= 36 , 45
pro fric=30 dil= 5 reg= 36 , 45
pro perm=1.00e-14 porosity=0.3 reg= 36 , 45
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 36 , 43
pro coh=8.00e5 tens=8.00e5 reg= 36 , 43
pro fric=30 dil= 5 reg= 36 , 43
pro perm=1.00e-14 porosity=0.3 reg= 36 , 43
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 36 , 40
pro coh=8.00e5 tens=8.00e5 reg= 36 , 40
pro fric=30 dil= 5 reg= 36 , 40
pro perm=1.00e-14 porosity=0.3 reg= 36 , 40

; RIGHT Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 59 , 80
pro coh=8.00e5 tens=8.00e5 reg= 59 , 80
pro fric=30 dil= 5 reg= 59 , 80
pro perm=1.00e-14 porosity=0.3 reg= 59 , 80
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 59 , 79
pro coh=8.00e5 tens=8.00e5 reg= 59 , 79
pro fric=30 dil= 5 reg= 59 , 79
pro perm=1.00e-14 porosity=0.3 reg= 59 , 79
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 58 , 77
pro coh=8.00e5 tens=8.00e5 reg= 58 , 77
pro fric=30 dil= 5 reg= 58 , 77
pro perm=1.00e-14 porosity=0.3 reg= 58 , 77
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 57 , 75
pro coh=8.00e5 tens=8.00e5 reg= 57 , 75
```

pro fric=30 dil= 5 reg= 57 , 75
pro perm=1.00e-14 porosity=0.3 reg= 57 , 75
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 55 , 71
pro coh=8.00e5 tens=8.00e5 reg= 55 , 71
pro fric=30 dil= 5 reg= 55 , 71
pro perm=1.00e-14 porosity=0.3 reg= 55 , 71
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 56 , 73
pro coh=8.00e5 tens=8.00e5 reg= 56 , 73
pro fric=30 dil= 5 reg= 56 , 73
pro perm=1.00e-14 porosity=0.3 reg= 56 , 73
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 53 , 68
pro coh=8.00e5 tens=8.00e5 reg= 53 , 68
pro fric=30 dil= 5 reg= 53 , 68
pro perm=1.00e-14 porosity=0.3 reg= 53 , 68
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 52 , 66
pro coh=8.00e5 tens=8.00e5 reg= 52 , 66
pro fric=30 dil= 5 reg= 52 , 66
pro perm=1.00e-14 porosity=0.3 reg= 52 , 66
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 52 , 65
pro coh=8.00e5 tens=8.00e5 reg= 52 , 65
pro fric=30 dil= 5 reg= 52 , 65
pro perm=1.00e-14 porosity=0.3 reg= 52 , 65
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 50 , 61
pro coh=8.00e5 tens=8.00e5 reg= 50 , 61
pro fric=30 dil= 5 reg= 50 , 61
pro perm=1.00e-14 porosity=0.3 reg= 50 , 61
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 47 , 56
pro coh=8.00e5 tens=8.00e5 reg= 47 , 56
pro fric=30 dil= 5 reg= 47 , 56
pro perm=1.00e-14 porosity=0.3 reg= 47 , 56
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=51 j=62,63
pro coh=8.00e5 tens=8.00e5 i=51 j=62,63
pro fric=30 dil= 5 i=51 j=62,63
pro perm=1.00e-14 porosity=0.3 i=51 j=62,63
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=49 j=58,59
pro coh=8.00e5 tens=8.00e5 i=49 j=58,59
pro fric=30 dil= 5 i=49 j=58,59
pro perm=1.00e-14 porosity=0.3 i=49 j=58,59
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=50 j=62,63
pro coh=8.00e5 tens=8.00e5 i=50 j=62,63
pro fric=30 dil= 5 i=50 j=62,63
pro perm=1.00e-14 porosity=0.3 i=50 j=62,63
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=48 j=58,59
pro coh=8.00e5 tens=8.00e5 i=48 j=58,59
pro fric=30 dil= 5 i=48 j=58,59
pro perm=1.00e-14 porosity=0.3 i=48 j=58,59
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=47 j=54,55
pro coh=8.00e5 tens=8.00e5 i=47 j=54,55
pro fric=30 dil= 5 i=47 j=54,55
pro perm=1.00e-14 porosity=0.3 i=47 j=54,55
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=46 j=52,53
pro coh=8.00e5 tens=8.00e5 i=46 j=52,53
pro fric=30 dil= 5 i=46 j=52,53
pro perm=1.00e-14 porosity=0.3 i=46 j=52,53
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 45 , 51
pro coh=8.00e5 tens=8.00e5 reg= 45 , 51
pro fric=30 dil= 5 reg= 45 , 51
pro perm=1.00e-14 porosity=0.3 reg= 45 , 51
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 44 , 50
pro coh=8.00e5 tens=8.00e5 reg= 44 , 50

pro fric=30 dil= 5 reg= 44 , 50
pro perm=1.00e-14 porosity=0.3 reg= 44 , 50
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 44 , 49
pro coh=8.00e5 tens=8.00e5 reg= 44 , 49
pro fric=30 dil= 5 reg= 44 , 49
pro perm=1.00e-14 porosity=0.3 reg= 44 , 49
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 43 , 48
pro coh=8.00e5 tens=8.00e5 reg= 43 , 48
pro fric=30 dil= 5 reg= 43 , 48
pro perm=1.00e-14 porosity=0.3 reg= 43 , 48
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=46 j=54,55
pro coh=8.00e5 tens=8.00e5 i=46 j=54,55
pro fric=30 dil= 5 i=46 j=54,55
pro perm=1.00e-14 porosity=0.3 i=46 j=54,55
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=45 j=52,53
pro coh=8.00e5 tens=8.00e5 i=45 j=52,53
pro fric=30 dil= 5 i=45 j=52,53
pro perm=1.00e-14 porosity=0.3 i=45 j=52,53
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=43 j=46,47
pro coh=8.00e5 tens=8.00e5 i=43 j=46,47
pro fric=30 dil= 5 i=43 j=46,47
pro perm=1.00e-14 porosity=0.3 i=43 j=46,47
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=42 j=44,45
pro coh=8.00e5 tens=8.00e5 i=42 j=44,45
pro fric=30 dil= 5 i=42 j=44,45
pro perm=1.00e-14 porosity=0.3 i=42 j=44,45
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=41 j=42,43
pro coh=8.00e5 tens=8.00e5 i=41 j=42,43
pro fric=30 dil= 5 i=41 j=42,43
pro perm=1.00e-14 porosity=0.3 i=41 j=42,43
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=40 j=40,41
pro coh=8.00e5 tens=8.00e5 i=40 j=40,41
pro fric=30 dil= 5 i=40 j=40,41
pro perm=1.00e-14 porosity=0.3 i=40 j=40,41
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=42 j=46,47
pro coh=8.00e5 tens=8.00e5 i=42 j=46,47
pro fric=30 dil= 5 i=42 j=46,47
pro perm=1.00e-14 porosity=0.3 i=42 j=46,47
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 41 , 44
pro coh=8.00e5 tens=8.00e5 reg= 41 , 44
pro fric=30 dil= 5 reg= 41 , 44
pro perm=1.00e-14 porosity=0.3 reg= 41 , 44
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=40 j=42,43
pro coh=8.00e5 tens=8.00e5 i=40 j=42,43
pro fric=30 dil= 5 i=40 j=42,43
pro perm=1.00e-14 porosity=0.3 i=40 j=42,43
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=39 j=38,41
pro coh=8.00e5 tens=8.00e5 i=39 j=38,41
pro fric=30 dil= 5 i=39 j=38,41
pro perm=1.00e-14 porosity=0.3 i=39 j=38,41
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=38 j=38,39
pro coh=8.00e5 tens=8.00e5 i=38 j=38,39
pro fric=30 dil= 5 i=38 j=38,39
pro perm=1.00e-14 porosity=0.3 i=38 j=38,39
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=36,37 j=35
pro coh=8.00e5 tens=8.00e5 i=36,37 j=35
pro fric=30 dil= 5 i=36,37 j=35
pro perm=1.00e-14 porosity=0.3 i=36,37 j=35
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 37 , 34
pro coh=8.00e5 tens=8.00e5 reg= 37 , 34

pro fric=30 dil= 5 reg= 37 , 34
pro perm=1.00e-14 porosity=0.3 reg= 37 , 34
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 35 , 32
pro coh=8.00e5 tens=8.00e5 reg= 35 , 32
pro fric=30 dil= 5 reg= 35 , 32
pro perm=1.00e-14 porosity=0.3 reg= 35 , 32
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=35 j=30,31
pro coh=8.00e5 tens=8.00e5 i=35 j=30,31
pro fric=30 dil= 5 i=35 j=30,31
pro perm=1.00e-14 porosity=0.3 i=35 j=30,31
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=34 j=28,31
pro coh=8.00e5 tens=8.00e5 i=34 j=28,31
pro fric=30 dil= 5 i=34 j=28,31
pro perm=1.00e-14 porosity=0.3 i=34 j=28,31
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=33 j=26,29
pro coh=8.00e5 tens=8.00e5 i=33 j=26,29
pro fric=30 dil= 5 i=33 j=26,29
pro perm=1.00e-14 porosity=0.3 i=33 j=26,29
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=32 j=25,27
pro coh=8.00e5 tens=8.00e5 i=32 j=25,27
pro fric=30 dil= 5 i=32 j=25,27
pro perm=1.00e-14 porosity=0.3 i=32 j=25,27
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=31 j=24,25
pro coh=8.00e5 tens=8.00e5 i=31 j=24,25
pro fric=30 dil= 5 i=31 j=24,25
pro perm=1.00e-14 porosity=0.3 i=31 j=24,25
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=31 j=22,25
pro coh=8.00e5 tens=8.00e5 i=31 j=22,25
pro fric=30 dil= 5 i=31 j=22,25
pro perm=1.00e-14 porosity=0.3 i=31 j=22,25
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 29 , 20
pro coh=8.00e5 tens=8.00e5 reg= 29 , 20
pro fric=30 dil= 5 reg= 29 , 20
pro perm=1.00e-14 porosity=0.3 reg= 29 , 20
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=30 j=20,23
pro coh=8.00e5 tens=8.00e5 i=30 j=20,23
pro fric=30 dil= 5 i=30 j=20,23
pro perm=1.00e-14 porosity=0.3 i=30 j=20,23
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 28 , 18
pro coh=8.00e5 tens=8.00e5 reg= 28 , 18
pro fric=30 dil= 5 reg= 28 , 18
pro perm=1.00e-14 porosity=0.3 reg= 28 , 18
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 28 , 17
pro coh=8.00e5 tens=8.00e5 reg= 28 , 17
pro fric=30 dil= 5 reg= 28 , 17
pro perm=1.00e-14 porosity=0.3 reg= 28 , 17
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 26 , 13
pro coh=8.00e5 tens=8.00e5 reg= 26 , 13
pro fric=30 dil= 5 reg= 26 , 13
pro perm=1.00e-14 porosity=0.3 reg= 26 , 13
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 25 , 12
pro coh=8.00e5 tens=8.00e5 reg= 25 , 12
pro fric=30 dil= 5 reg= 25 , 12
pro perm=1.00e-14 porosity=0.3 reg= 25 , 12
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 26 , 15
pro coh=8.00e5 tens=8.00e5 reg= 26 , 15
pro fric=30 dil= 5 reg= 26 , 15
pro perm=1.00e-14 porosity=0.3 reg= 26 , 15
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 25 , 11
pro coh=8.00e5 tens=8.00e5 reg= 25 , 11

pro fric=30 dil= 5 reg= 25 , 11
pro perm=1.00e-14 porosity=0.3 reg= 25 , 11
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 24 , 10
pro coh=8.00e5 tens=8.00e5 reg= 24 , 10
pro fric=30 dil= 5 reg= 24 , 10
pro perm=1.00e-14 porosity=0.3 reg= 24 , 10
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 24 , 9
pro coh=8.00e5 tens=8.00e5 reg= 24 , 9
pro fric=30 dil= 5 reg= 24 , 9
pro perm=1.00e-14 porosity=0.3 reg= 24 , 9
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 23 , 7
pro coh=8.00e5 tens=8.00e5 reg= 23 , 7
pro fric=30 dil= 5 reg= 23 , 7
pro perm=1.00e-14 porosity=0.3 reg= 23 , 7
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 22 , 5
pro coh=8.00e5 tens=8.00e5 reg= 22 , 5
pro fric=30 dil= 5 reg= 22 , 5
pro perm=1.00e-14 porosity=0.3 reg= 22 , 5
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 21 , 3
pro coh=8.00e5 tens=8.00e5 reg= 21 , 3
pro fric=30 dil= 5 reg= 21 , 3
pro perm=1.00e-14 porosity=0.3 reg= 21 , 3
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 20 , 1
pro coh=8.00e5 tens=8.00e5 reg= 20 , 1
pro fric=30 dil= 5 reg= 20 , 1
pro perm=1.00e-14 porosity=0.3 reg= 20 , 1
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 i=45 j=50
pro coh=2.7e7 tens=2.00e6 i=45 j=50
pro fric=27 dil= 4 i=45 j=50
pro perm=1.00e-19 porosity=0.3 i=45 j=50
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 i=58 j=80
pro coh=2.7e7 tens=2.00e6 i=58 j=80
pro fric=27 dil= 4 i=58 j=80
pro perm=1.00e-19 porosity=0.3 i=58 j=80

; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=38 j=40,41
pro coh=3.47e7 tens=2.00e6 i=38 j=40,41
pro fric=32 dil= 4 i=38 j=40,41
pro perm=1.00e-16 porosity=0.3 i=38 j=40,41
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=41 j=45
pro coh=3.47e7 tens=2.00e6 i=41 j=45
pro fric=32 dil= 4 i=41 j=45
pro perm=1.00e-16 porosity=0.3 i=41 j=45
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=36 j=31
pro coh=3.47e7 tens=2.00e6 i=36 j=31
pro fric=32 dil= 4 i=36 j=31
pro perm=1.00e-16 porosity=0.3 i=36 j=31
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=20 j=45
pro coh=3.47e7 tens=2.00e6 i=20 j=45
pro fric=32 dil= 4 i=20 j=45
pro perm=1.00e-16 porosity=0.3 i=20 j=45
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 25 , j=14,16
pro coh=3.84e7 tens=8.00e5 i= 25 , j=14,16
pro fric=14 dil= 1 i= 25 , j=14,16
pro perm=1.00e-19 porosity=0.2 i= 25 , j=14,16
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 26 , j=16
pro coh=3.84e7 tens=8.00e5 i= 26 , j=16
pro fric=14 dil= 1 i= 26 , j=16
pro perm=1.00e-19 porosity=0.2 i= 26 , j=16
; Shale (ore zone)
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 22 , j=21

```

pro coh=3.84e7 tens=8.00e5 i= 22 , j=21
pro fric=14 dil= 5 i= 22 , j=21
pro perm=5.00e-15 porosity=0.2 i= 22 , j=21
; Shale (ore zone)
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 33 , j=25
pro coh=3.84e7 tens=8.00e5 i= 33 , j=25
pro fric=14 dil= 5 i= 33 , j=25
pro perm=5.00e-15 porosity=0.2 i= 33 , j=25
; Shale (ore zone)
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 29 , j=22
pro coh=3.84e7 tens=8.00e5 i= 29 , j=22
pro fric=14 dil= 5 i= 29 , j=22
pro perm=5.00e-15 porosity=0.2 i= 29 , j=22
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 21 , j=1
pro coh=3.84e7 tens=8.00e5 i= 21 , j=1
pro fric=14 dil= 1 i= 21 , j=1
pro perm=1.00e-19 porosity=0.2 i= 21 , j=1
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 i=24,28 j=20
pro coh=3.6e7 tens=8.00e5 i=24,28 j=20
pro fric=23 dil= 2 i=24,28 j=20
pro perm=5.00e-16 porosity=0.3 i=24,28 j=20
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 i=34 , j=27
pro coh=3.6e7 tens=8.00e5 i=34 , j=27
pro fric=23 dil= 2 reg= i=34 , j=27
pro perm=5.00e-16 porosity=0.3 i=34 , j=27
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 i=31 , j=21
pro coh=3.6e7 tens=8.00e5 i=31 , j=21
pro fric=23 dil= 2 i=31 , j=21
pro perm=1.00e-18 porosity=0.2 i=31 , j=21
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 i=27 , j=18
pro coh=3.6e7 tens=8.00e5 i=27 , j=18
pro fric=23 dil= 2 i=27 , j=18
pro perm=1.00e-18 porosity=0.2 i=27 , j=18
;-----END OF PROPERTIES-----

def ini_stress
hh1 = 0.5*abs(y(1,2) - y(1,1))
surf_load = -2.5e3*9.8*2500
str_add = hh1*9.8*2700
bot_str = (-1.0)*(2.9e3*9.8*2500 - str_add)
top_str = (-1.0)*(2.5e3*9.8*2500 + str_add)

str_var = top_str - bot_str

command
ini sxx bot_str var=0,str_var i=1,80 j=1,80
ini syy bot_str var=0,str_var i=1,80 j=1,80
ini szz bot_str var=0,str_var i=1,80 j=1,80
ini sxy = 0.0
end_command

end
ini_stress

apply ns surf_load i=1,81 j=81

def hydro_pp
surf_pp = 2.5e3*9.8*1000 + 1e5 ;pp (2.5km) + pp (atmospheric loading)
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
;sss2 = 0
sss2 = surf_pp
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa + surf_pp
end_if
gpp(i, j) = sss2
end_loop

```

```

end_loop
end
hydro_pp
*
;
;
;
ini sat 1
fix sat

;fix pp j=81
;
set gravity=9.8
;
set large
;
;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=40 j=40
;hist 3 pp i=40 j=40

hist 3 pp i=10 j=18;sst/mud
hist 4 pp i=10 j=20;lower sst/sh
hist 5 pp i=10 j=22;shale
hist 6 pp i=10 j=26;higher sst/sh
hist 7 pp i=10 j=28;sst cap

;Movie every 500 steps
plot pp fill
sav m2c_ini.sav
movie on file m2c.dcx step 500

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTLING
fix x i=1
fix x i=81
fix y j=1

; Gravity settling
STEP 1500

;Set fluid on run to equilibrium
set flow on
pl pp fi fl bl
STEP 1500

;***Fish function to set overpressure from j=45 to j=1****
def overpress_pp
surf_pp = 3.0e3*9.8*2700 + 1e5 ;pp (3km) + pp (atmospheric loading)
loop i (1,igp)
loop j (1,45)
if j < 45 Then
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 2700 * 9.8 * aaa + surf_pp
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
overpress_pp
*
;
sav m2c_overpress.sav

free x
free y

;Compression 5% shortening
ini xvel 0.0008 var=-0.0016 ,0 i=1, 81 j=1, 81
fix x i=1
fix x i= 81
fix y j=1

step 2500
save m2c_1.sav ; 1 % compression
step 2500

```

```

save m2c_2.sav ; 2 % compression
step 2500
save m2c_3.sav ; 3 % compression
step 2500
save m2c_4.sav ; 4 % compression
step 2500
save m2c_5.sav ; 5 % compression
step 2500
save m2c_6.sav ; 6 % extension
step 2500
save m2c_7.sav ; 7 % extension
step 2500
save m2c_9.sav ; 8 % compression
step 2500
save m2c_10.sav ; 9 % compression
step 2500
save m2c_11.sav ; 10 % compression
step 2500
save m2c_12.sav ; 11 % compression
step 2500
save m2c_13.sav ; 12 % compression

return
stop

```

C.6 Model 2d

```

;
tit
Century Model 2 - Compression
;
config extra 9 gw
grid 80 80
gen 0.00e0,-2.90e3 0.00e0,-2.50e3 4.00e2,-2.50e3 4.00e2,-2.90e3 i=1,81 j=1,81
mark i=1
mark j=1
mark i = 81
mark j = 81
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3 ; to be elaborated below
;; 1 mech step = 1 fluid step;
set nmech 1 ngw 1 flow off
*****

```

GEOMETRY AS PREVIOUS MODEL

```

; Properties for each sub-regions:
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 21 , 62
pro coh=2.7e7 tens=2.00e6 reg= 21 , 62
pro fric=27 dil= 4 reg= 21 , 62
pro perm=1.00e-19 porosity=0.3 reg= 21 , 62
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 65 , 62
pro coh=2.7e7 tens=2.00e6 reg= 65 , 62
pro fric=27 dil= 4 reg= 65 , 62
pro perm=1.00e-19 porosity=0.3 reg= 65 , 62
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 8 , 36
pro coh=3.47e7 tens=2.00e6 reg= 8 , 36
pro fric=32 dil= 4 reg= 8 , 36
pro perm=1.00e-16 porosity=0.3 reg= 8 , 36
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 60 , 38
pro coh=3.47e7 tens=2.00e6 reg= 60 , 38
pro fric=32 dil= 4 reg= 60 , 38
pro perm=1.00e-16 porosity=0.3 reg= 60 , 38
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 11 , 8

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pro coh=3.84e7 tens=8.00e5 reg= 11 , 8
pro fric=14 dil= 1 reg= 11 , 8
pro perm=1.00e-19 porosity=0.2 reg= 11 , 8
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 reg= 57 , 8
pro coh=3.84e7 tens=8.00e5 reg= 57 , 8
pro fric=14 dil= 1 reg= 57 , 8
pro perm=1.00e-19 porosity=0.2 reg= 57 , 8
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 5 , 24
pro coh=3.6e7 tens=8.00e5 reg= 5 , 24
pro fric=23 dil= 2 reg= 5 , 24
pro perm=5.00e-16 porosity=0.3 reg= 5 , 24
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 55 , 28
pro coh=3.6e7 tens=8.00e5 reg= 55 , 28
pro fric=23 dil= 2 reg= 55 , 28
pro perm=5.00e-16 porosity=0.3 reg= 55 , 28
; Shale (ore zone)
pro dens= 2500 bulk=2.2e11 shear=1.66e11 reg= 3 , 21
pro coh=3.84e8 tens=2.00e5 reg= 3 , 21
pro fric=14 dil= 5 reg= 3 , 21
pro perm=1.00e-15 porosity=0.2 reg= 3 , 21
; Shale (ore zone)
pro dens= 2500 bulk=2.2e11 shear=1.66e11 reg= 75 , 25
pro coh=3.84e8 tens=2.00e5 reg= 75 , 25
pro fric=14 dil= 5 reg= 75 , 25
pro perm=1.00e-15 porosity=0.2 reg= 75 , 25
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 12 , 19
pro coh=3.6e7 tens=8.00e5 reg= 12 , 19
pro fric=23 dil= 2 reg= 12 , 19
pro perm=5.00e-16 porosity=0.3 reg= 12 , 19
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 32 , 23
pro coh=3.6e7 tens=8.00e5 reg= 32 , 23
pro fric=23 dil= 2 reg= 32 , 23
pro perm=5.00e-16 porosity=0.3 reg= 32 , 23
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 reg= 5 , 17
pro coh=3.6e7 tens=8.00e5 reg= 5 , 17
pro fric=23 dil= 2 reg= 5 , 17
pro perm=1.00e-18 porosity=0.2 reg= 5 , 17
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 reg= 55 , 21
pro coh=3.6e7 tens=8.00e5 reg= 55 , 21
pro fric=23 dil= 2 reg= 55 , 21
pro perm=1.00e-18 porosity=0.2 reg= 55 , 21
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 27 , 36
pro coh=3.47e7 tens=2.00e6 reg= 27 , 36
pro fric=32 dil= 4 reg= 27 , 36
pro perm=1.00e-16 porosity=0.3 reg= 27 , 36
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 reg= 38 , 43
pro coh=3.47e7 tens=2.00e6 reg= 38 , 43
pro fric=32 dil= 4 reg= 38 , 43
pro perm=1.00e-16 porosity=0.3 reg= 38 , 43
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 24 , 24
pro coh=3.6e7 tens=8.00e5 reg= 24 , 24
pro fric=23 dil= 2 reg= 24 , 24
pro perm=5.00e-16 porosity=0.3 reg= 24 , 24
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 reg= 25 , 19
pro coh=3.6e7 tens=8.00e5 reg= 25 , 19
pro fric=23 dil= 2 reg= 25 , 19
pro perm=5.00e-16 porosity=0.3 reg= 25 , 19
; Shale (ore zone)
pro dens= 2500 bulk=2.2e11 shear=1.66e11 reg= 25 , 21
pro coh=3.84e8 tens=2.00e5 reg= 25 , 21
pro fric=14 dil= 5 reg= 25 , 21
pro perm=1.00e-15 porosity=0.2 reg= 25 , 21
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 reg= 25 , 17

pro coh=3.6e7 tens=8.00e5 reg= 25 , 17
pro fric=23 dil= 2 reg= 25 , 17
pro perm=1.00e-18 porosity=0.2 reg= 25 , 17
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 4 , 56
pro coh=2.7e7 tens=2.00e6 reg= 4 , 56
pro fric=27 dil= 4 reg= 4 , 56
pro perm=1.00e-19 porosity=0.3 reg= 4 , 56
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 reg= 38 , 63
pro coh=2.7e7 tens=2.00e6 reg= 38 , 63
pro fric=27 dil= 4 reg= 38 , 63
pro perm=1.00e-19 porosity=0.3 reg= 38 , 63
;
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 14 , 79
pro coh=8.00e5 tens=8.00e5 reg= 14 , 79
pro fric=30 dil= 5 reg= 14 , 79
pro perm=1.00e-14 porosity=0.3 reg= 14 , 79
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 14 , 74
pro coh=8.00e5 tens=8.00e5 reg= 14 , 74
pro fric=30 dil= 5 reg= 14 , 74
pro perm=1.00e-14 porosity=0.3 reg= 14 , 74
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 15 , 68
pro coh=8.00e5 tens=8.00e5 reg= 15 , 68
pro fric=30 dil= 5 reg= 15 , 68
pro perm=1.00e-14 porosity=0.3 reg= 15 , 68

; LEFT Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 16 , 62
pro coh=8.00e5 tens=8.00e5 reg= 16 , 62
pro fric=30 dil= 5 reg= 16 , 62
pro perm=1.00e-14 porosity=0.3 reg= 16 , 62
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 17 , 56
pro coh=8.00e5 tens=8.00e5 reg= 17 , 56
pro fric=30 dil= 5 reg= 17 , 56
pro perm=1.00e-14 porosity=0.3 reg= 17 , 56
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 18 , 50
pro coh=8.00e5 tens=8.00e5 reg= 18 , 50
pro fric=30 dil= 5 reg= 18 , 50
pro perm=1.00e-14 porosity=0.3 reg= 18 , 50
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 19 , 44
pro coh=8.00e5 tens=8.00e5 reg= 19 , 44
pro fric=30 dil= 5 reg= 19 , 44
pro perm=1.00e-14 porosity=0.3 reg= 19 , 44
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 20 , 38
pro coh=8.00e5 tens=8.00e5 reg= 20 , 38
pro fric=30 dil= 5 reg= 20 , 38
pro perm=1.00e-14 porosity=0.3 reg= 20 , 38
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 21 , 32
pro coh=8.00e5 tens=8.00e5 reg= 21 , 32
pro fric=30 dil= 5 reg= 21 , 32
pro perm=1.00e-14 porosity=0.3 reg= 21 , 32
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 21 , 31
pro coh=8.00e5 tens=8.00e5 reg= 21 , 31
pro fric=30 dil= 5 reg= 21 , 31
pro perm=1.00e-14 porosity=0.3 reg= 21 , 31
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 22 , 25
pro coh=8.00e5 tens=8.00e5 reg= 22 , 25
pro fric=30 dil= 5 reg= 22 , 25
pro perm=1.00e-14 porosity=0.3 reg= 22 , 25
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 23 , 18
pro coh=8.00e5 tens=8.00e5 reg= 23 , 18
pro fric=30 dil= 5 reg= 23 , 18
pro perm=1.00e-14 porosity=0.3 reg= 23 , 18

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 23 , 16
pro coh=8.00e5 tens=8.00e5 reg= 23 , 16
pro fric=30 dil= 5 reg= 23 , 16
pro perm=1.00e-14 porosity=0.3 reg= 23 , 16

;MID Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 29 , 80
pro coh=8.00e5 tens=8.00e5 reg= 29 , 80
pro fric=30 dil= 5 reg= 29 , 80
pro perm=1.00e-14 porosity=0.3 reg= 29 , 80

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 30 , 74
pro coh=8.00e5 tens=8.00e5 reg= 30 , 74
pro fric=30 dil= 5 reg= 30 , 74
pro perm=1.00e-14 porosity=0.3 reg= 30 , 74

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 31 , 68
pro coh=8.00e5 tens=8.00e5 reg= 31 , 68
pro fric=30 dil= 5 reg= 31 , 68
pro perm=1.00e-14 porosity=0.3 reg= 31 , 68

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 33 , 61
pro coh=8.00e5 tens=8.00e5 reg= 33 , 61
pro fric=30 dil= 5 reg= 33 , 61
pro perm=1.00e-14 porosity=0.3 reg= 33 , 61

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 33 , 57
pro coh=8.00e5 tens=8.00e5 reg= 33 , 57
pro fric=30 dil= 5 reg= 33 , 57
pro perm=1.00e-14 porosity=0.3 reg= 33 , 57

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 34 , 53
pro coh=8.00e5 tens=8.00e5 reg= 34 , 53
pro fric=30 dil= 5 reg= 34 , 53
pro perm=1.00e-14 porosity=0.3 reg= 34 , 53

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 34 , 51
pro coh=8.00e5 tens=8.00e5 reg= 34 , 51
pro fric=30 dil= 5 reg= 34 , 51
pro perm=1.00e-14 porosity=0.3 reg= 34 , 51

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 35 , 47
pro coh=8.00e5 tens=8.00e5 reg= 35 , 47
pro fric=30 dil= 5 reg= 35 , 47
pro perm=1.00e-14 porosity=0.3 reg= 35 , 47

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 36 , 45
pro coh=8.00e5 tens=8.00e5 reg= 36 , 45
pro fric=30 dil= 5 reg= 36 , 45
pro perm=1.00e-14 porosity=0.3 reg= 36 , 45

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 36 , 43
pro coh=8.00e5 tens=8.00e5 reg= 36 , 43
pro fric=30 dil= 5 reg= 36 , 43
pro perm=1.00e-14 porosity=0.3 reg= 36 , 43

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 36 , 40
pro coh=8.00e5 tens=8.00e5 reg= 36 , 40
pro fric=30 dil= 5 reg= 36 , 40
pro perm=1.00e-14 porosity=0.3 reg= 36 , 40

; RIGHT Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 59 , 80
pro coh=8.00e5 tens=8.00e5 reg= 59 , 80
pro fric=30 dil= 5 reg= 59 , 80
pro perm=1.00e-14 porosity=0.3 reg= 59 , 80

; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 59 , 79
pro coh=8.00e5 tens=8.00e5 reg= 59 , 79
pro fric=30 dil= 5 reg= 59 , 79
pro perm=1.00e-14 porosity=0.3 reg= 59 , 79
; Fault

pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 58 , 77
pro coh=8.00e5 tens=8.00e5 reg= 58 , 77
pro fric=30 dil= 5 reg= 58 , 77
pro perm=1.00e-14 porosity=0.3 reg= 58 , 77
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 57 , 75
pro coh=8.00e5 tens=8.00e5 reg= 57 , 75
pro fric=30 dil= 5 reg= 57 , 75
pro perm=1.00e-14 porosity=0.3 reg= 57 , 75
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 55 , 71
pro coh=8.00e5 tens=8.00e5 reg= 55 , 71
pro fric=30 dil= 5 reg= 55 , 71
pro perm=1.00e-14 porosity=0.3 reg= 55 , 71
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 56 , 73
pro coh=8.00e5 tens=8.00e5 reg= 56 , 73
pro fric=30 dil= 5 reg= 56 , 73
pro perm=1.00e-14 porosity=0.3 reg= 56 , 73
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 53 , 68
pro coh=8.00e5 tens=8.00e5 reg= 53 , 68
pro fric=30 dil= 5 reg= 53 , 68
pro perm=1.00e-14 porosity=0.3 reg= 53 , 68
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 52 , 66
pro coh=8.00e5 tens=8.00e5 reg= 52 , 66
pro fric=30 dil= 5 reg= 52 , 66
pro perm=1.00e-14 porosity=0.3 reg= 52 , 66
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 52 , 65
pro coh=8.00e5 tens=8.00e5 reg= 52 , 65
pro fric=30 dil= 5 reg= 52 , 65
pro perm=1.00e-14 porosity=0.3 reg= 52 , 65
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 50 , 61
pro coh=8.00e5 tens=8.00e5 reg= 50 , 61
pro fric=30 dil= 5 reg= 50 , 61
pro perm=1.00e-14 porosity=0.3 reg= 50 , 61
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 47 , 56
pro coh=8.00e5 tens=8.00e5 reg= 47 , 56
pro fric=30 dil= 5 reg= 47 , 56
pro perm=1.00e-14 porosity=0.3 reg= 47 , 56
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=51 j=62,63
pro coh=8.00e5 tens=8.00e5 i=51 j=62,63
pro fric=30 dil= 5 i=51 j=62,63
pro perm=1.00e-14 porosity=0.3 i=51 j=62,63
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=49 j=58,59
pro coh=8.00e5 tens=8.00e5 i=49 j=58,59
pro fric=30 dil= 5 i=49 j=58,59
pro perm=1.00e-14 porosity=0.3 i=49 j=58,59
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=50 j=62,63
pro coh=8.00e5 tens=8.00e5 i=50 j=62,63
pro fric=30 dil= 5 i=50 j=62,63
pro perm=1.00e-14 porosity=0.3 i=50 j=62,63
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=48 j=58,59
pro coh=8.00e5 tens=8.00e5 i=48 j=58,59
pro fric=30 dil= 5 i=48 j=58,59
pro perm=1.00e-14 porosity=0.3 i=48 j=58,59
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=47 j=54,55
pro coh=8.00e5 tens=8.00e5 i=47 j=54,55
pro fric=30 dil= 5 i=47 j=54,55
pro perm=1.00e-14 porosity=0.3 i=47 j=54,55
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=46 j=52,53
pro coh=8.00e5 tens=8.00e5 i=46 j=52,53
pro fric=30 dil= 5 i=46 j=52,53
pro perm=1.00e-14 porosity=0.3 i=46 j=52,53
; Fault

pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 45 , 51
pro coh=8.00e5 tens=8.00e5 reg= 45 , 51
pro fric=30 dil= 5 reg= 45 , 51
pro perm=1.00e-14 porosity=0.3 reg= 45 , 51
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 44 , 50
pro coh=8.00e5 tens=8.00e5 reg= 44 , 50
pro fric=30 dil= 5 reg= 44 , 50
pro perm=1.00e-14 porosity=0.3 reg= 44 , 50
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 44 , 49
pro coh=8.00e5 tens=8.00e5 reg= 44 , 49
pro fric=30 dil= 5 reg= 44 , 49
pro perm=1.00e-14 porosity=0.3 reg= 44 , 49
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 43 , 48
pro coh=8.00e5 tens=8.00e5 reg= 43 , 48
pro fric=30 dil= 5 reg= 43 , 48
pro perm=1.00e-14 porosity=0.3 reg= 43 , 48
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=46 j=54,55
pro coh=8.00e5 tens=8.00e5 i=46 j=54,55
pro fric=30 dil= 5 i=46 j=54,55
pro perm=1.00e-14 porosity=0.3 i=46 j=54,55
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=45 j=52,53
pro coh=8.00e5 tens=8.00e5 i=45 j=52,53
pro fric=30 dil= 5 i=45 j=52,53
pro perm=1.00e-14 porosity=0.3 i=45 j=52,53
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=43 j=46,47
pro coh=8.00e5 tens=8.00e5 i=43 j=46,47
pro fric=30 dil= 5 i=43 j=46,47
pro perm=1.00e-14 porosity=0.3 i=43 j=46,47
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=42 j=44,45
pro coh=8.00e5 tens=8.00e5 i=42 j=44,45
pro fric=30 dil= 5 i=42 j=44,45
pro perm=1.00e-14 porosity=0.3 i=42 j=44,45
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=41 j=42,43
pro coh=8.00e5 tens=8.00e5 i=41 j=42,43
pro fric=30 dil= 5 i=41 j=42,43
pro perm=1.00e-14 porosity=0.3 i=41 j=42,43
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=40 j=40,41
pro coh=8.00e5 tens=8.00e5 i=40 j=40,41
pro fric=30 dil= 5 i=40 j=40,41
pro perm=1.00e-14 porosity=0.3 i=40 j=40,41
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=42 j=46,47
pro coh=8.00e5 tens=8.00e5 i=42 j=46,47
pro fric=30 dil= 5 i=42 j=46,47
pro perm=1.00e-14 porosity=0.3 i=42 j=46,47
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 41 , 44
pro coh=8.00e5 tens=8.00e5 reg= 41 , 44
pro fric=30 dil= 5 reg= 41 , 44
pro perm=1.00e-14 porosity=0.3 reg= 41 , 44
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=40 j=42,43
pro coh=8.00e5 tens=8.00e5 i=40 j=42,43
pro fric=30 dil= 5 i=40 j=42,43
pro perm=1.00e-14 porosity=0.3 i=40 j=42,43
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=39 j=38,41
pro coh=8.00e5 tens=8.00e5 i=39 j=38,41
pro fric=30 dil= 5 i=39 j=38,41
pro perm=1.00e-14 porosity=0.3 i=39 j=38,41
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=38 j=38,39
pro coh=8.00e5 tens=8.00e5 i=38 j=38,39
pro fric=30 dil= 5 i=38 j=38,39
pro perm=1.00e-14 porosity=0.3 i=38 j=38,39
; Fault

pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=36,37 j=35
pro coh=8.00e5 tens=8.00e5 i=36,37 j=35
pro fric=30 dil= 5 i=36,37 j=35
pro perm=1.00e-14 porosity=0.3 i=36,37 j=35
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 37 , 34
pro coh=8.00e5 tens=8.00e5 reg= 37 , 34
pro fric=30 dil= 5 reg= 37 , 34
pro perm=1.00e-14 porosity=0.3 reg= 37 , 34
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 35 , 32
pro coh=8.00e5 tens=8.00e5 reg= 35 , 32
pro fric=30 dil= 5 reg= 35 , 32
pro perm=1.00e-14 porosity=0.3 reg= 35 , 32
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=35 j=30,31
pro coh=8.00e5 tens=8.00e5 i=35 j=30,31
pro fric=30 dil= 5 i=35 j=30,31
pro perm=1.00e-14 porosity=0.3 i=35 j=30,31
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=34 j=28,31
pro coh=8.00e5 tens=8.00e5 i=34 j=28,31
pro fric=30 dil= 5 i=34 j=28,31
pro perm=1.00e-14 porosity=0.3 i=34 j=28,31
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=33 j=26,29
pro coh=8.00e5 tens=8.00e5 i=33 j=26,29
pro fric=30 dil= 5 i=33 j=26,29
pro perm=1.00e-14 porosity=0.3 i=33 j=26,29
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=32 j=25,27
pro coh=8.00e5 tens=8.00e5 i=32 j=25,27
pro fric=30 dil= 5 i=32 j=25,27
pro perm=1.00e-14 porosity=0.3 i=32 j=25,27
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=31 j=24,25
pro coh=8.00e5 tens=8.00e5 i=31 j=24,25
pro fric=30 dil= 5 i=31 j=24,25
pro perm=1.00e-14 porosity=0.3 i=31 j=24,25
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=31 j=22,25
pro coh=8.00e5 tens=8.00e5 i=31 j=22,25
pro fric=30 dil= 5 i=31 j=22,25
pro perm=1.00e-14 porosity=0.3 i=31 j=22,25
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 29 , 20
pro coh=8.00e5 tens=8.00e5 reg= 29 , 20
pro fric=30 dil= 5 reg= 29 , 20
pro perm=1.00e-14 porosity=0.3 reg= 29 , 20
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 i=30 j=20,23
pro coh=8.00e5 tens=8.00e5 i=30 j=20,23
pro fric=30 dil= 5 i=30 j=20,23
pro perm=1.00e-14 porosity=0.3 i=30 j=20,23
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 28 , 18
pro coh=8.00e5 tens=8.00e5 reg= 28 , 18
pro fric=30 dil= 5 reg= 28 , 18
pro perm=1.00e-14 porosity=0.3 reg= 28 , 18
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 28 , 17
pro coh=8.00e5 tens=8.00e5 reg= 28 , 17
pro fric=30 dil= 5 reg= 28 , 17
pro perm=1.00e-14 porosity=0.3 reg= 28 , 17
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 26 , 13
pro coh=8.00e5 tens=8.00e5 reg= 26 , 13
pro fric=30 dil= 5 reg= 26 , 13
pro perm=1.00e-14 porosity=0.3 reg= 26 , 13
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 25 , 12
pro coh=8.00e5 tens=8.00e5 reg= 25 , 12
pro fric=30 dil= 5 reg= 25 , 12
pro perm=1.00e-14 porosity=0.3 reg= 25 , 12
; Fault

```

pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 26 , 15
pro coh=8.00e5 tens=8.00e5 reg= 26 , 15
pro fric=30 dil= 5 reg= 26 , 15
pro perm=1.00e-14 porosity=0.3 reg= 26 , 15
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 25 , 11
pro coh=8.00e5 tens=8.00e5 reg= 25 , 11
pro fric=30 dil= 5 reg= 25 , 11
pro perm=1.00e-14 porosity=0.3 reg= 25 , 11
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 24 , 10
pro coh=8.00e5 tens=8.00e5 reg= 24 , 10
pro fric=30 dil= 5 reg= 24 , 10
pro perm=1.00e-14 porosity=0.3 reg= 24 , 10
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 24 , 9
pro coh=8.00e5 tens=8.00e5 reg= 24 , 9
pro fric=30 dil= 5 reg= 24 , 9
pro perm=1.00e-14 porosity=0.3 reg= 24 , 9
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 23 , 7
pro coh=8.00e5 tens=8.00e5 reg= 23 , 7
pro fric=30 dil= 5 reg= 23 , 7
pro perm=1.00e-14 porosity=0.3 reg= 23 , 7
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 22 , 5
pro coh=8.00e5 tens=8.00e5 reg= 22 , 5
pro fric=30 dil= 5 reg= 22 , 5
pro perm=1.00e-14 porosity=0.3 reg= 22 , 5
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 21 , 3
pro coh=8.00e5 tens=8.00e5 reg= 21 , 3
pro fric=30 dil= 5 reg= 21 , 3
pro perm=1.00e-14 porosity=0.3 reg= 21 , 3
; Fault
pro dens= 2300 bulk=4.70e9 shear=4.30e9 reg= 20 , 1
pro coh=8.00e5 tens=8.00e5 reg= 20 , 1
pro fric=30 dil= 5 reg= 20 , 1
pro perm=1.00e-14 porosity=0.3 reg= 20 , 1

; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 i=45 j=50
pro coh=2.7e7 tens=2.00e6 i=45 j=50
pro fric=27 dil= 4 i=45 j=50
pro perm=1.00e-19 porosity=0.3 i=45 j=50
; Sandstone
pro dens= 2400 bulk=2.68e10 shear=7.0e9 i=58 j=80
pro coh=2.7e7 tens=2.00e6 i=58 j=80
pro fric=27 dil= 4 i=58 j=80
pro perm=1.00e-19 porosity=0.3 i=58 j=80
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=38 j=40,41
pro coh=3.47e7 tens=2.00e6 i=38 j=40,41
pro fric=32 dil= 4 i=38 j=40,41
pro perm=1.00e-16 porosity=0.3 i=38 j=40,41
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=41 j=45
pro coh=3.47e7 tens=2.00e6 i=41 j=45
pro fric=32 dil= 4 i=41 j=45
pro perm=1.00e-16 porosity=0.3 i=41 j=45
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=36 j=31
pro coh=3.47e7 tens=2.00e6 i=36 j=31
pro fric=32 dil= 4 i=36 j=31
pro perm=1.00e-16 porosity=0.3 i=36 j=31
; Siltstone
pro dens= 2450 bulk=1.56e10 shear=1.08e10 i=20 j=45
pro coh=3.47e7 tens=2.00e6 i=20 j=45
pro fric=32 dil= 4 i=20 j=45
pro perm=1.00e-16 porosity=0.3 i=20 j=45
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 25 , j=14,16
pro coh=3.84e7 tens=8.00e5 i= 25 , j=14,16
pro fric=14 dil= 1 i= 25 , j=14,16
pro perm=1.00e-19 porosity=0.2 i= 25 , j=14,16

```

```

; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 26 , j=16
pro coh=3.84e7 tens=8.00e5 i= 26 , j=16
pro fric=14 dil= 1 i= 26 , j=16
pro perm=1.00e-19 porosity=0.2 i= 26 , j=16
; Shale (ore zone)
pro dens= 2500 bulk=2.2e11 shear=1.66e11 i= 22 , j=21
pro coh=3.84e8 tens=2.00e5 i= 22 , j=21
pro fric=14 dil= 5 i= 22 , j=21
pro perm=1.00e-15 porosity=0.2 i= 22 , j=21
; Shale (ore zone)
pro dens= 2500 bulk=2.2e11 shear=1.66e11 i= 33 , j=25
pro coh=3.84e8 tens=2.00e5 i= 33 , j=25
pro fric=14 dil= 5 i= 33 , j=25
pro perm=1.00e-15 porosity=0.2 i= 33 , j=25
; Shale (ore zone)
pro dens= 2500 bulk=2.2e11 shear=1.66e11 i= 29 , j=22
pro coh=3.84e8 tens=2.00e5 i= 29 , j=22
pro fric=14 dil= 5 i= 29 , j=22
pro perm=1.00e-15 porosity=0.2 i= 29 , j=22
; Shale
pro dens= 2500 bulk=8.8e9 shear=4.3e9 i= 21 , j=1
pro coh=3.84e7 tens=8.00e5 i= 21 , j=1
pro fric=14 dil= 1 i= 21 , j=1
pro perm=1.00e-19 porosity=0.2 i= 21 , j=1
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 i=24,28 j=20
pro coh=3.6e7 tens=8.00e5 i=24,28 j=20
pro fric=23 dil= 2 i=24,28 j=20
pro perm=5.00e-16 porosity=0.3 i=24,28 j=20
; Siltstone / Shale
pro dens= 2500 bulk=1.0e10 shear=7.5e9 i=34 , j=27
pro coh=3.6e7 tens=8.00e5 i=34 , j=27
pro fric=23 dil= 2 reg= i=34 , j=27
pro perm=5.00e-16 porosity=0.3 i=34 , j=27
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 i=31 , j=21
pro coh=3.6e7 tens=8.00e5 i=31 , j=21
pro fric=23 dil= 2 i=31 , j=21
pro perm=1.00e-18 porosity=0.2 i=31 , j=21
; Siltstone / Mudstone
pro dens= 2600 bulk=1.0e10 shear=7.5e9 i=27 , j=18
pro coh=3.6e7 tens=8.00e5 i=27 , j=18
pro fric=23 dil= 2 i=27 , j=18
pro perm=1.00e-18 porosity=0.2 i=27 , j=18
;------END OF PROPERTIES-----

def ini_stress
hh1 = 0.5*abs(y(1,2) - y(1,1))
surf_load = -2.5e3*9.8*2500
str_add = hh1*9.8*2700
bot_str = (-1.0)*(2.9e3*9.8*2500 - str_add)
top_str = (-1.0)*(2.5e3*9.8*2500 + str_add)

str_var = top_str - bot_str

command
ini sxx bot_str var=0,str_var i=1,80 j=1,80
ini syy bot_str var=0,str_var i=1,80 j=1,80
ini szz bot_str var=0,str_var i=1,80 j=1,80
ini sxy = 0.0
end_command

end
ini_stress

apply ns surf_load i=1,81 j=81

def hydro_pp

surf_pp = 2.5e3*9.8*1000 + 1e5 ;pp (2.5km) + pp (atmospheric loading)
loop i (1,igp)
loop j (1,jgp)

```

```

if j = jgp Then
;sss2 = 0
sss2 = surf_pp
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa + surf_pp
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
;
;
;
ini sat 1
fix sat

;fix pp j=81
;
set gravity=9.8
;
set large
;
;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=40 j=40
;hist 3 pp i=40 j=40

hist 3 pp i=10 j=18;sst/mud
hist 4 pp i=10 j=20;lower sst/sh
hist 5 pp i=10 j=22;shale
hist 6 pp i=10 j=26;higher sst/sh
hist 7 pp i=10 j=28;sst cap

;Movie every 500 steps
plot pp fill
sav m2d_ini.sav
movie on file m2d.dcx step 500

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTLING
fix x i=1
fix x i=81
fix y j=1

; Gravity settling
STEP 1500

;Set fluid on run to equilibrium
set flow on
pl pp fi fl bl
STEP 1500

;***Fish function to set overpressure from j=45 to j=1****
def overpress_pp
surf_pp = 3.0e3*9.8*2700 + 1e5 ;pp (3km) + pp (atmospheric loading)
loop i (1,i,igp)
loop j (1,45)
if j < 45 Then
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 2700 * 9.8 * aaa + surf_pp
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
overpress_pp
*
;
sav m2d_overpress.sav

```

```
;FISH FUNCTION TO STORE THE ORIGINAL PERMEABILITIES
;IN THE EXTRA VARIABLE ex_9
```

```
def store_perm_isotropic
  loop i1 (1,izones)
    loop j1 (1,jzones)
      ex_9(i1,j1) = k11(i1,j1)
    end_loop
  end_loop
end
store_perm_isotropic
;
```

```
;FISH function to test each zone and set it's
;permeability to an order of magnitude higher than it's original
;value if it is at yield (according to the FLAC state variables).
```

```
def yld_pincr1ordermag_isotropic

  WHILE_STEPPING
  incrval = 10.0 ; value to increment the permability by, 0.1 = 10%

  loop i1 (1,izones)
    loop j1 (1,jzones)
      case_of state(i1,j1)
        case 1 ; at yield in shear
          k11(i1,j1) = ex_9(i1,j1) * incrval
          k12(i1,j1) = 0.0
          k22(i1,j1) = ex_9(i1,j1) * incrval
        case 2 ; was at yield, but not now
          k11(i1,j1) = ex_9(i1,j1)
          k12(i1,j1) = 0.0
          k22(i1,j1) = ex_9(i1,j1)
        case 3 ; at yield in tension
          k11(i1,j1) = ex_9(i1,j1) * incrval
          k12(i1,j1) = 0.0
          k22(i1,j1) = ex_9(i1,j1) * incrval
        end_case
      end_loop
    end_loop
  end
;
```

```
free x
free y

;Compression
ini xvel 0.0008 var=-0.0016 ,0 i=1, 81 j=1, 81
fix x i=1
fix x i= 81
fix y j=1
;
```

```
step 2500
save m2d_1.sav ; 1 % compression
step 2500
```



```

save m2d_2.sav ; 2 % compression
step 2500
save m2d_3.sav ; 3 % compression
step 2500
save m2d_4.sav ; 4 % compression
step 2500
save m2d_5.sav ; 5 % compression
step 2500
save m2d_6.sav ; 6 % compression
step 2500
save m2d_7.sav ; 7 % compression
step 2500
save m2d_8.sav ; 8 % compression
step 2500
save m2d_9.sav ; 9 % compression
step 2500
save m2d_10.sav ; 10 % compression
step 2500
save m2d_11.sav ; 11 % compression
step 2500
save m2d_12.sav ; 12 % compression

return
stop

```

E Extension Models

E.1 Model 1a

```

FLAC Modelling Input File
:
config extra 4 gw
grid 120 80
gen 0.00e0,-8.00e3 0.00e0,0.00e0 1.20e4,0.00e0 1.20e4,-8.00e3 i=1,121 j=1,81
mark i=1
mark j=1
mark i = 121
mark j = 81
:
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3 ; to be elaborated below
;; 1 mech step = 1 fluid step;
set nmech 1 ngw 1 flow on
*****

tab 1 0 ,-4000 12000 ,-4000
;
;tab 2 0 ,-2000 12000 ,-2000
;
;tab 3 3000 ,-7000 8500 ,-1000 8800 ,-1000 3300 ,-7000

gen tab 1
;gen line 3000 -7000 8500 ,-1000
;;gen line 8500 ,-1000 8800 ,-1000
;gen line 8800 ,-1000 3300 ,-7000
;gen line 3300 ,-7000 3000 -7000
;gen tab 2
;gen tab 3
;

; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 reg= 20 , 64
pro coh=4.00e6 tens=2.00e6 reg= 20 , 64
pro fric=30 dil= 4 reg= 20 , 64
pro perm=1.00e-10 porosity=0.3 reg= 20 , 64
; Granite

```

```

pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 18 , 34
pro coh=4.00e6 tens=2.00e6 reg= 18 , 34
pro fric=30 dil= 4 reg= 18 , 34
pro perm=2.00e-13 porosity=0.3 reg= 18 , 34
;
def hydro_pp
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
;
ini sat 1
fix sat
fix pp j=81
;
set gravity=9.8
set large
;
;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=60 j=40
hist 3 pp i=60 j=5; basement
hist 4 pp i=60 j=40; middle
hist 5 pp i=60 j=80; top

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTling
fix x i=1
fix x i=121
fix y j=1 ;

plot pp fill
sav block1_ini.sav

;Create Movie files every 10000 steps
plot pp fill
movie on file block1.dcx step 10000
;

;RUN TO GRAVITY SETTling
STEP 5000
;SET FLUID FLOW ON AND RUN TO EQUILIBRIUM
set flow on

pl pp fi fl bl
sav block1_grav.sav
step 5000
sav block1_flow.sav
;
free x
free y
ini xvel -0.0024 var= 0.0048 ,0 i=1, 121 j=1, 81 :

fix x i=1
fix x i=121
fix y j=1

his reset

; fish function for determining the sum of the stresses at each end of the model, for plotting as a history.

def stress_sum
while_stepping
sum_left = 0.0
sum_right = 0.0
sum_ave = 0.0

```

```

loop j (1,jzones)
depth_corr = 2700.0*10.0
sum_left = -(sum_left + sxx(1,j)-depth_corr*(y(1,j)-y(1,1)))
sum_right = -(sum_right + sxx(120,j)-depth_corr*(y(120,j)-y(120,1)))
sum_ave = (sum_left+sum_right)/2.0
end_loop
end

hist 1 unbalanced
hist 2 ydispl i=60 j=30
his 3 sum_left
his 4 sum_right
his 5 sum_ave
his 6 xdispl i 1 j 30
his 7 xdispl i 121 j 30
hist 8 pp i=60 j=5; basement
hist 9 pp i=60 j=40; middle
hist 10 pp i=60 j=80; top

step 50000
save block1_1.sav; 2 % deformation
step 50000
save block1_2.sav; 4 % deformation
step 50000
save block1_3.sav; 6 % deformation
step 50000
save block1_4.sav; 8 % deformation
step 50000
save block1_5.sav; 10 % deformation
pause
return
stop

```

E.2 Model 1b

```

FLAC Modelling Input File
;
config extra 4 gw
grid 120 80
gen 0,00e0,-8.00e3 0.00e0,0.00e0 1.20e4,0.00e0 1.20e4,-8.00e3 i=1,121 j=1,81
mark i=1
mark j=1
mark i = 121
mark j = 81
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3 ; to be elaborated below
;; 1 mech step = 1 fluid step;
set nmech 1 ngw 10 flow on
*****
tab 1 0,-4000 12000,-4000
;
;tab 2 0,-2000 12000,-2000
;
;tab 3 3000,-7000 8500,-1000 8800,-1000 3300,-7000

gen tab 1
;gen line 3000 -7000 8500,-1000
;;gen line 8500,-1000 8800,-1000
;gen line 8800,-1000 3300,-7000
;gen line 3300,-7000 3000 -7000
;gen tab 2
;gen tab 3
;
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 reg= 20 , 64
pro coh=4.00e6 tens=2.00e6 reg= 20 , 64
pro fric=30 dil= 4 reg= 20 , 64
pro perm=1.00e-10 porosity=0.3 reg= 20 , 64
; Granite

```

```

pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 18 , 34
pro coh=4.00e6 tens=2.00e6 reg= 18 , 34
pro fric=30 dil= 4 reg= 18 , 34
pro perm=2.00e-13 porosity=0.3 reg= 18 , 34
;
def hydro_pp
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
;
def litho_pp
loop i (1,igp)
loop j (1,41)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 2650 * 9.8 * aaa + 1e5
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
litho_pp
*

ini sat 1
fix sat
fix pp j=81
;
set gravity=9.8
set large
;
;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=60 j=40
hist 3 pp i=60 j=5; basement
hist 4 pp i=60 j=40; middle
hist 5 pp i=60 j=80; top

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTLING
fix x i=1
fix x i=121
fix y j=1 ;

plot pp fill
sav block2_10_ini.sav

;Create Movie files every 10000 steps
plot pp fill
movie on file block2_10.dcx step 10000
;

;RUN TO GRAVITY SETTLING
STEP 5000
;SET FLUID FLOW ON AND RUN TO EQUILIBRIUM
set flow on

pl pp fi fl bl
sav block2_10_grav.sav
step 5000

sav block2_10_flow.sav
free x

```

```

free y
ini xvel -0.0024 var= 0.0048 ,0 i=1, 121 j=1, 81 :

fix x i=1
fix x i=121
fix y j=1

his reset

; fish function for determining the sum of the stresses at each end of the model, for plotting as a history.
def stress_sum
while_stepping
sum_left = 0.0
sum_right = 0.0
sum_ave = 0.0
loop j (1,jzones)
depth_corr = 2700.0*10.0
sum_left = -(sum_left + sxx(1,j)-depth_corr*(y(1,j)-y(1,1)))
sum_right = -(sum_right + sxx(120,j)-depth_corr*(y(120,j)-y(120,1)))
sum_ave = (sum_left+sum_right)/2.0
end_loop
end

hist 1 unbalanced
hist 2 ydispl i=60 j=30
his 3 sum_left
his 4 sum_right
his 5 sum_ave
his 6 xdispl i 1 j 30
his 7 xdispl i 121 j 30
hist 8 pp i=60 j=5; basement
hist 9 pp i=60 j=40; middle
hist 10 pp i=60 j=80; top

step 50000
save block2_10_10_1.sav; 2 % deformation
step 50000
save block2_10_10_2.sav; 4 % deformation
step 10000
sav block2_10_10_2,1.sav
step 10000
sav block2_10_10_2,2.sav
step 10000
sav block2_10_10_2,3.sav
step 10000
sav block2_10_10_2,4.sav
step 10000
save block2_10_10_3.sav; 6 % deformation
step 10000
sav block2_10_10_3,1.sav
step 10000
sav block2_10_10_3,2.sav
step 10000
sav block2_10_10_3,3.sav
step 10000
sav block2_10_10_3,4.sav
step 10000
save block2_10_10_4.sav; 8 % deformation
step 50000
save block2_10_5.sav; 10 % deformation
step 50000
save block2_10_6.sav; 12 % deformation
step 50000
save block2_10_7.sav; 14 % deformation
step 50000
save block2_10_8.sav; 16 % deformation
step 50000
save block2_10_9.sav; 18 % deformation
step 50000
save block2_10_10.sav; 20 % deformation

return
stop

```

E.3 Model 2a

```

FLAC Modelling Input File
;
config extra 4 gw
grid 120 80
gen 0.00e0,-8.00e3 0.00e0,0.00e0 1.20e4,0.00e0 1.20e4,-8.00e3 i=1,121 j=1,81
mark i=1
mark j=1
mark i = 121
mark j = 81
;
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3 ; to be elaborated below
;; 1 mech step = 1 fluid step;
set nmech 1 ngw 1 flow on
*****
tab 1 0 ,-4000 12000 ,-4000
;
;tab 2 0 ,-2000 12000 ,-2000
;
;
tab 3 3000 ,-8000 8500 , 0 8800 , 0
tab 3 3300 ,-8000
;
gen tab 1
;gen tab 2
gen tab 3
;
; Moving the gridpoints i=63 j=41 at base i=60 j=80 at top of fault to straighten it out
ini x add 75 i=88 j=81
ini x add 25 i=58 j=41
ini x add -25 i=62 j=41

; Properties for each sub-regions
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 reg= 20 , 64
pro coh=4.00e6 tens=2.00e6 reg= 20 , 64
pro fric=30 dil= 4 reg= 20 , 64
pro perm=1.00e-10 porosity=0.3 reg= 20 , 64
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 reg= 90 , 64
pro coh=4.00e6 tens=2.00e6 reg= 90 , 64
pro fric=30 dil= 4 reg= 90 , 64
pro perm=1.00e-10 porosity=0.3 reg= 90 , 64
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 18 , 34
pro coh=4.00e6 tens=2.00e6 reg= 18 , 34
pro fric=30 dil= 4 reg= 18 , 34
pro perm=2.00e-13 porosity=0.3 reg= 18 , 34
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 60 , 34
pro coh=4.00e6 tens=2.00e6 reg= 60 , 34
pro fric=30 dil= 4 reg= 60 , 34
pro perm=2.00e-13 porosity=0.3 reg= 60 , 34
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 i= 34 j= 1
pro coh=4.00e6 tens=2.00e6 i= 34 j= 1
pro fric=30 dil= 4 i= 34 j= 1
pro perm=2.00e-13 porosity=0.3 i= 34 j= 1
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 i= 60 j= 40
pro coh=4.00e6 tens=2.00e6 i= 60 j= 40
pro fric=30 dil= 4 i= 60 j= 40
pro perm=2.00e-13 porosity=0.3 i= 60 j= 40
; Fault
pro dens= 2500 bulk=2.81e10 shear=1.69e9 reg= 52 , 30
pro coh=3.00e3 tens=1.50e6 reg= 52 , 30
pro fric=30 dil= 4 reg= 52 , 30
pro perm=1.00e-11 porosity=0.3 reg= 52 , 30
;Additional commands to sort out loose zones
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 i= 57 j= 40

```

```

pro coh=4.00e6 tens=2.00e6 i= 57 j= 40
pro fric=30 dil= 4 i= 57 j= 40
pro perm=2.00e-13 porosity=0.3 i= 57 j= 40
; Fault
pro dens= 2500 bulk=2.81e10 shear=1.69e9 reg= 61 , 42
pro coh=3.00e3 tens=1.50e6 reg= 61 , 42
pro fric=30 dil= 4 reg= 61 , 42
pro perm=1.00e-11 porosity=0.3 reg= 61 , 42
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 i= 62 j= 41
pro coh=4.00e6 tens=2.00e6 i= 62 j= 41
pro fric=30 dil= 4 i= 62 j= 41
pro perm=1.00e-10 porosity=0.3 i= 62 j= 41

;
def hydro_pp
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
;
ini sat 1
fix sat
fix pp j=81
;
set gravity=9.8
set large
;
;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=60 j=40
hist 3 pp i=60 j=5; basement
hist 4 pp i=60 j=40; middle
hist 5 pp i=60 j=80; top

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTling
fix x i=1
fix x i=121
fix y j=1 ;

plot pp fill
sav faultnb2_ini.sav

;Create Movie files every 10000 steps
plot pp fill
movie on file faultnb2.dcx step 10000
;

;RUN TO GRAVITY SETTling
STEP 5000
;SET FLUID FLOW ON AND RUN TO EQUILIBRIUM
set flow on

pl pp fi fl bl
sav faultnb2_grav.sav
step 5000

sav faultnb2_flow.sav
;
free x
free y

ini xvel -0.0024 var= 0.0048 , 0 i=1, 121 j=1, 81 :
fix x i=1
fix x i=121

```

```

fix y j=1

his reset

; fish function for determining the sum of the stresses at each end of the model, for plotting as a history.
def stress_sum
while_stepping
sum_left = 0.0
sum_right = 0.0
sum_ave = 0.0
loop j (1,jzones)
depth_corr = 2700.0*10.0
sum_left = -(sum_left + sxx(1,j)-depth_corr*(y(1,j)-y(1,1)))
sum_right = -(sum_right + sxx(120,j)-depth_corr*(y(120,j)-y(120,1)))
sum_ave = (sum_left+sum_right)/2.0
end_loop
end

hist 1 unbalanced
hist 2 ydispl i=60 j=30
his 3 sum_left
his 4 sum_right
his 5 sum_ave
his 6 xdispl i 1 j 30
his 7 xdispl i 121 j 30
hist 8 pp i=60 j=5; basement
hist 9 pp i=60 j=40; middle
hist 10 pp i=60 j=80; top

step 50000
save faultnb2_1.sav; 2 % deformation
step 50000
save faultnb2_2.sav; 4 % deformation
step 50000
save faultnb2_3.sav; 6 % deformation
step 50000
save faultnb2_4.sav; 8 % deformation
step 50000
save faultnb2_5.sav; 10 % deformation
step 50000
save faultnb2_6.sav; 12 % deformation
step 50000
save faultnb2_7.sav; 14 % deformation

return
stop

```

E.4 Model 2b

```

FLAC Modelling Input File
;
config extra 4 gw
grid 120 80
gen 0.00e0,-8.00e3 0.00e0,0.00e0 1.20e4,0.00e0 1.20e4,-8.00e3 i=1,121 j=1,81
mark i=1
mark j=1
mark i = 121
mark j = 81
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3 ; to be elaborated below
;; 1 mech step = 1 fluid step;
set nmech 1 ngw 1 flow on
*****
tab 1 0,-4000 12000,-4000
;
;tab 2 0,-2000 12000,-2000
;
;tab 3 3000,-7000 8500,-1000 8800,-1000 3300,-7000
gen tab 1
gen line 3000 -7000 8500,-1000

```



```

gen line 8500 ,-1000 8800 ,-1000
gen line 8800 ,-1000 3300 ,-7000
gen line 3300 ,-7000 3000 -7000

;gen tab 2
;gen tab 3
;
; Moving the gridpoints i=63 j=41 at base i=60 j=80 at top of fault to straighten it out
;ini x add 75 i=88 j=81
;ini x add 25 i=58 j=41
;ini x add -25 i=62 j=41

; Properties for each sub-regions:
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 reg= 20 , 64
pro coh=4.00e6 tens=2.00e6 reg= 20 , 64
pro fric=30 dil= 4 reg= 20 , 64
pro perm=1.00e-10 porosity=0.3 reg= 20 , 64
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 reg= 90 , 64
pro coh=4.00e6 tens=2.00e6 reg= 90 , 64
pro fric=30 dil= 4 reg= 90 , 64
pro perm=1.00e-10 porosity=0.3 reg= 90 , 64
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 18 , 34
pro coh=4.00e6 tens=2.00e6 reg= 18 , 34
pro fric=30 dil= 4 reg= 18 , 34
pro perm=2.00e-13 porosity=0.3 reg= 18 , 34
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 60 , 34
pro coh=4.00e6 tens=2.00e6 reg= 60 , 34
pro fric=30 dil= 4 reg= 60 , 34
pro perm=2.00e-13 porosity=0.3 reg= 60 , 34

;Additional commands to sort out loose zones

; Fault
pro dens= 2500 bulk=2.81e10 shear=1.69e9 reg= 72 , 54
pro coh=3.00e3 tens=1.50e6 reg= 72 , 54
pro fric=30 dil= 4 reg= 72 , 54
pro perm=1.00e-11 porosity=0.3 reg= 72 , 54
; Fault
pro dens= 2500 bulk=2.81e10 shear=1.69e9 reg= 41 , 20
pro coh=3.00e3 tens=1.50e6 reg= 41 , 20
pro fric=30 dil= 4 reg= 41 , 20
pro perm=1.00e-11 porosity=0.3 reg= 41 , 20
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 18 , 34
pro coh=4.00e6 tens=2.00e6 reg= 18 , 34
pro fric=30 dil= 4 reg= 18 , 34
pro perm=2.00e-13 porosity=0.3 reg= 18 , 34
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 60 , 34
pro coh=4.00e6 tens=2.00e6 reg= 60 , 34
pro fric=30 dil= 4 reg= 60 , 34
pro perm=2.00e-13 porosity=0.3 reg= 60 , 34
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 i= 62 j= 41
pro coh=4.00e6 tens=2.00e6 i= 62 j= 41
pro fric=30 dil= 4 i= 62 j= 41
pro perm=1.00e-10 porosity=0.3 i= 62 j= 41
; Fault
pro dens= 2500 bulk=2.81e10 shear=1.69e9 reg= 41 , 20
pro coh=3.00e3 tens=1.50e6 reg= 41 , 20
pro fric=30 dil= 4 reg= 41 , 20
pro perm=1.00e-11 porosity=0.3 reg= 41 , 20
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 i=57,58 j=40
pro coh=4.00e6 tens=2.00e6 i=57,58 j=40
pro fric=30 dil= 4 i=57,58 j=40
pro perm=2.00e-13 porosity=0.3 i=57,58 j=40
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 i=61,62 j= 41
pro coh=4.00e6 tens=2.00e6 i=61,62 j= 41
pro fric=30 dil= 4 i=61,62 j= 41

```

```

pro perm=1.00e-10 porosity=0.3 i=61,62 j= 41

;
def hydro_pp
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
;

ini sat 1
fix sat
fix pp j=81
;
set gravity=9.8
set large
;
;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=60 j=40
hist 3 pp i=60 j=5; basement
hist 4 pp i=60 j=40; middle
hist 5 pp i=60 j=80; top

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTLING
fix x i=1
fix x i=121
fix y j=1 ;

plot pp fill
sav faultnb4_ini.sav

;Create Movie files every 10000 steps
plot pp fill
movie on file faultnb4.dcx step 10000
;

;RUN TO GRAVITY SETTLING
STEP 5000
;SET FLUID FLOW ON AND RUN TO EQUILIBRIUM
set flow on

pl pp fi fl bl
sav faultnb4_grav.sav
step 5000

sav faultnb4_flow.sav

free x
free y
ini xvel -0.0024 var= 0.0048 ,0 i=1, 121 j=1, 81 :
fix x i=1
fix x i=121
fix y j=1

his reset

; fish function for determining the sum of the stresses at each end of the model, for plotting as a history.
def stress_sum
while_stepping

sum_left = 0.0
sum_right = 0.0
sum_ave = 0.0

```

```

loop j (1,jzones)
depth_corr = 2700.0*10.0
sum_left = -(sum_left + sxx(1,j)-depth_corr*(y(1,j)-y(1,1)))
sum_right = -(sum_right + sxx(120,j)-depth_corr*(y(120,j)-y(120,1)))
sum_ave = (sum_left+sum_right)/2.0
end_loop
end

hist 1 unbalanced
hist 2 ydispl i=60 j=30
his 3 sum_left
his 4 sum_right
his 5 sum_ave
his 6 xdispl i 1 j 30
his 7 xdispl i 121 j 30
hist 8 pp i=60 j=5; basement
hist 9 pp i=60 j=40; middle
hist 10 pp i=60 j=80; top

step 50000
save faultnb4_1.sav; 2 % deformation
step 50000
save faultnb4_2.sav; 4 % deformation
step 50000
save faultnb4_3.sav; 6 % deformation
step 50000
save faultnb4_4.sav; 8 % deformation
step 50000
save faultnb4_5.sav; 10 % deformation
step 50000
save faultnb4_6.sav; 12 % deformation
step 50000
save faultnb4_7.sav; 14 % deformation
step 50000
save faultnb4_8.sav; 16 % deformation
step 50000
save faultnb4_9.sav; 18 % deformation
step 50000
save faultnb4_10.sav; 20 % deformation

return
stop

```

E.5 Model 2c

FLAC Modelling Input File

```

;
config extra 4 gw
grid 120 80
gen 0.00e0,-8.00e3 0.00e0,0.00e0 1.20e4,0.00e0 1.20e4,-8.00e3 i=1,121 j=1,81
mark i=1
mark j=1
mark i = 121
mark j = 81
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3 ; to be elaborated below
;; 1 mech step = 1 fluid step;
set nmech 1 ngw 1 flow on
*****
tab 1 0,-4000 12000,-4000
;
;tab 2 0,-2000 12000,-2000
;
;tab 3 3000,-7000 8500,-1000 8800,-1000 3300,-7000

gen tab 1
gen line 3000 -7000 8500 ,-1000
gen line 8500 ,-1000 8800 ,-1000
gen line 8800 ,-1000 3300 ,-7000
gen line 3300 ,-7000 3000 -7000

```

```

;gen tab 2
;gen tab 3
;
; Moving the gridpoints i=63 j=41 at base i=60 j=80 at top of fault to straighten it out
;ini x add 75 i=88 j=81
;ini x add 25 i=58 j=41
;ini x add -25 i=62 j=41

; Properties for each sub-regions:
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 reg= 20 , 64
pro coh=4.00e6 tens=2.00e6 reg= 20 , 64
pro fric=30 dil= 4 reg= 20 , 64
pro perm=1.00e-10 porosity=0.3 reg= 20 , 64
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 reg= 90 , 64
pro coh=4.00e6 tens=2.00e6 reg= 90 , 64
pro fric=30 dil= 4 reg= 90 , 64
pro perm=1.00e-10 porosity=0.3 reg= 90 , 64
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 18 , 34
pro coh=4.00e6 tens=2.00e6 reg= 18 , 34
pro fric=30 dil= 4 reg= 18 , 34
pro perm=2.00e-13 porosity=0.3 reg= 18 , 34
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 60 , 34
pro coh=4.00e6 tens=2.00e6 reg= 60 , 34
pro fric=30 dil= 4 reg= 60 , 34
pro perm=2.00e-13 porosity=0.3 reg= 60 , 34

;Additional commands to sort out loose zones
; Fault
pro dens= 2500 bulk=2.81e10 shear=1.69e9 reg= 72 , 54
pro coh=3.00e3 tens=1.50e6 reg= 72 , 54
pro fric=30 dil= 4 reg= 72 , 54
pro perm=1.00e-11 porosity=0.3 reg= 72 , 54
; Fault
pro dens= 2500 bulk=2.81e10 shear=1.69e9 reg= 41 , 20
pro coh=3.00e3 tens=1.50e6 reg= 41 , 20
pro fric=30 dil= 4 reg= 41 , 20
pro perm=1.00e-11 porosity=0.3 reg= 41 , 20
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 18 , 34
pro coh=4.00e6 tens=2.00e6 reg= 18 , 34
pro fric=30 dil= 4 reg= 18 , 34
pro perm=2.00e-13 porosity=0.3 reg= 18 , 34
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 60 , 34
pro coh=4.00e6 tens=2.00e6 reg= 60 , 34
pro fric=30 dil= 4 reg= 60 , 34
pro perm=2.00e-13 porosity=0.3 reg= 60 , 34
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 i= 62 j= 41
pro coh=4.00e6 tens=2.00e6 i= 62 j= 41
pro fric=30 dil= 4 i= 62 j= 41
pro perm=1.00e-10 porosity=0.3 i= 62 j= 41
; Fault
pro dens= 2500 bulk=2.81e10 shear=1.69e9 reg= 41 , 20
pro coh=3.00e3 tens=1.50e6 reg= 41 , 20
pro fric=30 dil= 4 reg= 41 , 20
pro perm=1.00e-11 porosity=0.3 reg= 41 , 20
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 i=57,58 j=40
pro coh=4.00e6 tens=2.00e6 i=57,58 j=40
pro fric=30 dil= 4 i=57,58 j=40
pro perm=2.00e-13 porosity=0.3 i=57,58 j=40
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 i=61,62 j= 41
pro coh=4.00e6 tens=2.00e6 i=61,62 j= 41
pro fric=30 dil= 4 i=61,62 j= 41
pro perm=1.00e-10 porosity=0.3 i=61,62 j= 41
;
def hydro_pp
loop i (1,igp)
loop j (1,jgp)

```

```

if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
;

def litho_pp
loop i (1,igp)
loop j (1,41)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 2650 * 9.8 * aaa + 1e5
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
litho_pp
*
;

ini sat 1
fix sat
fix pp j=81
;
set gravity=9.8
set large
;
;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=60 j=40
hist 3 pp i=60 j=5; basement
hist 4 pp i=60 j=40; middle
hist 5 pp i=60 j=80; top

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTLING
fix x i=1
fix x i=121
fix y j=1 ;
plot pp fill
sav faultnb3_ini.sav

;Create Movie files every 10000 steps
plot pp fill
movie on file faultnb3.dcx step 10000
;

;RUN TO GRAVITY SETTLING
STEP 5000
;SET FLUID FLOW ON AND RUN TO EQUILIBRIUM
set flow on
pl pp fi fl bl
sav faultnb3_grav.sav
step 5000
sav faultnb3_flow.sav
;

free x
free y
ini xvel -0.0024 var= 0.0048 ,0 i=1, 121 j=1, 81 :
fix x i=1
fix x i=121
fix y j=1

```

```

his reset

; fish function for determining the sum of the stresses at each end of the model, for plotting as a history.
def stress_sum
while_stepping
sum_left = 0.0
sum_right = 0.0
sum_ave = 0.0
loop j (1,jzones)
depth_corr = 2700.0*10.0
sum_left = -(sum_left + sxx(1,j)-depth_corr*(y(1,j)-y(1,1)))
sum_right = -(sum_right + sxx(120,j)-depth_corr*(y(120,j)-y(120,1)))
sum_ave = (sum_left+sum_right)/2.0
end_loop
end

hist 1 unbalanced
hist 2 ydispl i=60 j=30
his 3 sum_left
his 4 sum_right
his 5 sum_ave
his 6 xdispl i 1 j 30
his 7 xdispl i 121 j 30
hist 8 pp i=60 j=5; basement
hist 9 pp i=60 j=40; middle
hist 10 pp i=60 j=80; top

step 50000
save faultnb3_1.sav; 2 % deformation
step 50000
save faultnb3_2.sav; 4 % deformation
step 50000
save faultnb3_3.sav; 6 % deformation
step 50000
save faultnb3_4.sav; 8 % deformation
step 50000
save faultnb3_5.sav; 10 % deformation
step 50000
save faultnb3_6.sav; 12 % deformation
step 50000
save faultnb3_7.sav; 14 % deformation
step 50000
save faultnb3_8.sav; 16 % deformation
step 50000
save faultnb3_9.sav; 18 % deformation
step 50000
save faultnb3_10.sav; 20 % deformation

return
stop

```

E.6 Model 2d

```

FLAC Modelling Input File
;
config extra 4 gw
grid 120 80
gen 0.00e0,-8.00e3 0.00e0,0.00e0 1.20e4,0.00e0 1.20e4,-8.00e3 i=1,121 j=1,81
mark i=1
mark j=1
mark i = 121
mark j = 81
;
*****
model mohr
water bulk 2e9 dens 1000
prop poro=0.3 ; to be elaborated below
;; 1 mech step = 1 fluid step;
set nmech 1 ngw 1 flow on
*****
tab 1 0 ,-4000 12000 ,-4000
;

```

```

;tab 2 0,-2000 12000,-2000
;tab 3 3000,-8000 6000,-4000 6300,-4000
;tab 3 3300,-8000
;
;gen tab 1
;gen tab 2
;gen tab 3
;
; Moving the gridpoints i=63 j=41 at base i=60 j=80 at top of fault to straighten it out
;ini x add 75 i=63 j=41

; Properties for each sub-regions: NEW PERM PROPS !!!!!
; Sandstone
pro dens= 2400 bulk=3.20e10 shear=1.92e10 reg= 20 , 64
pro coh=4.00e6 tens=2.00e6 reg= 20 , 64
pro fric=30 dil= 4 reg= 20 , 64
pro perm=1.00e-10 porosity=0.3 reg= 20 , 64
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 18 , 34
pro coh=4.00e6 tens=2.00e6 reg= 18 , 34
pro fric=30 dil= 4 reg= 18 , 34
pro perm=2.00e-13 porosity=0.3 reg= 18 , 34
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 reg= 60 , 34
pro coh=4.00e6 tens=2.00e6 reg= 60 , 34
pro fric=30 dil= 4 reg= 60 , 34
pro perm=2.00e-13 porosity=0.3 reg= 60 , 34
; Fault
pro dens= 2500 bulk=2.81e10 shear=1.69e9 reg= 54 , 30
pro coh=3.00e3 tens=1.50e6 reg= 54 , 30
pro fric=30 dil= 4 reg= 54 , 30
pro perm=1.00e-11 porosity=0.3 reg= 54 , 30
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 i= 34 j= 1
pro coh=4.00e6 tens=2.00e6 i= 34 j= 1
pro fric=30 dil= 4 i= 34 j= 1
pro perm=2.00e-13 porosity=0.3 i= 34 j= 1
; Granite
pro dens= 2650 bulk=4.95e10 shear=2.97e10 i= 60 j= 40
pro coh=4.00e6 tens=2.00e6 i= 60 j= 40
pro fric=30 dil= 4 i= 60 j= 40
pro perm=2.00e-13 porosity=0.3 i= 60 j= 40
;
def hydro_pp
loop i (1,igp)
loop j (1,jgp)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 1000 * 9.8 * aaa
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
hydro_pp
*
;
def litho_pp
loop i (1,igp)
loop j (1,41)
if j = jgp Then
sss2 = 0
else
aaa = abs(y(i, j) - y(i, jgp))
sss2 = 2650 * 9.8 * aaa + 1e5
end_if
gpp(i, j) = sss2
end_loop
end_loop
end
litho_pp
*
;

```

```

ini sat 1
fix sat
fix pp j=81
;
set gravity=9.8
;
set large
;
;SET UP A COUPLE OF HISTORIES
hist 1 unbalanced
hist 2 ydispl i=60 j=40
hist 3 pp i=60 j=5; basement
hist 4 pp i=60 j=40; middle
hist 5 pp i=60 j=42; base of cover
hist 4 pp i=60 j=80; top

;FIX THE SIDES OF THE MODEL TO RUN TO GRAVITY SETTling
fix x i=1
fix x i=121
fix y j=1 ;

plot pp fill
sav faultnb1_ini.sav

;Create Movie files every 10000 steps
plot pp fill
movie on file faultnb1.dcx step 10000
;

;RUN TO GRAVITY SETTling
STEP 5000
;SET FLUID FLOW ON AND RUN TO EQUILIBRIUM
set flow on

pl pp fi fl bl
sav faultnb1_grav.sav
step 5000

sav faultnb1_flow.sav
;
free x
free y
ini xvel -0.0024 var= 0.0048 ,0 i=1, 121 j=1, 81 :

fix x i=1
fix x i=121
fix y j=1

step 50000
save faultnb1_1.sav; 2 % deformation
step 50000
save faultnb1_2.sav; 4 % deformation
step 50000
save faultnb1_3.sav; 6 % deformation
step 50000
save faultnb1_4.sav; 8 % deformation
step 50000
save faultnb1_5.sav; 10 % deformation
step 50000
save faultnb1_6.sav; 12 % deformation
step 50000
save faultnb1_7.sav; 14 % deformation
step 50000
save faultnb1_8.sav; 16 % deformation
step 50000
save faultnb1_9.sav; 18 % deformation
step 50000
save faultnb1_10.sav; 20 % deformation

return
stop

```


Appendix 2

UDEC numerical code

(note: Geometry was constructed by digital tracing in Corel Draw, then using a grid, coordinates at each point were recorded and code was entered by user. Geometry files are only included in Models1a and 2a due to the extensive code.)

U UDEC Models

U.1 Model 1a – dry model $\sigma_1 = 90^\circ$

```
>1530Ma (Map Interp)MODEL 1 Old Granites- DRY MODEL
```

```
prop mat=1 dens 2850 bulk 25e9 shear 25e9 cohesion 10e6 tens 5e6 fric 31 dil 4
```

```
prop mat=2 dens 2650 bulk 49e9 shear 27e9 cohesion 20e6 tens 10e6 fric 37 dil 5
```

```
:contact properties
```

```
prop jmat=1 jkn 5e6 jks 1e3 jcoh 4e2 jtens 2e6 jfri 30 jdil 5
```

```
:prop jmat=1 jper 300 azero 0.05 ares 0.03
```

```
prop jmat=2 jkn 5e9 jks 1e5 jcoh 10e2 jtens 3e6 jfri 35 jdil 5
```

```
:prop jmat=2 jper 238 azero 0.03 ares 0.01
```

```
:Pseudo joints
```

```
prop jmat=5 jkn 100e9 jks 40e9 jcoh 190e10 jtens 190e10 jdil 0
```

```
:prop jmat=5 jper 0 azero 0 ares 0
```

```
round 100
```

```
block 0,0 0,200000 124000,200000 124000,0
```

```
:*****(Geometry File Start)*****
```

```
crack 1000 200000 1500 192000;1-2
crack 1500 192000 1000 191000;2-3
crack 1000 191000 0 189000;3-4
crack 6500 200000 5500 199000;7-6
crack 5500 199000 4000 198000;6-5
crack 4000 198000 1500 192000;5-2
crack 5500 199000 6000 193000;6-8
crack 6000 193000 4000 186000;8-9
crack 4000 186000 4000 180000;9-10
crack 4000 180000 4500 176000;10-11
crack 4500 176000 2000 171000;11-12
crack 4000 198000 3500 188000;5-17
crack 3500 188000 2500 184000;17-18
crack 2500 184000 2500 175000;18-19
crack 2500 175000 2000 171000;19-12
crack 2000 171000 1500 170000;12-13
crack 1500 170000 1500 160000;13-14
crack 1500 160000 5000 155000;14-15
crack 5000 155000 2000 150000;15-16
crack 2000 150000 0 148000;16-20
crack 21500 200000 21500 189000;21-22
crack 21500 189000 20000 182000;22-23
crack 27500 200000 23000 185000;25-26
crack 23000 185000 20000 182000;26-23
crack 20000 182000 19500 179000;23-24
crack 19500 179000 13500 168000;24-27
crack 13500 168000 10500 165000;27-28
crack 10500 165000 9500 162000;28-29
crack 9500 162000 5000 155000;29-15
crack 9500 162000 10000 160000;29-30
crack 10000 160000 6500 154000;30-31
crack 6500 154000 4000 149000;31-32
crack 4000 149000 0 147000;32-33
crack 4000 149000 0 141000;32-34
```

crack	69000	200000	64000	181000;35-36
crack	64000	181000	62000	181000;36-37 gr1 bound centr:57000,60000,175000,180000
crack	62000	181000	61000	180000;37-38 gr1 bound
crack	61000	180000	54500	180000;38-39 gr1 bound
crack	54500	180000	53000	179500;39-40 gr1 bound
crack	53000	179500	53000	176000;40-41 gr1 bound
crack	53000	176000	54000	175000;41-42 gr1 bound
crack	54000	175000	56000	173000;42-43 gr1 bound
crack	56000	173000	57000	171000;43-44 gr1 bound
crack	57000	171000	58000	172000;44-45 gr1 bound
crack	58000	172000	60000	172500;45-46 gr1 bound
crack	60000	172500	59500	173500;46-47 gr1 bound
crack	59500	173500	58000	173000;47-48 gr1 bound
crack	58000	173000	57000	173500;48-49 gr1 bound
crack	57000	173500	57500	175000;49-50 gr1 bound
crack	57500	175000	61000	175000;50-51 gr1 bound
crack	61000	175000	63000	177000;51-52 gr1 bound
crack	63000	177000	64000	181000;52-36 gr1 bound
crack	54000	175000	52000	176000;42-53
crack	52000	176000	47000	179000;53-54
crack	47000	179000	45000	179000;54-55
crack	45000	179000	41000	181000;55-56
crack	41000	181000	38000	179000;56-57
crack	38000	179000	38500	173000;57-58
crack	38500	173000	37000	169000;58-59
crack	37000	169000	25000	164000;59-60
crack	25000	164000	21000	163000;60-61
crack	21000	163000	11000	158000;61-62
crack	11000	158000	8000	145000;62-63
crack	8000	145000	0	130000;63-64
crack	38500	173000	42000	170000;58-65
crack	42000	170000	42000	163000;65-66
crack	42000	163000	38000	153000;66-67
crack	38000	153000	40000	152000;67-68
crack	40000	152000	43000	150000;68-69
crack	43000	150000	38000	144000;69-70
crack	38000	144000	32000	141000;70-71
crack	32000	141000	23000	130000;71-72
crack	23000	130000	16000	127000;72-73
crack	16000	127000	14000	123000;73-74
crack	14000	123000	11000	119000;74-75
crack	11000	119000	6000	114000;75-76
crack	6000	114000	2000	111000;76-77
crack	2000	111000	0	107000;77-78
crack	38000	144000	36000	141000;70-79
crack	36000	141000	35000	135000;79-80
crack	35000	135000	37000	134500;80-81
crack	37000	134500	39000	131000;81-82
crack	39000	131000	35000	123000;82-83
crack	35000	123000	31000	120000;83-84
crack	31000	120000	25000	118000;84-85
crack	25000	118000	23000	114000;85-86
crack	23000	114000	16000	109000;86-87
crack	16000	109000	6000	105000;87-88
crack	6000	105000	3000	107000;88-89
crack	3000	107000	0	107000;89-78
crack	43000	150000	43000	147000;69-90
crack	43000	147000	43000	141000;90-91
crack	43000	141000	44000	138000;91-92
crack	44000	138000	50000	133000;92-93
crack	50000	133000	53000	129000;93-94
crack	53000	129000	57000	124000;94-95
crack	43000	147000	44000	142000;90-96
crack	44000	142000	53000	131000;96-97
crack	53000	131000	57000	124000;97-95
crack	57000	124000	55000	120000;95-98
crack	55000	120000	55000	112000;98-99
crack	55000	112000	52000	89000;99-100
crack	52000	89000	45000	84000;100-101
crack	45000	84000	44000	81000;101-102
crack	44000	81000	43000	75000;102-103
crack	43000	75000	39000	66000;103-104
crack	39000	66000	39000	60000;104-105
crack	39000	60000	38000	58000;105-106
crack	38000	58000	38000	54000;106-107

crack	38000	54000	38000	48000;107-108
crack	38000	48000	38000	46000;108-191
crack	52000	89000	46000	62000;100-109
crack	46000	62000	43000	56000;109-110
crack	43000	56000	47000	59000;110-111
crack	47000	59000	48000	58000;111-112
crack	48000	58000	47000	53000;112-113
crack	47000	53000	48000	50000;113-114
crack	48000	50000	47000	38000;114-118
crack	47000	38000	48000	36000;118-119
crack	48000	36000	47000	31000;119-120
crack	43000	56000	42000	54000;110-115
crack	42000	54000	45000	43000;115-116
crack	45000	43000	45000	36000;116-117
crack	45000	36000	47000	31000;117-120
crack	48000	50000	49000	47000;114-121
crack	49000	47000	51000	47000;121-122
crack	51000	47000	53000	54000;122-123
crack	53000	54000	54000	57000;123-124
crack	54000	57000	57000	55000;124-125
crack	57000	55000	57500	54000;125-126
crack	57500	54000	59000	48000;126-127
crack	59000	48000	59000	41000;127-128
crack	59000	41000	58000	35000;128-129
crack	58000	35000	55000	31000;129-130
crack	55000	31000	54000	27000;130-131
crack	54000	27000	51000	24000;131-132
crack	51000	24000	48000	14000;132-133
crack	49000	47000	50000	42000;121-134
crack	50000	42000	49000	40000;134-135;gr11 bound centr:53000,55000,45000,47000
crack	49000	40000	51000	38000;135-136;gr11 bound
crack	51000	38000	55000	38000;136-137;gr11 bound
crack	55000	38000	58000	46000;137-138;gr11 bound
crack	58000	46000	58000	48000;138-139;gr11 bound
crack	58000	48000	57000	48500;139-140;gr11 bound
crack	57000	48500	57500	49000;140-141;gr11 bound
crack	57500	49000	57000	53000;141-142;gr11 bound
crack	57000	53000	56000	54000;142-143;gr11 bound
crack	56000	54000	54000	54000;143-144;gr11 bound
crack	54000	54000	54000	51000;144-145;gr11 bound
crack	54000	51000	53000	50000;145-146;gr11 bound
crack	53000	50000	51000	43000;146-147;gr11 bound
crack	51000	43000	50000	42000;147-134;gr11 bound
crack	56000	54000	57000	54000;143-126
crack	47000	31000	45000	18000;120-148
crack	45000	18000	43000	14000;148-149
crack	43000	14000	43000	7000;149-150
crack	43000	7000	43500	4500;150-151
crack	43500	4500	43500	0;151-152
crack	48000	14000	47000	14500;133-153
crack	47000	14500	45000	9000;153-154
crack	45000	9000	45000	0;154-155
crack	48000	14000	49000	13000;133-160
crack	49000	13000	50000	15000;160-161
crack	49000	13000	51000	11000;160-159
crack	51000	11000	47000	7000;159-158
crack	47000	7000	46500	5000;158-157
crack	46500	5000	46000	0;157-156
crack	50000	15000	53000	18000;161-162
crack	53000	18000	53000	13000;162-163
crack	53000	13000	55000	10000;163-164
crack	55000	10000	56000	4000;164-165
crack	56000	4000	56000	0;165-166
crack	56000	4000	60000	14000;165-167
crack	60000	14000	62000	17000;167-168
crack	62000	17000	69000	23000;168-169
crack	69000	23000	67000	19000;169-170
crack	67000	19000	63000	14000;170-171
crack	63000	14000	61000	11000;171-172
crack	61000	11000	59000	6000;172-173
crack	59000	6000	59000	0;173-174
crack	71500	0	72000	4000;175-176
crack	72000	4000	78000	12000;176-177
crack	78000	12000	79000	15000;177-178
crack	79000	15000	84000	21000;178-179

crack	84000	21000	86000	21000;179-180
crack	86000	21000	84000	18000;180-181
crack	84000	18000	79000	11000;181-182
crack	79000	11000	77000	6000;182-183
crack	77000	6000	76000	0;183-184
crack	38000	48000	40000	45000;108-185
crack	40000	45000	41000	39000;185-186
crack	41000	39000	42000	30500;186-187
crack	42000	30500	40000	31000;187-188
crack	40000	31000	39500	34000;188-189
crack	39500	34000	38000	42000;189-190
crack	38000	42000	38000	46000;190-191
crack	38000	46000	36000	54000;191-192
crack	36000	54000	35500	55500;192-193
crack	35500	55500	36000	59000;193-194
crack	36000	59000	34000	56000;194-195
crack	34000	56000	34000	53000;195-196
crack	34000	53000	34000	52000;196-197
crack	34000	52000	34000	50000;197-198
crack	34000	50000	35000	48000;198-199
crack	35000	48000	36000	36000;199-200
crack	36000	36000	37500	34000;200-201
crack	36000	36000	39500	34000;200-201
crack	37500	34000	37000	33000;201-202
crack	37000	33000	34000	36000;202-203
crack	34000	36000	34000	41000;203-204
crack	34000	41000	32000	44000;204-205
crack	32000	44000	32000	46000;205-206
crack	32000	46000	31000	49000;206-207
crack	31000	49000	31000	54000;207-208
crack	31000	54000	31000	55000;208-209
crack	31000	55000	34000	53000;209-196
crack	31000	54000	34000	52000;208-197
crack	40000	31000	39000	31000;188-210
crack	39000	31000	36000	31000;210-211
crack	37000	33000	36000	31000;202-211
crack	36000	31000	32000	35000;211-212
crack	32000	35000	32000	33000;212-213
crack	32000	33000	35000	31000;213-214
crack	35000	31000	38000	30000;214-219
crack	39000	31000	38000	30000;210-219
crack	35000	31000	35000	28000;214-215
crack	38000	30000	37000	26000;219-218
crack	37000	26000	39000	23000;218-217
crack	39000	23000	36500	24000;217-216
crack	36500	24000	35000	28000;216-215
crack	36500	24000	36500	18000;216-220
crack	36500	18000	39000	14000;220-221
crack	39000	14000	40000	9000;221-222
crack	40000	9000	40000	0;222-223
crack	63000	177000	65000	170000;52-224
crack	65000	170000	72000	175000;224-225
crack	72000	175000	74000	175000;225-226
crack	74000	175000	76000	172000;226-227
crack	76000	172000	79000	165000;227-228
crack	76000	172000	78000	173000;227-235
crack	79000	165000	83000	164000;228-229
crack	83000	164000	84000	166000;229-230
crack	84000	166000	82000	170000;230-231
crack	82000	170000	85000	170000;231-232
crack	85000	170000	83000	172000;232-233
crack	83000	172000	80000	171000;233-234
crack	80000	171000	78000	173000;234-235
crack	78000	173000	80000	174000;235-236
crack	80000	174000	78000	176000;236-237
crack	78000	176000	80000	179000;237-238
crack	80000	179000	85000	185000;238-239
crack	85000	185000	90000	188000;239-240
crack	90000	188000	99000	190000;240-241
crack	99000	190000	96000	190000;241-242
crack	96000	190000	86000	194000;242-243
crack	86000	194000	85500	197000;243-244
crack	85500	197000	84000	200000;244-245
crack	86000	194000	75000	196000;243-246
crack	75000	196000	71000	200000;246-247

crack	99000	190000	102000	194000;241-248
crack	102000	194000	104000	195000;248-249
crack	104000	195000	105000	196000;249-250
crack	105000	196000	105000	198000;250-251
crack	105000	198000	106000	200000;251-252
crack	104000	195000	99000	182000;249-253
crack	99000	182000	97000	180000;253-254
crack	97000	180000	91000	179000;254-255
crack	91000	179000	87000	175000;255-256
crack	87000	175000	84000	174000;256-257
crack	84000	174000	82000	174000;257-258
crack	82000	174000	80000	176000;258-259
crack	80000	176000	80000	179000;259-238
crack	82000	174000	80000	174000;258-236
crack	65000	170000	68000	158000;224-260
crack	68000	158000	82000	133000;260-261
crack	82000	133000	82000	131000;261-262 gr2 bound centr: 83000,85000,126000,129000
crack	82000	131000	83000	130000;262-263 gr2 bound
crack	83000	130000	81000	130000;263-264 gr2 bound
crack	81000	130000	79000	129000;264-265 gr2 bound
crack	79000	129000	78000	127500;265-266 gr2 bound
crack	78000	127500	79000	126000;266-267 gr2 bound
crack	79000	126000	80000	125000;267-268 gr2 bound
crack	80000	125000	82000	123000;268-269 gr2 bound
crack	82000	123000	83000	122500;269-270 gr2 bound
crack	83000	122500	84000	123000;270-271 gr2 bound
crack	84000	123000	83000	124000;271-272 gr2 bound
crack	83000	124000	83000	125000;272-273 gr2 bound
crack	83000	125000	84000	125000;273-274 gr2 bound
crack	84000	125000	84000	127000;274-275 gr2 bound
crack	84000	127000	85000	127000;275-276 gr2 bound
crack	85000	127000	87500	126500;276-277 gr2 bound
crack	87500	126500	88000	129000;277-278 gr2 bound
crack	88000	129000	89000	129500;278-279 gr2 bound
crack	89000	129500	89500	131000;279-280 gr2 bound
crack	89500	131000	89000	132000;280-281 gr2 bound
crack	89000	132000	88000	132500;281-282 gr2 bound
crack	88000	132500	85000	132500;282-283 gr2 bound
crack	85000	132500	84000	133000;283-284 gr2 bound
crack	84000	133000	82000	133000;284-261 gr2 bound
crack	84000	125000	86500	115000;274-285
crack	86500	115000	85000	118000;285-286 gr7 bound centr: 85500,87500,100500,102500
crack	85000	118000	84000	119000;286-287 gr7 bound
crack	84000	119000	82500	119000;287-288 gr7 bound
crack	82500	119000	81000	118500;288-289 gr7 bound
crack	81000	118500	80000	118500;289-290 gr7 bound
crack	80000	118500	79000	116000;290-291 gr7 bound
crack	79000	116000	81000	116000;291-292 gr7 bound
crack	81000	116000	79000	114000;292-293 gr7 bound
crack	79000	114000	79500	113000;293-294 gr7 bound
crack	79500	113000	81000	113500;294-295 gr7 bound
crack	81000	113500	81000	113000;295-296 gr7 bound
crack	81000	113000	78000	110000;296-297 gr7 bound
crack	78000	110000	77500	108000;297-298 gr7 bound
crack	77500	108000	77500	107000;298-299 gr7 bound
crack	77500	107000	81500	100000;299-300 gr7 bound
crack	81500	100000	84000	100000;300-301 gr7 bound
crack	84000	100000	86000	99000;301-302 gr7 bound
crack	86000	99000	87000	96500;302-303 gr7 bound
crack	87000	96500	86000	96000;303-304 gr7 bound
crack	86000	96000	85000	94000;304-305 gr7 bound
crack	85000	94000	85000	92000;305-306 gr7 bound
crack	85000	92000	85500	91000;306-307 gr7 bound
crack	85500	91000	85000	89000;307-308 gr7 bound
crack	85000	89000	88000	86000;308-309 gr7 bound
crack	88000	86000	90000	85000;309-310 gr7 bound
crack	90000	85000	92000	85500;310-311 gr7 bound
crack	92000	85500	93000	87000;311-312 gr7 bound
crack	93000	87000	94000	87000;312-313 gr7 bound
crack	94000	87000	95500	86500;313-314 gr7 bound
crack	95500	86500	97000	87000;314-315 gr7 bound
crack	97000	87000	96000	89500;315-316 gr7 bound
crack	96000	89500	93000	91000;316-317 gr7 bound
crack	93000	91000	93000	93000;317-318 gr7 bound
crack	93000	93000	92500	93000;318-319 gr7 bound

crack	92500	93000	91500	97000;319-320	gr7 bound
crack	91500	97000	89000	97000;320-321	gr7 bound
crack	89000	97000	89000	98000;321-322	gr7 bound
crack	89000	98000	88000	102000;322-323	gr7 bound
crack	88000	102000	86000	104000;323-324	gr7 bound
crack	86000	104000	87000	104000;324-325	gr7 bound
crack	87000	104000	87000	105000;325-326	gr7 bound
crack	87000	105000	86000	106000;326-327	gr7 bound
crack	86000	106000	85000	106000;327-328	gr7 bound
crack	85000	106000	87000	108000;328-329	gr7 bound
crack	87000	108000	87000	109500;329-330	gr7 bound
crack	87000	109500	86000	110000;330-331	gr7 bound
crack	86000	110000	86500	115000;331-285	gr7 bound
crack	87500	126500	86000	125000;277-341	
crack	86000	125000	86000	123000;341-342	gr3 bound centr: 89000,91000,117000,119000
crack	86000	123000	87000	121000;342-343	gr3 bound
crack	87000	121000	87500	122000;343-344	gr3 bound
crack	87500	122000	87000	122000;344-345	gr3 bound
crack	87000	122000	87000	125000;345-346	gr3 bound
crack	87000	125000	88000	125000;346-347	gr3 bound
crack	88000	125000	88000	123000;347-348	gr3 bound
crack	88000	123000	89000	121500;348-349	gr3 bound
crack	89000	121500	89000	115000;349-350	gr3 bound
crack	89000	115000	90000	112000;350-351	gr3 bound
crack	90000	112000	89000	109000;351-352	gr3 bound
crack	89000	109000	90000	108000;352-353	gr3 bound
crack	90000	108000	91000	109000;353-354	gr3 bound
crack	91000	109000	91500	109000;354-355	gr3 bound
crack	91500	109000	92000	108000;355-356	gr3 bound
crack	92000	108000	92500	107500;356-357	gr3 bound
crack	92500	107500	94000	108000;357-358	gr3 bound
crack	94000	108000	92000	109000;358-359	gr3 bound
crack	92000	109000	92000	110000;359-360	gr3 bound
crack	92000	110000	92000	110500;360-361	gr3 bound
crack	92000	110500	94000	110500;361-362	gr3 bound
crack	94000	110500	94500	111000;362-363	gr3 bound
crack	94500	111000	94000	114000;363-364	gr3 bound
crack	94000	114000	93000	116000;364-365	gr3 bound
crack	93000	116000	92000	116500;365-366	gr3 bound
crack	92000	116500	92000	118000;366-367	gr3 bound
crack	92000	118000	93000	118500;367-368	gr3 bound
crack	93000	118500	93000	120000;368-369	gr3 bound
crack	93000	120000	92000	124000;369-370	gr3 bound
crack	92000	124000	93000	124000;370-371	gr3 bound
crack	93000	124000	93500	125000;371-372	gr3 bound
crack	93500	125000	90500	128500;372-373	gr3 bound
crack	90500	128500	88000	126000;373-374	gr3 bound
crack	88000	126000	86000	125000;374-341	gr3 bound
crack	93500	125000	94000	124500;372-375	
crack	94000	124500	94000	129000;375-376	gr4 bound centr: 97000,99000,124000,126000
crack	94000	129000	96000	130000;376-377	gr4 bound
crack	96000	130000	97000	130000;377-378	gr4 bound
crack	97000	130000	97000	131000;378-379	gr4 bound
crack	97000	131000	98000	131500;379-380	gr4 bound
crack	98000	131500	101500	131500;380-381	gr4 bound
crack	101500	131500	103000	129000;381-382	gr4 bound
crack	103000	129000	103000	127000;382-383	gr4 bound
crack	103000	127000	102000	126000;383-384	gr4 bound
crack	102000	126000	102000	124500;384-385	gr4 bound
crack	102000	124500	101000	124000;385-386	gr4 bound
crack	101000	124000	101000	123000;386-387	gr4 bound
crack	101000	123000	102000	123000;387-388	gr4 bound
crack	102000	123000	102000	121500;388-389	gr4 bound
crack	102000	121500	101000	120000;389-390	gr4 bound
crack	101000	120000	98000	119000;390-391	gr4 bound
crack	98000	119000	94000	121000;391-392	gr4 bound
crack	94000	121000	94000	124500;392-375	gr4 bound
crack	94000	121000	94000	120000;392-393	
crack	94000	120000	93500	118000;393-394	gr5 bound centr:94000,96000,117000,119000
crack	93500	118000	94000	116500;394-395	gr5 bound
crack	94000	116500	95000	115000;395-396	gr5 bound
crack	95000	115000	96500	116500;396-397	gr5 bound
crack	96500	116500	97000	116500;397-398	gr5 bound
crack	97000	116500	97000	118000;398-399	gr5 bound
crack	97000	118000	94000	120000;399-393	gr5 bound

crack	94500	111000	95500	111000;363-400
crack	95500	111000	96000	112500;400-401 gr6 bound centr:96000,98000,108000,110000
crack	96000	112500	97000	113000;401-402 gr6 bound
crack	97000	113000	98500	112000;402-403 gr6 bound
crack	98500	112000	99500	110000;403-404 gr6 bound
crack	99500	110000	99500	107500;404-405 gr6 bound
crack	99500	107500	99000	106000;405-406 gr6 bound
crack	99000	106000	98000	106000;406-407 gr6 bound
crack	98000	106000	97000	105500;407-408 gr6 bound
crack	97000	105500	95000	108000;408-409 gr6 bound
crack	95000	108000	95000	110000;409-410 gr6 bound
crack	95000	110000	95500	111000;410-400 gr6 bound
crack	86500	115000	91000	101000;285-332
crack	91000	101000	90500	99000;332-333
crack	90500	99000	91500	97000;333-320
crack	91000	101000	92500	98000;332-334
crack	92500	98000	97000	98000;334-335
crack	97000	98000	97000	97000;335-336 gr8 bound centr:98000,100000,97000,99000
crack	97000	97000	98000	96000;336-337 gr8 bound
crack	98000	96000	99500	96000;337-338 gr8 bound
crack	99500	96000	101000	98000;338-339 gr8 bound
crack	101000	98000	99500	99500;339-340 gr8 bound
crack	99500	99500	97000	98000;340-335 gr8 bound
crack	92500	98000	96000	91500;334-411
crack	96000	91500	98500	86000;411-412
crack	98500	86000	100000	76000;412-415
crack	88000	86000	92000	82500;309-413
crack	92000	85500	92000	82500;311-413
crack	92000	82500	98000	76500;413-414
crack	98000	76500	100000	76000;414-415
crack	92000	82500	94500	76000;413-427
crack	94500	76000	95500	64000;427-428
crack	95500	64000	96000	57000;428-429
crack	96000	57000	97000	48000;429-430
crack	97000	48000	98000	41000;430-431
crack	98000	41000	100500	33000;431-432
crack	100500	33000	103000	29500;432-433
crack	103000	29500	109500	22000;433-422
crack	100000	76000	101500	73000;415-416
crack	101500	73000	103000	69500;416-417
crack	103000	69500	107000	52000;417-418
crack	107000	52000	108500	46000;418-419
crack	108500	46000	110000	35000;419-420
crack	110000	35000	109500	29000;420-421
crack	109500	29000	109500	22000;421-422
crack	109500	22000	109000	21000;422-423
crack	109000	21000	108500	15000;423-424
crack	108500	15000	110500	8500;424-425
crack	110500	8500	112500	0;425-426
crack	109500	22000	114000	17000;422-445
crack	114000	17000	117000	14500;445-446
crack	117000	14500	122500	6000;446-447
crack	122500	6000	122500	4500;447-448
crack	122500	4500	124000	3000;448-449
crack	101500	73000	107000	68000;416-434
crack	107000	68000	111500	59000;434-435
crack	111500	59000	112000	49000;435-436
crack	112000	49000	113000	41000;436-437
crack	113000	41000	117000	29000;437-438
crack	117000	29000	115000	28500;438-439
crack	115000	28500	115000	27000;439-440
crack	115000	27000	114000	26000;440-441
crack	109500	29000	114000	26000;421-441
crack	114000	26000	118500	23000;441-442
crack	118500	23000	120000	21000;442-443
crack	120000	21000	124000	19000;443-444
crack	117000	29000	123000	32000;438-450
crack	123000	32000	124000	31000;450-451
crack	124000	165000	123000	163000;452-453
crack	123000	163000	117000	160000;453-454
crack	117000	160000	117000	153000;454-455
crack	117000	153000	117500	145000;455-456
crack	117500	145000	115500	138000;456-457
crack	115500	138000	113000	135000;457-458
crack	113000	135000	113500	130000;458-459

crack	113500	130000	112500	125000;459-460
crack	112500	125000	112000	120000;460-461
crack	112000	120000	110000	114500;461-462
crack	110000	114500	106500	110000;462-463
crack	106500	110000	104000	105000;463-464
crack	104000	105000	104500	102000;464-465
crack	104500	102000	105500	100000;465-466
crack	105500	100000	106000	95000;466-467
crack	106000	95000	109500	84000;467-468
crack	109500	84000	111500	82000;468-469
crack	111500	82000	112000	80000;469-470 gr9 bound centr:112000,114000,80000,82000
crack	112000	80000	113000	78000;470-471 gr9 bound
crack	113000	78000	114500	76500;471-472 gr9 bound
crack	114500	76500	115000	77000;472-473 gr9 bound
crack	115000	77000	115000	82000;473-474 gr9 bound
crack	115000	82000	114000	84000;474-475 gr9 bound
crack	114000	84000	113000	85000;475-476 gr9 bound
crack	113000	85000	112000	85000;476-477 gr9 bound
crack	112000	85000	111000	84000;477-478 gr9 bound
crack	111000	84000	111500	82000;478-469 gr9 bound
crack	114500	76500	115500	75000;472-479
crack	115500	75000	117000	70000;479-480
crack	117000	70000	120500	61000;480-481
crack	120500	61000	121000	59000;481-482
crack	121000	59000	120000	54500;482-483
crack	120000	54500	123000	45000;483-484
crack	123000	45000	122500	41000;484-485
crack	122500	41000	124000	39000;485-486
crack	123000	163000	122000	159000;453-487
crack	122000	159000	120000	147000;487-488
crack	120000	147000	119500	142000;488-489
crack	119500	142000	121000	137000;489-490
crack	121000	137000	121500	129000;490-491
crack	121500	129000	122000	122000;491-492
crack	122000	122000	121000	117000;492-493
crack	121000	117000	119500	115000;493-494
crack	119500	115000	115000	107000;494-495
crack	115000	107000	118500	105500;495-496
crack	118500	105500	117000	104000;496-497
crack	117000	104000	115000	100500;497-498
crack	115000	100500	115000	96000;498-499
crack	115000	96000	116000	92500;499-500
crack	116000	92500	119000	89000;500-501
crack	119000	89000	121500	87500;501-515
crack	118500	105500	117000	102000;496-509
crack	117000	102000	117000	99000;509-510
crack	117000	99000	119000	94500;510-511
crack	119000	94500	121500	94500;511-512
crack	121500	94500	123000	92500;512-513
crack	123000	92500	122000	91000;513-514
crack	122000	91000	121500	87500;514-515
crack	121500	87500	121000	84500;515-516
crack	118500	105500	119500	104000;496-502
crack	119500	104000	119500	101000;502-503
crack	119500	101000	122000	98000;503-504
crack	122000	98000	124000	98000;504-505
crack	119500	101000	120000	97500;503-506
crack	120000	97500	123000	94500;506-507
crack	123000	94500	124000	94500;507-508
crack	113500	130000	114000	125000;459-520
crack	114000	125000	113000	114000;520-521
crack	113000	114000	112500	111000;521-522
crack	112500	111000	113500	108000;522-523
crack	113500	108000	113000	89500;523-524
crack	105500	100000	113000	89500;466-524
crack	113000	89500	120500	80000;524-525
crack	120500	80000	120500	77000;525-526
crack	120500	77000	118500	74000;526-527
crack	118500	74000	118000	71000;527-528
crack	118000	71000	120500	65000;528-532
crack	120500	65000	120500	61000;532-481
crack	121000	84500	120500	80000;516-525
crack	121000	84500	123000	82000;516-517
crack	123000	82000	124000	81000;517-518
crack	123000	82000	124000	86500;517-519


```

crack 124000 86500 122500 80000;517-529
crack 122500 80000 122500 76000;529-530
crack 122500 76000 120000 72000;530-531
crack 120000 72000 120500 65000;531-532
crack 124000 70000 123500 68500;533-534 gr10 bound centr: 122000,124000,66000,67000
crack 123500 68500 122500 67500;534-535 gr10 bound
crack 122500 67500 122500 65500;535-536 gr10 bound
crack 122500 65500 123000 64000;536-537 gr10 bound
crack 123000 64000 124000 63000;537-538 gr10 bound
crack 52000 176000 57000 169500;53-539
crack 57000 169500 56000 168000;539-540
crack 56000 168000 53000 168500;540-541
crack 53000 168500 49000 171000;541-542
crack 49000 171000 43500 171500;542-543
crack 43500 171500 44000 170000;543-544
crack 44000 170000 52000 168000;544-545
crack 52000 168000 49000 162000;545-546
crack 49000 162000 48000 161000;546-547
crack 48000 161000 47000 157000;547-548
crack 47000 157000 43000 150000;548-69
;*****(Geometry File End)*****

```

```

:Pseudo contacts to reduce block size and allow zoning
crack 0 66000 39000 66000;Pj1(left block)
crack 47000 71000 96000 71000;Pj2(mid block)
crack 80000 135000 114000 135000;Pj3(rmid block)
;crack 90000 102000 106000 102000;Pj4(rmid block)
crack 104000 70000 108000 70000;Pj5(rmid block)
;crack 90000 102000 106000 102000;Pj6(rmid block)
crack 88000 110000 90000 110000;Pj7(rmid block)
crack 103000 127000 113000 127000;Pj8(rmid block)
crack 99000 107000 106000 107000;Pj9(rmid block)
crack 101000 98000 106000 98000;Pj10(rmid block)
crack 55000 38000 59000 38000;Pj11(rmid block)
crack 93000 115000 95000 115000;Pj12(rmid block)

```

```

hist unbal : hist1
hist sxx 62000 100000;hist2 (red 2)
hist syy 62000 100000;hist3 (red 2)

hist sst 60000 41000;hist4 (yel 4)Shear Stress selwyn high strain zone
hist sst 43000 40000;hist5 (yel 5)Shear Stress left of gin ck gr
hist sst 61000 172000;hist7 (yel 6)Shear Stress cloncurry

```

```
sav m1a_block.sav
```

```
gen 0 124000 0 200000 auto 1000
```

```
insitu stress -210e6 0 -140e6 szz -175e6
bound stress -210e6 0 -140e6
```

```
damp auto
```

```
;changing whole model to mat=1 (schist)
change 0 200000 0 124000 mat=1 cons=3
```

```
;changing all joints to jmat=1
change 0 200000 0 124000 jmat=1 jcon=2
```

```
;changing granite blocks to mat=2 (granite) constit model 3
change 57000,60000,175000,180000 mat=2 con=3 change 83000,85000,126000,129000 mat=2 con=3 ;gr2
change 89000,91000,117000,119000 mat=2 con=3 ;gr3
change 97000,99000,124000,126000 mat=2 con=3 ;gr4
change 94000,96000,117000,119000 mat=2 con=3 ;gr5
change 96000,98000,108000,110000 mat=2 con=3 ;gr6
change 85500,87500,100500,102500 mat=2 con=3 ;gr7
change 98000,100000,97000,99000 mat=2 con=3 ;gr8
change 112000,114000,80000,82000 mat=2 con=3 ;gr9
change 122000,124000,66000,67000 mat=2 con=3 ;gr10
change 53000,55000,45000,47000 mat=2 con=3 ;gr11

```

```
change jmat=2 range minterface 1 2
```

```

:changing pseudo joint properties to jmat=5
change jmat=5 range xr 0,39000 yr 65900 66100 ang -5,5;Pj1 properties
:pl hold mat jo
change jmat=5 range xr 47000,96000 yr 70900 71100 ang -5,5;Pj2 properties
:pl hold mat jo
change jmat=5 range xr 80000,114000 yr 134900 135100 ang -5,5; Pj3 properties
:pl hold mat jo
:change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj4 properties
change jmat=5 range xr 104000,108000 yr 69900 70100 ang -5,5; Pj5 properties
:pl hold mat jo
:change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj6 properties
change jmat=5 range xr 88000,90000 yr 109900 110100 ang -5,5; Pj7 properties
:pl hold mat jo
change jmat=5 range xr 103000,113000 yr 126900 127100 ang -5,5; Pj8 properties
:pl hold mat jo
change jmat=5 range xr 99000,106000 yr 106900 107100 ang -5,5; Pj9 properties
:pl hold mat jo
change jmat=5 range xr 101000,106000 yr 97900 98100 ang -5,5; Pj10 properties
:pl hold mat jo
change jmat=5 range xr 55000,59000 yr 37900 38100 ang -5,5; Pj11 properties
change jmat=5 range xr 93000,95000 yr 114900 115100 ang -5,5; Pj12 properties

:Create Movie files every 100 steps
plot ccfail blo bla
movie on file m1a.dcx step 500

sav m1a_prop.sav
step 10
sav m1a_stress.sav

step 500
sav m1a_1.sav
step 500
sav m1a_2.sav
step 500
sav m1a_3.sav
step 500
sav m1a_4.sav

step 500
sav m1a_5.sav
step 500
sav m1a_6.sav
step 500
sav m1a_7.sav
step 500
sav m1a_8.sav

return

```

U.2 Model 1b – dry model $\sigma_1 = 112.5^\circ$

```

:>1530Ma (Map Interp)MODEL 1 Old Granites- DRY MODEL

prop mat=1 dens 2850 bulk 25e9 shear 25e9 cohesion 10e6 tens 5e6 fric 31 dil 4

prop mat=2 dens 2650 bulk 49e9 shear 27e9 cohesion 20e6 tens 10e6 fric 37 dil 5

:contact properties
prop jmat=1 jkn 5e6 jks 1e3 jcoh 4e2 jtens 2e6 jfri 30 jdil 5
:prop jmat=1 jper 300 azero 0.05 ares 0.03

prop jmat=2 jkn 5e9 jks 1e5 jcoh 10e2 jtens 3e6 jfri 35 jdil 5
:prop jmat=2 jper 238 azero 0.03 ares 0.01

:Pseudo joints
prop jmat=5 jkn 100e9 jks 40e9 jcoh 190e10 jtens 190e10 jdil 0
:prop jmat=5 jper 0 azero 0 ares 0

round 100

block 0,0 0,200000 124000,200000 124000,0

```

*****(Geometry files as per Model 1a)******

```

;Pseudo contacts to reduce block size and allow zoning
crack 0 66000 39000 66000;Pj1(left block)
crack 47000 71000 96000 71000;Pj2(mid block)
crack 80000 135000 114000 135000;Pj3(rmid block)
;crack 90000 102000 106000 102000;Pj4(rmid block)
crack 104000 70000 108000 70000;Pj5(rmid block)
;crack 90000 102000 106000 102000;Pj6(rmid block)
crack 88000 110000 90000 110000;Pj7(rmid block)
crack 103000 127000 113000 127000;Pj8(rmid block)
crack 99000 107000 106000 107000;Pj9(rmid block)
crack 101000 98000 106000 98000;Pj10(rmid block)
crack 55000 38000 59000 38000;Pj11(rmid block)
crack 93000 115000 95000 115000;Pj12(rmid block)

hist unbal ; hist1
hist sxx 62000 100000;hist2 (red 2)
hist syy 62000 100000;hist3 (red 2)

hist sst 60000 41000;hist4 (yel 4)selwyn high strain zone
hist sst 43000 40000;hist5 (yel 5)left of gin ck gr
hist sst 61000 172000;hist7 (yel 6)cloncurry

sav mlb_block.sav

gen 0 124000 0 200000 auto 1000

insitu stress -210e6 52.5e6 -140e6 szz -175e6
bound stress -210e6 52.5e6 -140e6

damp auto

;changing whole model to mat=1 (schist)
change 0 200000 0 124000 mat=1 cons=3

;changing all joints to jmat=1
change 0 200000 0 124000 jmat=1 jcon=2

;changing granite blocks to mat=2 (granite) constit model 3
change 57000,60000,175000,180000 mat=2 con=3 ;gr1
change 83000,85000,126000,129000 mat=2 con=3 ;gr2
change 89000,91000,117000,119000 mat=2 con=3 ;gr3
change 97000,99000,124000,126000 mat=2 con=3 ;gr4
change 94000,96000,117000,119000 mat=2 con=3 ;gr5
change 96000,98000,108000,110000 mat=2 con=3 ;gr6
change 85500,87500,100500,102500 mat=2 con=3 ;gr7
change 98000,100000,97000,99000 mat=2 con=3 ;gr8
change 112000,114000,80000,82000 mat=2 con=3 ;gr9
change 122000,124000,66000,67000 mat=2 con=3 ;gr10
change 53000,55000,45000,47000 mat=2 con=3 ;gr11

;changing granite edges to jmat=2
change jmat=2 range minterface 1 2

;changing pseudo joint properties to jmat=5
change jmat=5 range xr 0,39000 yr 65900 66100 ang -5,5;Pj1 properties
;pl hold mat jo
change jmat=5 range xr 47000,96000 yr 70900 71100 ang -5,5;Pj2 properties
;pl hold mat jo
change jmat=5 range xr 80000,114000 yr 134900 135100 ang -5,5; Pj3 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj4 properties
change jmat=5 range xr 104000,108000 yr 69900 70100 ang -5,5; Pj5 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj6 properties
change jmat=5 range xr 88000,90000 yr 109900 110100 ang -5,5; Pj7 properties
;pl hold mat jo
change jmat=5 range xr 103000,113000 yr 126900 127100 ang -5,5; Pj8 properties
;pl hold mat jo
change jmat=5 range xr 99000,106000 yr 106900 107100 ang -5,5; Pj9 properties
;pl hold mat jo
change jmat=5 range xr 101000,106000 yr 97900 98100 ang -5,5; Pj10 properties
;pl hold mat jo

```

```

change jmat=5 range xr 55000,59000 yr 37900 38100 ang -5,5; Pj11 properties
;pl hold mat jo
change jmat=5 range xr 93000,95000 yr 114900 115100 ang -5,5; Pj12 properties
;pl hold mat jo

;Create Movie files every 100 steps
plot ccfail blo bla
movie on file m1b.dcx step 500

sav m1b_prop.sav
step 10
sav m1b_stress.sav

step 500
sav m1b_1.sav
step 500
sav m1b_2.sav
step 500
sav m1b_3.sav
step 500
sav m1b_4.sav

step 500
sav m1b_5.sav
step 500
sav m1b_6.sav
step 500
sav m1b_7.sav
step 500
sav m1b_8.sav

return

```

U.3 Model 1c – wet model $\sigma_1 = 90^\circ$

```
>1530Ma (Map Interp)MODEL 1 Old Granites- DRY MODEL
```

```

prop mat=1 dens 2850 bulk 25e9 shear 25e9 cohesion 10e6 tens 5e6 fric 31 dil 4
prop mat=2 dens 2650 bulk 49e9 shear 27e9 cohesion 20e6 tens 10e6 fric 37 dil 5

;contact properties
prop jmat=1 jkn 5e6 jks 1e3 jcoh 4e2 jtens 2e6 jfri 30 jdil 5
;prop jmat=1 jper 300 azero 0.05 ares 0.03

prop jmat=2 jkn 5e9 jks 1e5 jcoh 10e2 jtens 3e6 jfri 35 jdil 5
;prop jmat=2 jper 238 azero 0.03 ares 0.01

;Pseudo joints
prop jmat=5 jkn 100e9 jks 40e9 jcoh 190e10 jtens 190e10 jdil 0
;prop jmat=5 jper 0 azero 0 ares 0

round 100

block 0,0,0,200000 124000,200000 124000,0

***(Geometry files as per Model 1a)***

;Pseudo contacts to reduce block size and allow zoning
crack 0 66000 39000 66000;Pj1(left block)
crack 47000 71000 96000 71000;Pj2(mid block)
crack 80000 135000 114000 135000;Pj3(rmid block)
;crack 90000 102000 106000 102000;Pj4(rmid block)
crack 104000 70000 108000 70000;Pj5(rmid block)
;crack 90000 102000 106000 102000;Pj6(rmid block)
crack 88000 110000 90000 110000;Pj7(rmid block)
crack 103000 127000 113000 127000;Pj8(rmid block)
crack 99000 107000 106000 107000;Pj9(rmid block)
crack 101000 98000 106000 98000;Pj10(rmid block)

```

```
crack 55000 38000 59000 38000;Pj11(rmid block)
crack 93000 115000 95000 115000;Pj12(rmid block)
```

```
hist unbal ; hist1
hist sxx 62000 100000;hist2 (red 2)
hist syy 62000 100000;hist3 (red 2)
```

```
hist sst 60000 41000;hist4 (yel 4)selwyn high strain zone
hist sst 43000 40000;hist5 (yel 5)left of gin ck gr
hist sst 61000 172000;hist7 (yel 6)cloncurry
```

```
sav m1c_block.sav
```

```
gen 0 124000 0 200000 auto 1000
```

```
insitu stress -210e6 0 -140e6 szz -175e6
bound stress -210e6 0 -140e6
damp auto
```

```
;changing whole model to mat=1 (schist)
change 0 200000 0 124000 mat=1 cons=3
```

```
;changing all joints to jmat=1
change 0 200000 0 124000 jmat=1 jcon=2
```

```
;changing granite blocks to mat=2 (granite) constit model 3
change 57000,60000,175000,180000 mat=2 con=3 ;gr1
change 83000,85000,126000,129000 mat=2 con=3 ;gr2
change 89000,91000,117000,119000 mat=2 con=3 ;gr3
change 97000,99000,124000,126000 mat=2 con=3 ;gr4
change 94000,96000,117000,119000 mat=2 con=3 ;gr5
change 96000,98000,108000,110000 mat=2 con=3 ;gr6
change 85500,87500,100500,102500 mat=2 con=3 ;gr7
change 98000,100000,97000,99000 mat=2 con=3 ;gr8
change 112000,114000,80000,82000 mat=2 con=3 ;gr9
change 122000,124000,66000,67000 mat=2 con=3 ;gr10
change 53000,55000,45000,47000 mat=2 con=3 ;gr11
```

```
;changing granite edges to jmat=2 - must follow commands setting jmat=2 blocks
change jmat=2 range minterface 1 2
```

```
;changing pseudo joint properties to jmat=5
change jmat=5 range xr 0,39000 yr 65900 66100 ang -5,5;Pj1 properties
;pl hold mat jo
change jmat=5 range xr 47000,96000 yr 70900 71100 ang -5,5;Pj2 properties
;pl hold mat jo
change jmat=5 range xr 80000,114000 yr 134900 135100 ang -5,5; Pj3 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj4 properties
change jmat=5 range xr 104000,108000 yr 69900 70100 ang -5,5; Pj5 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj6 properties
change jmat=5 range xr 88000,90000 yr 109900 110100 ang -5,5; Pj7 properties
;pl hold mat jo
change jmat=5 range xr 103000,113000 yr 126900 127100 ang -5,5; Pj8 properties
;pl hold mat jo
change jmat=5 range xr 99000,106000 yr 106900 107100 ang -5,5; Pj9 properties
;pl hold mat jo
change jmat=5 range xr 101000,106000 yr 97900 98100 ang -5,5; Pj10 properties
;pl hold mat jo
change jmat=5 range xr 55000,59000 yr 37900 38100 ang -5,5; Pj11 properties
;pl hold mat jo
change jmat=5 range xr 93000,95000 yr 114900 115100 ang -5,5; Pj12 properties
;pl hold mat jo
```

```
;Create Movie files every 100 steps
plot ccfail blo bla
movie on file m1c.dcx step 500
```

```
sav m1c_prop.sav
step 10
sav m1c_stress.sav
```

```
step 500
```

```

sav m1c_1.sav
step 500
sav m1c_2.sav
step 500
sav m1c_3.sav
step 500
sav m1c_4.sav

;Establishing fluid pressure
fluid dens=1000;fluid density of 1000kgm3
set flow steady;set steady state flow
bo pp=125e6;
pfx pressure=125e6

step 500
sav m1c_5.sav
step 500
sav m1c_6.sav
step 500
sav m1c_7.sav
step 500
sav m1c_8.sav

step 500
sav m1c_9.sav
step 500
sav m1c_10.sav
step 500
sav m1c_11.sav
step 500
sav m1c_12.sav

step 500
sav m1c_13.sav
step 500
sav m1c_14.sav

return

```

U.4 Model 1d – wet model $\sigma_1 = 112.5^\circ$

```
>1530Ma (Map Interp)MODEL 1 Old Granites- DRY MODEL
```

```
prop mat=1 dens 2850 bulk 25e9 shear 25e9 cohesion 10e6 tens 5e6 fric 31 dil 4
```

```
prop mat=2 dens 2650 bulk 49e9 shear 27e9 cohesion 20e6 tens 10e6 fric 37 dil 5
```

```
;contact properties
prop jmat=1 jkn 5e6 jks 1e3 jcoh 4e2 jtens 2e6 jfri 30 jdil 5
;prop jmat=1 jper 300 azero 0.05 ares 0.03
```

```
prop jmat=2 jkn 5e9 jks 1e5 jcoh 10e2 jtens 3e6 jfri 35 jdil 5
;prop jmat=2 jper 238 azero 0.03 ares 0.01
```

```
;Pseudo joints
prop jmat=5 jkn 100e9 jks 40e9 jcoh 190e10 jtens 190e10 jdil 0
;prop jmat=5 jper 0 azero 0 ares 0
```

```
round 100
```

```
block 0,0 0,200000 124000,200000 124000,0
```

```
***(Geometry files as per Model 1a)***
```

```
;Psuedo contacts to reduce block size and allow zoning
crack 0 66000 39000 66000;Pj1(left block)
crack 47000 71000 96000 71000;Pj2(mid block)
crack 80000 135000 114000 135000;Pj3(rmid block)
;crack 90000 102000 106000 102000;Pj4(rmid block)
crack 104000 70000 108000 70000;Pj5(rmid block)
;crack 90000 102000 106000 102000;Pj6(rmid block)
```

```

crack      88000   110000   90000   110000;Pj7(rmid block)
crack      103000  127000  113000  127000;Pj8(rmid block)
crack      99000   107000  106000  107000;Pj9(rmid block)
crack      101000  98000   106000  98000;Pj10(rmid block)
crack      55000   38000   59000   38000;Pj11(rmid block)
crack      93000   115000  95000   115000;Pj12(rmid block)

hist unbal ; hist1
hist sxx 62000 100000;hist2 (red 2)
hist syy 62000 100000;hist3 (red 2)

hist sst 60000 41000;hist4 (yel 4)selwyn high strain zone
hist sst 43000 40000;hist5 (yel 5)left of gin ck gr
hist sst 61000 172000;hist7 (yel 6)cloncurry

sav m1d_block.sav

gen 0 124000 0 200000 auto 1000

insitu stress -210e6 52.5e6 -140e6 szz -175e6
bound stress -210e6 0 -140e6
damp auto

;changing whole model to mat=1 (schist)
change 0 200000 0 124000 mat=1 cons=3

;changing all joints to jmat=1
change 0 200000 0 124000 jmat=1 jcon=2

;changing granite blocks to mat=2 (granite) constit model 3
change 57000,60000,175000,180000 mat=2 con=3 ;gr1
change 83000,85000,126000,129000 mat=2 con=3 ;gr2
change 89000,91000,117000,119000 mat=2 con=3 ;gr3
change 97000,99000,124000,126000 mat=2 con=3 ;gr4
change 94000,96000,117000,119000 mat=2 con=3 ;gr5
change 96000,98000,108000,110000 mat=2 con=3 ;gr6
change 85500,87500,100500,102500 mat=2 con=3 ;gr7
change 98000,100000,97000,99000 mat=2 con=3 ;gr8
change 112000,114000,80000,82000 mat=2 con=3 ;gr9
change 122000,124000,66000,67000 mat=2 con=3 ;gr10
change 53000,55000,45000,47000 mat=2 con=3 ;gr11

;changing granite edges to jmat=2 - must follow commands setting jmat=2 blocks
change jmat=2 range minterface 1 2

;changing pseudo joint properties to jmat=5
change jmat=5 range xr 0,39000 yr 65900 66100 ang -5,5;Pj1 properties
;pl hold mat jo
change jmat=5 range xr 47000,96000 yr 70900 71100 ang -5,5;Pj2 properties
;pl hold mat jo
change jmat=5 range xr 80000,114000 yr 134900 135100 ang -5,5;Pj3 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj4 properties
change jmat=5 range xr 104000,108000 yr 69900 70100 ang -5,5; Pj5 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj6 properties
change jmat=5 range xr 88000,90000 yr 109900 110100 ang -5,5; Pj7 properties
;pl hold mat jo
change jmat=5 range xr 103000,113000 yr 126900 127100 ang -5,5; Pj8 properties
;pl hold mat jo
change jmat=5 range xr 99000,106000 yr 106900 107100 ang -5,5; Pj9 properties
;pl hold mat jo
change jmat=5 range xr 101000,106000 yr 97900 98100 ang -5,5; Pj10 properties
;pl hold mat jo
change jmat=5 range xr 55000,59000 yr 37900 38100 ang -5,5; Pj11 properties
;pl hold mat jo
change jmat=5 range xr 93000,95000 yr 114900 115100 ang -5,5; Pj12 properties
;pl hold mat jo

;Create Movie files every 100 steps
plot ccfail blo bla
movie on file m1d.dcx step 500

sav m1d_prop.sav
step 10

```

```

sav m1d_stress.sav

step 500
sav m1d_1.sav
step 500
sav m1d_2.sav
step 500
sav m1d_3.sav
step 500
sav m1d_4.sav

;Establishing fluid pressure
fluid dens=1000;fluid density of 1000kgm'3
set flow steady;set steady state flow
bo pp=125e6;
pfix pressure=125e6

step 500
sav m1d_5.sav
step 500
sav m1d_6.sav
step 500
sav m1d_7.sav
step 500
sav m1d_8.sav

step 500
sav m1d_9.sav
step 500
sav m1d_10.sav
step 500
sav m1d_11.sav
step 500
sav m1d_12.sav

step 500
sav m1d_13.sav
step 500
sav m1d_14.sav

return

```

U.5 Model 2a – dry model $\sigma_1 = 90^\circ$

```

;>1490Ma (Map Interp)MODEL 2 Young Granites- DRY MODEL

;metasediment properties
prop mat=1 dens 2850 bulk 25e9 shear 25e9 cohesion 10e6 tens 5e6 fric 31 dil 4

;granite properties
prop mat=2 dens 2650 bulk 49e9 shear 27e9 cohesion 20e6 tens 10e6 fric 37 dil 5

;contact properties
prop jmat=1 jkn 5e6 jks 1e3 jcoh 4e2 jtens 2e6 jfri 30 jdil 5
;prop jmat=1 jper 300 azero 0.05 ares 0.03

prop jmat=2 jkn 5e9 jks 1e5 jcoh 10e2 jtens 3e6 jfri 35 jdil 5
;prop jmat=2 jper 238 azero 0.03 ares 0.01

;Pseudo joints
prop jmat=5 jkn 100e9 jks 40e9 jcoh 190e10 jtens 190e10 jdil 0
;prop jmat=5 jper 0 azero 0 ares 0

round 100

block 0,0,0,200000 124000,200000 124000,0

;***** (Geometry File Start) *****
crack 1000 200000 1500 192000;1-2
crack 1500 192000 1000 191000;2-3
crack 1000 191000 0 189000;3-4

```


crack	6500	200000	5500	199000;7-6	
crack	5500	199000	4000	198000;6-5	
crack	4000	198000	1500	192000;5-2	
crack	5500	199000	6000	193000;6-8	
crack	6000	193000	4000	186000;8-9	
crack	4000	186000	4000	180000;9-10	
crack	4000	180000	4500	176000;10-11	
crack	4500	176000	2000	171000;11-12	
crack	4000	198000	3500	188000;5-17	
crack	3500	188000	2500	184000;17-18	
crack	2500	184000	2500	175000;18-19	
crack	2500	175000	2000	171000;19-12	
crack	2000	171000	1500	170000;12-13	
crack	1500	170000	1500	160000;13-14	
crack	1500	160000	5000	155000;14-15	
crack	5000	155000	2000	150000;15-16	
crack	2000	150000	0	148000;16-20	
crack	21500	200000	21500	189000;21-22	
crack	21500	189000	20000	182000;22-23	
crack	27500	200000	23000	185000;25-26	
crack	23000	185000	20000	182000;26-23	
crack	20000	182000	19500	179000;23-24	
crack	19500	179000	13500	168000;24-27	
crack	13500	168000	10500	165000;27-28	
crack	10500	165000	9500	162000;28-29	
crack	9500	162000	5000	155000;29-15	
crack	9500	162000	10000	160000;29-30	
crack	10000	160000	6500	154000;30-31	
crack	6500	154000	4000	149000;31-32	
crack	4000	149000	0	147000;32-33	
crack	4000	149000	0	141000;32-34	
;crack	69000	200000	64000	181000;35-36	
crack	64000	181000	62000	181000;36-37	gr1 bound centr:57000,60000,175000,180000
crack	62000	181000	61000	180000;37-38	gr1 bound
crack	61000	180000	54500	180000;38-39	gr1 bound
crack	54500	180000	53000	179500;39-40	gr1 bound
crack	53000	179500	53000	176000;40-41	gr1 bound
crack	53000	176000	54000	175000;41-42	gr1 bound
crack	54000	175000	56000	173000;42-43	gr1 bound
crack	56000	173000	57000	171000;43-44	gr1 bound
crack	57000	171000	58000	172000;44-45	gr1 bound
crack	58000	172000	60000	172500;45-46	gr1 bound
crack	60000	172500	59500	173500;46-47	gr1 bound
crack	59500	173500	58000	173000;47-48	gr1 bound
crack	58000	173000	57000	173500;48-49	gr1 bound
crack	57000	173500	57500	175000;49-50	gr1 bound
crack	57500	175000	61000	175000;50-51	gr1 bound
crack	61000	175000	63000	177000;51-52	gr1 bound
;crack	63000	177000	64000	181000;52-36	gr1 bound
crack	54000	175000	52000	176000;42-53	
crack	52000	176000	47000	179000;53-54	
crack	47000	179000	45000	179000;54-55	
crack	45000	179000	41000	181000;55-56	
crack	41000	181000	38000	179000;56-57	
crack	38000	179000	38500	173000;57-58	
crack	38500	173000	37000	169000;58-59	
crack	37000	169000	25000	164000;59-60	
crack	25000	164000	21000	163000;60-61	
crack	21000	163000	11000	158000;61-62	
crack	11000	158000	8000	145000;62-63	
crack	8000	145000	0	130000;63-64	
crack	38500	173000	42000	170000;58-65	
crack	42000	170000	42000	163000;65-66	
crack	42000	163000	38000	153000;66-67	
crack	38000	153000	40000	152000;67-68	
crack	40000	152000	43000	150000;68-69	
crack	43000	150000	38000	144000;69-70	
crack	38000	144000	32000	141000;70-71	
crack	32000	141000	23000	130000;71-72	
crack	23000	130000	16000	127000;72-73	
crack	16000	127000	14000	123000;73-74	
crack	14000	123000	11000	119000;74-75	
crack	11000	119000	6000	114000;75-76	
crack	6000	114000	2000	111000;76-77	
crack	2000	111000	0	107000;77-78	

crack	38000	144000	36000	141000;70-79
crack	36000	141000	35000	135000;79-80
crack	35000	135000	37000	134500;80-81
crack	37000	134500	39000	131000;81-82
crack	39000	131000	35000	123000;82-83
crack	35000	123000	31000	120000;83-84
crack	31000	120000	25000	118000;84-85
crack	25000	118000	23000	114000;85-86
crack	23000	114000	16000	109000;86-87
crack	16000	109000	6000	105000;87-88
crack	6000	105000	3000	107000;88-89
crack	3000	107000	0	107000;89-78
crack	43000	150000	43000	147000;69-90
crack	43000	147000	43000	141000;90-91
crack	43000	141000	44000	138000;91-92
crack	44000	138000	50000	133000;92-93
crack	50000	133000	53000	129000;93-94
crack	53000	129000	57000	124000;94-95
crack	43000	147000	44000	142000;90-96
crack	44000	142000	53000	131000;96-97
crack	53000	131000	57000	124000;97-95
crack	57000	124000	55000	120000;95-98
crack	55000	120000	55000	112000;98-99
crack	55000	112000	52000	89000;99-100
crack	52000	89000	45000	84000;100-101
crack	45000	84000	44000	81000;101-102
crack	44000	81000	43000	75000;102-103
crack	43000	75000	39000	66000;103-104
crack	39000	66000	39000	60000;104-105
crack	39000	60000	38000	58000;105-106
crack	38000	58000	38000	54000;106-107
crack	38000	54000	38000	48000;107-108
crack	38000	48000	38000	46000;108-191
crack	52000	89000	46000	62000;100-109
crack	46000	62000	43000	56000;109-110
crack	43000	56000	47000	59000;110-111
crack	47000	59000	48000	58000;111-112
crack	48000	58000	47000	53000;112-113
crack	47000	53000	48000	50000;113-114
crack	48000	50000	47000	38000;114-118
crack	47000	38000	48000	36000;118-119
crack	48000	36000	47000	31000;119-120
crack	43000	56000	42000	54000;110-115
crack	42000	54000	45000	43000;115-116
crack	45000	43000	45000	36000;116-117
crack	45000	36000	47000	31000;117-120
crack	48000	50000	49000	47000;114-121
crack	49000	47000	51000	47000;121-122
crack	51000	47000	53000	54000;122-123
crack	53000	54000	54000	57000;123-124
crack	54000	57000	57000	55000;124-125
crack	57000	55000	57500	54000;125-126
crack	57500	54000	59000	48000;126-127
crack	59000	48000	59000	41000;127-128
crack	59000	41000	58000	35000;128-129
crack	58000	35000	55000	31000;129-130
crack	55000	31000	54000	27000;130-131
crack	54000	27000	51000	24000;131-132
crack	51000	24000	48000	14000;132-133
crack	49000	47000	50000	42000;121-134
crack	50000	42000	49000	40000;134-135;gr11 bound centr:53000,55000,45000,47000
crack	49000	40000	51000	38000;135-136;gr11 bound
crack	51000	38000	55000	38000;136-137;gr11 bound
crack	55000	38000	58000	46000;137-138;gr11 bound
crack	58000	46000	58000	48000;138-139;gr11 bound
crack	58000	48000	57000	48500;139-140;gr11 bound
crack	57000	48500	57500	49000;140-141;gr11 bound
crack	57500	49000	57000	53000;141-142;gr11 bound
crack	57000	53000	56000	54000;142-143;gr11 bound
crack	56000	54000	54000	54000;143-144;gr11 bound
crack	54000	54000	54000	51000;144-145;gr11 bound
crack	54000	51000	53000	50000;145-146;gr11 bound
crack	53000	50000	51000	43000;146-147;gr11 bound
crack	51000	43000	50000	42000;147-134;gr11 bound
crack	56000	54000	57500	54000;143-126

crack	47000	31000	45000	18000;120-148
crack	45000	18000	43000	14000;148-149
crack	43000	14000	43000	7000;149-150
crack	43000	7000	43500	4500;150-151
crack	43500	4500	43500	0;151-152
crack	48000	14000	47000	14500;133-153
crack	47000	14500	45000	9000;153-154
crack	45000	9000	45000	0;154-155
crack	48000	14000	49000	13000;133-160
crack	49000	13000	50000	15000;160-161
crack	49000	13000	51000	11000;160-159
crack	51000	11000	47000	7000;159-158
crack	47000	7000	46500	5000;158-157
crack	46500	5000	46000	0;157-156
crack	50000	15000	53000	18000;161-162
crack	53000	18000	53000	13000;162-163
crack	53000	13000	55000	10000;163-164
crack	55000	10000	56000	4000;164-165
crack	56000	4000	56000	0;165-166
crack	56000	4000	60000	14000;165-167
crack	60000	14000	62000	17000;167-168
crack	62000	17000	69000	23000;168-169
crack	69000	23000	67000	19000;169-170
crack	67000	19000	63000	14000;170-171
crack	63000	14000	61000	11000;171-172
crack	61000	11000	59000	6000;172-173
crack	59000	6000	59000	0;173-174
crack	71500	0	72000	4000;175-176
crack	72000	4000	78000	12000;176-177
crack	78000	12000	79000	15000;177-178
crack	79000	15000	83000	20000;178-179
crack	83000	20000	85000	20000;179-180
crack	86000	21000	84000	18000;180-181
crack	84000	18000	79000	11000;181-182
crack	79000	11000	77000	6000;182-183
crack	77000	6000	76000	0;183-184
crack	38000	48000	40000	45000;108-185
crack	40000	45000	41000	39000;185-186
crack	41000	39000	42000	30500;186-187
crack	42000	30500	40000	31000;187-188
crack	40000	31000	39500	34000;188-189
crack	39500	34000	38000	42000;189-190
crack	38000	42000	38000	46000;190-191
crack	38000	46000	36000	54000;191-192
crack	36000	54000	35500	55500;192-193
crack	35500	55500	36000	59000;193-194
crack	36000	59000	34000	56000;194-195
crack	34000	56000	34000	53000;195-196
crack	34000	53000	34000	52000;196-197
crack	34000	52000	34000	50000;197-198
crack	34000	50000	35000	48000;198-199
crack	35000	48000	36000	36000;199-200
crack	36000	36000	37500	34000;200-201
crack	36000	36000	39500	34000;200-201
crack	37500	34000	37000	33000;201-202
crack	37000	33000	34000	36000;202-203
crack	34000	36000	34000	41000;203-204
crack	34000	41000	32000	44000;204-205
crack	32000	44000	32000	46000;205-206
crack	32000	46000	31000	49000;206-207
crack	31000	49000	31000	54000;207-208
crack	31000	54000	31000	55000;208-209
crack	31000	55000	34000	53000;209-196
crack	31000	54000	34000	52000;208-197
crack	40000	31000	39000	31000;188-210
crack	39000	31000	36000	31000;210-211
crack	37000	33000	36000	31000;202-211
crack	36000	31000	32000	35000;211-212
crack	32000	35000	32000	33000;212-213
crack	32000	33000	35000	31000;213-214
crack	35000	31000	38000	30000;214-219
crack	39000	31000	38000	30000;210-219
crack	35000	31000	35000	28000;214-215
crack	38000	30000	37000	26000;219-218
crack	37000	26000	39000	23000;218-217

crack	39000	23000	36500	24000;217-216
crack	36500	24000	35000	28000;216-215
crack	36500	24000	36500	18000;216-220
crack	36500	18000	39000	14000;220-221
crack	39000	14000	40000	9000;221-222
crack	40000	9000	40000	0;222-223
crack	63000	177000	65000	170000;52-224
crack	65000	170000	72000	175000;224-225
crack	72000	175000	74000	175000;225-226
crack	74000	175000	76000	172000;226-227
crack	76000	172000	79000	165000;227-228
crack	76000	172000	78000	173000;227-235
crack	79000	165000	83000	164000;228-229
crack	83000	164000	84000	166000;229-230
crack	84000	166000	82000	170000;230-231
crack	82000	170000	85000	170000;231-232
crack	85000	170000	83000	172000;232-233
crack	83000	172000	80000	171000;233-234
crack	80000	171000	78000	173000;234-235
crack	78000	173000	80000	174000;235-236
crack	80000	174000	78000	176000;236-237
crack	78000	176000	80000	179000;237-238
crack	80000	179000	85000	185000;238-239
crack	85000	185000	90000	188000;239-240
crack	90000	188000	99000	190000;240-241
crack	99000	190000	96000	190000;241-242
crack	96000	190000	86000	194000;242-243
crack	86000	194000	85500	197000;243-244
crack	85500	197000	84000	200000;244-245
;crack	86000	194000	75000	196000;243-246
;crack	75000	196000	71000	200000;246-247
crack	99000	190000	102000	194000;241-248
crack	102000	194000	104000	195000;248-249
crack	104000	195000	105000	196000;249-250
crack	105000	196000	105000	198000;250-251
crack	105000	198000	106000	200000;251-252
crack	104000	195000	99000	182000;249-253
crack	99000	182000	97000	180000;253-254
crack	97000	180000	91000	179000;254-255
crack	91000	179000	87000	175000;255-256
crack	87000	175000	84000	174000;256-257
crack	84000	174000	82000	174000;257-258
crack	82000	174000	80000	176000;258-259
crack	80000	176000	80000	179000;259-238
crack	82000	174000	80000	174000;258-236
crack	65000	170000	68000	158000;224-260
;crack	68000	158000	82000	133000;260-261
crack	82000	133000	82000	131000;261-262 gr2 bound centr: 83000,85000,126000,129000
crack	82000	131000	83000	130000;262-263 gr2 bound
crack	83000	130000	81000	130000;263-264 gr2 bound
crack	81000	130000	79000	129000;264-265 gr2 bound
crack	79000	129000	78000	127500;265-266 gr2 bound
crack	78000	127500	79000	126000;266-267 gr2 bound
crack	79000	126000	80000	125000;267-268 gr2 bound
crack	80000	125000	82000	123000;268-269 gr2 bound
crack	82000	123000	83000	122500;269-270 gr2 bound
crack	83000	122500	84000	123000;270-271 gr2 bound
crack	84000	123000	83000	124000;271-272 gr2 bound
crack	83000	124000	83000	125000;272-273 gr2 bound
crack	83000	125000	84000	125000;273-274 gr2 bound
crack	84000	125000	84000	127000;274-275 gr2 bound
crack	84000	127000	85000	127000;275-276 gr2 bound
crack	85000	127000	87500	126500;276-277 gr2 bound
crack	87500	126500	88000	129000;277-278 gr2 bound
crack	88000	129000	89000	129500;278-279 gr2 bound
crack	89000	129500	89500	131000;279-280 gr2 bound
crack	89500	131000	89000	132000;280-281 gr2 bound
crack	89000	132000	88000	132500;281-282 gr2 bound
crack	88000	132500	85000	132500;282-283 gr2 bound
crack	85000	132500	84000	133000;283-284 gr2 bound
crack	84000	133000	82000	133000;284-261 gr2 bound
crack	84000	125000	86500	115000;274-285
crack	86500	115000	85000	118000;285-286 gr7 bound centr: 85500,87500,100500,102500
crack	85000	118000	84000	119000;286-287 gr7 bound
crack	84000	119000	82500	119000;287-288 gr7 bound

crack	82500	119000	81000	118500;288-289	gr7 bound
crack	81000	118500	80000	118500;289-290	gr7 bound
crack	80000	118500	79000	116000;290-291	gr7 bound
crack	79000	116000	81000	116000;291-292	gr7 bound
crack	81000	116000	79000	114000;292-293	gr7 bound
crack	79000	114000	79500	113000;293-294	gr7 bound
crack	79500	113000	81000	113500;294-295	gr7 bound
crack	81000	113500	81000	113000;295-296	gr7 bound
crack	81000	113000	78000	110000;296-297	gr7 bound
crack	78000	110000	77500	108000;297-298	gr7 bound
crack	77500	108000	77500	107000;298-299	gr7 bound
crack	77500	107000	81500	100000;299-300	gr7 bound
crack	81500	100000	84000	100000;300-301	gr7 bound
crack	84000	100000	86000	99000;301-302	gr7 bound
crack	86000	99000	87000	96500;302-303	gr7 bound
crack	87000	96500	86000	96000;303-304	gr7 bound
crack	86000	96000	85000	94000;304-305	gr7 bound
crack	85000	94000	85000	92000;305-306	gr7 bound
crack	85000	92000	85500	91000;306-307	gr7 bound
crack	85500	91000	85000	89000;307-308	gr7 bound
crack	85000	89000	88000	86000;308-309	gr7 bound
crack	88000	86000	90000	85000;309-310	gr7 bound
crack	90000	85000	92000	85500;310-311	gr7 bound
crack	92000	85500	93000	87000;311-312	gr7 bound
crack	93000	87000	94000	87000;312-313	gr7 bound
crack	94000	87000	95500	86500;313-314	gr7 bound
crack	95500	86500	97000	87000;314-315	gr7 bound
crack	97000	87000	96000	89500;315-316	gr7 bound
crack	96000	89500	93000	91000;316-317	gr7 bound
crack	93000	91000	93000	93000;317-318	gr7 bound
crack	93000	93000	92500	93000;318-319	gr7 bound
crack	92500	93000	91500	97000;319-320	gr7 bound
crack	91500	97000	89000	97000;320-321	gr7 bound
crack	89000	97000	89000	98000;321-322	gr7 bound
crack	89000	98000	88000	102000;322-323	gr7 bound
crack	88000	102000	86000	104000;323-324	gr7 bound
crack	86000	104000	87000	104000;324-325	gr7 bound
crack	87000	104000	87000	105000;325-326	gr7 bound
crack	87000	105000	86000	106000;326-327	gr7 bound
crack	86000	106000	85000	106000;327-328	gr7 bound
crack	85000	106000	87000	108000;328-329	gr7 bound
crack	87000	108000	87000	109500;329-330	gr7 bound
crack	87000	109500	86000	110000;330-331	gr7 bound
crack	86000	110000	86500	115000;331-285	gr7 bound
crack	87500	126500	86000	125000;277-341	
crack	86000	125000	86000	123000;341-342	gr3 bound centr: 89000,91000,117000,119000
crack	86000	123000	87000	121000;342-343	gr3 bound
crack	87000	121000	87500	122000;343-344	gr3 bound
crack	87500	122000	87000	122000;344-345	gr3 bound
crack	87000	122000	87000	125000;345-346	gr3 bound
crack	87000	125000	88000	125000;346-347	gr3 bound
crack	88000	125000	88000	123000;347-348	gr3 bound
crack	88000	123000	89000	121500;348-349	gr3 bound
crack	89000	121500	89000	115000;349-350	gr3 bound
crack	89000	115000	90000	112000;350-351	gr3 bound
crack	90000	112000	89000	109000;351-352	gr3 bound
crack	89000	109000	90000	108000;352-353	gr3 bound
crack	90000	108000	91000	109000;353-354	gr3 bound
crack	91000	109000	91500	109000;354-355	gr3 bound
crack	91500	109000	92000	108000;355-356	gr3 bound
crack	92000	108000	92500	107500;356-357	gr3 bound
crack	92500	107500	94000	108000;357-358	gr3 bound
crack	94000	108000	92000	109000;358-359	gr3 bound
crack	92000	109000	92000	110000;359-360	gr3 bound
crack	92000	110000	92000	110500;360-361	gr3 bound
crack	92000	110500	94000	110500;361-362	gr3 bound
crack	94000	110500	94500	111000;362-363	gr3 bound
crack	94500	111000	94000	114000;363-364	gr3 bound
crack	94000	114000	93000	116000;364-365	gr3 bound
crack	93000	116000	92000	116500;365-366	gr3 bound
crack	92000	116500	92000	118000;366-367	gr3 bound
crack	92000	118000	93000	118500;367-368	gr3 bound
crack	93000	118500	93000	120000;368-369	gr3 bound
crack	93000	120000	92000	124000;369-370	gr3 bound
crack	92000	124000	93000	124000;370-371	gr3 bound

crack	93000	124000	93500	125000;371-372	gr3 bound
crack	93500	125000	90500	128500;372-373	gr3 bound
crack	90500	128500	88000	126000;373-374	gr3 bound
crack	88000	126000	86000	125000;374-341	gr3 bound
crack	93500	125000	94000	124500;372-375	
crack	94000	124500	94000	129000;375-376	gr4 bound centr: 97000,99000,124000,126000
crack	94000	129000	96000	130000;376-377	gr4 bound
crack	96000	130000	97000	130000;377-378	gr4 bound
crack	97000	130000	97000	131000;378-379	gr4 bound
crack	97000	131000	98000	131500;379-380	gr4 bound
crack	98000	131500	101500	131500;380-381	gr4 bound
crack	101500	131500	103000	129000;381-382	gr4 bound
crack	103000	129000	103000	127000;382-383	gr4 bound
crack	103000	127000	102000	126000;383-384	gr4 bound
crack	102000	126000	102000	124500;384-385	gr4 bound
crack	102000	124500	101000	124000;385-386	gr4 bound
crack	101000	124000	101000	123000;386-387	gr4 bound
crack	101000	123000	102000	123000;387-388	gr4 bound
crack	102000	123000	102000	121500;388-389	gr4 bound
crack	102000	121500	101000	120000;389-390	gr4 bound
crack	101000	120000	98000	119000;390-391	gr4 bound
crack	98000	119000	94000	121000;391-392	gr4 bound
crack	94000	121000	94000	124500;392-375	gr4 bound
crack	94000	121000	94000	120000;392-393	
crack	94000	120000	93500	118000;393-394	gr5 bound centr:94000,96000,117000,119000
crack	93500	118000	94000	116500;394-395	gr5 bound
crack	94000	116500	95000	115000;395-396	gr5 bound
crack	95000	115000	96500	116500;396-397	gr5 bound
crack	96500	116500	97000	116500;397-398	gr5 bound
crack	97000	116500	97000	118000;398-399	gr5 bound
crack	97000	118000	94000	120000;399-393	gr5 bound
crack	94500	111000	95500	111000;363-400	
crack	95500	111000	96000	112500;400-401	gr6 bound centr:96000,98000,108000,110000
crack	96000	112500	97000	113000;401-402	gr6 bound
crack	97000	113000	98500	112000;402-403	gr6 bound
crack	98500	112000	99500	110000;403-404	gr6 bound
crack	99500	110000	99500	107500;404-405	gr6 bound
crack	99500	107500	99000	106000;405-406	gr6 bound
crack	99000	106000	98000	106000;406-407	gr6 bound
crack	98000	106000	97000	105500;407-408	gr6 bound
crack	97000	105500	95000	108000;408-409	gr6 bound
crack	95000	108000	95000	110000;409-410	gr6 bound
crack	95000	110000	95500	111000;410-400	gr6 bound
crack	86500	115000	91000	101000;285-332	
crack	91000	101000	90500	99000;332-333	
crack	90500	99000	91500	97000;333-320	
crack	91000	101000	92500	98000;332-334	
crack	92500	98000	97000	98000;334-335	
crack	97000	98000	97000	97000;335-336	gr8 bound centr:98000,100000,97000,99000
crack	97000	97000	98000	96000;336-337	gr8 bound
crack	98000	96000	99500	96000;337-338	gr8 bound
crack	99500	96000	101000	98000;338-339	gr8 bound
crack	101000	98000	99500	99500;339-340	gr8 bound
crack	99500	99500	97000	98000;340-335	gr8 bound
crack	92500	98000	96000	91500;334-411	
crack	96000	91500	98500	86000;411-412	
crack	98500	86000	100000	76000;412-415	
crack	88000	86000	92000	82500;309-413	
crack	92000	85500	92000	82500;311-413	
crack	92000	82500	92000	82500;413-b393	
crack	98000	76500	100000	76000;414-415	
;crack	92000	82500	94500	76000;413-427	
;crack	94500	76000	95500	64000;427-428	
;crack	95500	64000	96000	57000;428-429	
;crack	96000	57000	97000	48000;429-430	
;crack	97000	48000	98000	41000;430-431	
;crack	98000	41000	100500	33000;431-432	
;crack	100500	33000	103000	29500;432-433	
crack	103000	29500	109500	22000;433-422	
crack	100000	76000	101500	73000;415-416	
crack	101500	73000	103000	69500;416-417	
crack	103000	69500	107000	52000;417-418	
crack	107000	52000	108500	46000;418-419	
crack	108500	46000	110000	35000;419-420	

crack	110000	35000	109500	29000;420-421
crack	109500	29000	109500	22000;421-422
crack	109500	22000	109000	21000;422-423
crack	109000	21000	108500	15000;423-424
crack	108500	15000	110500	8500;424-425
crack	110500	8500	112500	0;425-426
crack	109500	22000	114000	17000;422-445
crack	114000	17000	117000	14500;445-446
crack	117000	14500	122500	6000;446-447
crack	122500	6000	122500	4500;447-448
crack	122500	4500	124000	3000;448-449
crack	101500	73000	107000	68000;416-434
crack	107000	68000	111500	59000;434-435
crack	111500	59000	112000	49000;435-436
crack	112000	49000	113000	41000;436-437
crack	113000	41000	117000	29000;437-438
crack	117000	29000	115000	28500;438-439
crack	115000	28500	115000	27000;439-440
crack	115000	27000	114000	26000;440-441
crack	109500	29000	114000	26000;421-441
crack	114000	26000	118500	23000;441-442
crack	118500	23000	120000	21000;442-443
crack	120000	21000	121500	20500;443-444
crack	117000	29000	123000	32000;438-450
crack	123000	32000	124000	31000;450-451
crack	124000	165000	123000	163000;452-453
crack	123000	163000	117000	160000;453-454
crack	117000	160000	117000	153000;454-455
crack	117000	153000	117500	145000;455-456
crack	117500	145000	115500	138000;456-457
crack	115500	138000	113000	135000;457-458
crack	113000	135000	113500	130000;458-459
crack	113500	130000	112500	125000;459-460
crack	112500	125000	112000	120000;460-461
crack	112000	120000	110000	114500;461-462
crack	110000	114500	106500	110000;462-463
crack	106500	110000	104000	105000;463-464
crack	104000	105000	104500	102000;464-465
crack	104500	102000	105500	100000;465-466
crack	105500	100000	106000	95000;466-467
crack	106000	95000	109500	84000;467-468
crack	109500	84000	111500	82000;468-469
crack	111500	82000	112000	80000;469-470 gr9 bound centr:112000,114000,80000,82000
crack	112000	80000	113000	78000;470-471 gr9 bound
crack	113000	78000	114500	76500;471-472 gr9 bound
crack	114500	76500	115000	77000;472-473 gr9 bound
crack	115000	77000	115000	82000;473-474 gr9 bound
crack	115000	82000	114000	84000;474-475 gr9 bound
crack	114000	84000	113000	85000;475-476 gr9 bound
crack	113000	85000	112000	85000;476-477 gr9 bound
crack	112000	85000	111000	84000;477-478 gr9 bound
crack	111000	84000	111500	82000;478-469 gr9 bound
crack	114500	76500	115500	75000;472-479
crack	115500	75000	117000	70000;479-480
crack	117000	70000	120500	61000;480-481
crack	120500	61000	121000	59000;481-482
crack	121000	59000	120000	54500;482-483
crack	120000	54500	123000	45000;483-484
crack	123000	45000	122500	41000;484-485
crack	122500	41000	124000	39000;485-486
crack	123000	163000	122000	159000;453-487
crack	122000	159000	120000	147000;487-488
crack	120000	147000	119500	142000;488-489
crack	119500	142000	121000	137000;489-490
crack	121000	137000	121500	129000;490-491
crack	121500	129000	122000	122000;491-492
crack	122000	122000	121000	117000;492-493
crack	121000	117000	119500	115000;493-494
crack	119500	115000	115000	107000;494-495
crack	115000	107000	118500	105500;495-496
crack	118500	105500	117000	104000;496-497
crack	117000	104000	115000	100500;497-498
crack	115000	100500	115000	96000;498-499
crack	115000	96000	116000	92500;499-500
crack	116000	92500	119000	89000;500-501

crack	119000	89000	121500	87500;501-515
crack	118500	105500	117000	102000;496-509
crack	117000	102000	117000	99000;509-510
crack	117000	99000	119000	94500;510-511
crack	119000	94500	121500	94500;511-512
crack	121500	94500	123000	92500;512-513
crack	123000	92500	122000	91000;513-514
crack	122000	91000	121500	87500;514-515
crack	121500	87500	121000	84500;515-516
crack	118500	105500	119500	104000;496-502
crack	119500	104000	119500	101000;502-503
crack	119500	101000	122000	98000;503-504
crack	122000	98000	124000	98000;504-505
crack	119500	101000	120000	97500;503-506
crack	120000	97500	123000	94500;506-507
crack	123000	94500	124000	94500;507-508
crack	113500	130000	114000	125000;459-520
crack	114000	125000	113000	114000;520-521
crack	113000	114000	112500	111000;521-522
crack	112500	111000	113500	108000;522-523
crack	113500	108000	113000	89500;523-524
crack	105500	100000	113000	89500;466-524
crack	113000	89500	120500	80000;524-525
crack	120500	80000	120500	77000;525-526
crack	120500	77000	118500	74000;526-527
crack	118500	74000	118000	71000;527-528
crack	118000	71000	120500	65000;528-532
crack	120500	65000	120500	61000;532-481
crack	121000	84500	120500	80000;516-525
crack	121000	84500	123000	82000;516-517
crack	123000	82000	124000	81000;517-518
crack	123000	82000	124000	86500;517-519
crack	124000	86500	122500	80000;517-529
crack	122500	80000	122500	76000;529-530
crack	122500	76000	120000	72000;530-531
crack	120000	72000	120500	65000;531-532
crack	124000	70000	123500	68500;533-534 gr10 bound centr: 122000,124000,66000,67000
crack	123500	68500	122500	67500;534-535 gr10 bound
crack	122500	67500	122500	65500;535-536 gr10 bound
crack	122500	65500	123000	64000;536-537 gr10 bound
crack	123000	64000	124000	63000;537-538 gr10 bound
crack	52000	176000	57000	169500;53-539
crack	57000	169500	56000	168000;539-540
crack	56000	168000	53000	168500;540-541
crack	53000	168500	49000	171000;541-542
crack	49000	171000	43500	171500;542-543
crack	43500	171500	44000	170000;543-544
crack	44000	170000	52000	168000;544-545
crack	52000	168000	49000	162000;545-546
crack	49000	162000	48000	161000;546-547
crack	48000	161000	47000	157000;547-548
crack	47000	157000	43000	150000;548-69

;Pseudo contacts to reduce block size and allow zoning

;crack	0	66000	39000	66000;Pj1(left block)
;crack	47000	71000	96000	71000;Pj2(mid block)
;crack	80000	135000	114000	135000;Pj3(rmid block)
;crack	90000	102000	106000	102000;Pj4(rmid block)
;crack	104000	70000	108000	70000;Pj5(rmid block)
;crack	90000	102000	106000	102000;Pj6(rmid block)
crack	88000	110000	90000	110000;Pj7(rmid block)
;crack	103000	127000	113000	127000;Pj8(rmid block)
crack	99000	107000	106000	107000;Pj9(rmid block)
crack	101000	98000	106000	98000;Pj10(rmid block)
;crack	55000	38000	59000	38000;Pj11(rmid block)
crack	93000	115000	95000	115000;Pj12(rmid block)

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;New 1490 granites geometry and faults (above data may be out-commented)
;denoted by b

crack	18500	200000	19000	197000;b1-b2
crack	19000	197000	21500	195000;b2-b3
crack	21500	200000	21500	195000;21-b3
crack	21500	195000	21500	189000;b3-22

crack	19000	197000	18000	195000;b2-b4
crack	18000	195000	21000	186000;b4-b6
crack	21500	189000	21000	186000;22-b6
crack	21000	186000	20000	182000;b6-23
crack	18000	195000	14000	191000;b4-b5
crack	14000	191000	11500	183000;b5-b7
crack	11500	183000	7500	178000;b7-b8
crack	7500	178000	9000	171000;b8-b9
crack	7500	178000	6000	176000;b8-b11
crack	9000	171000	6000	174000;b9-b10
crack	6000	174000	6000	176000;b10-b11
crack	6000	174000	6500	170000;b10-b17
crack	6000	176000	1500	170000;b11-13
crack	1500	170000	0	169000;13-b12
crack	0	169000	1000	157000;b12-b13
crack	1000	157000	3000	154000;b13-b14
crack	3000	154000	2000	152000;b14-b15
crack	2000	152000	0	151000;b15-b16
crack	6500	170000	8500	160000;b17-b18
crack	9500	162000	8500	160000;29-b18
crack	8500	160000	5000	155000;b18-15
crack	26000	200000	24000	194000;b19-b20
crack	24000	194000	23500	187000;b20-b21
crack	23500	187000	24000	184000;b21-b22
crack	24000	184000	23000	181000;b22-blank
crack	23000	181000	19500	179000;blank-24
crack	24000	184000	23000	178000;b22-b23
crack	23000	178000	20000	171000;b23-b24
crack	20000	171000	20000	162500;b24-b25
crack	21000	163000	20000	162500;61-b25
crack	20000	162500	11000	158000;b25-62
crack	30000	200000	28000	197000;b26-b27
crack	28000	197000	27500	194000;b27-b28
crack	27500	194000	25500	193000;b28-b29
crack	27500	200000	25500	193000;25-b29
crack	25500	193000	24500	190000;b29-b30
crack	24500	190000	23000	185000;b30-26
crack	24500	190000	28000	186000;b30-b33
crack	32000	200000	27000	190000;b31-b32
crack	27000	190000	28000	186000;b32-b33
crack	28000	186000	30000	184000;b33-b34
crack	27000	190000	30000	187000;b32-b38
crack	30000	187000	30000	184000;b38-b34
crack	30000	184000	32500	176000;b34-b35
crack	32500	176000	34500	176000;b35-b36
crack	34500	176000	37500	171000;b36-b37
crack	38500	179000	37500	171000;58-b37
crack	37500	171000	37000	169000;b37-59
crack	30000	187000	31000	186000;b38-b39
crack	31000	186000	31500	183000;b39-b40
crack	31500	183000	34000	180000;b40-b41
crack	34000	180000	36500	175000;b41-b42
crack	36500	175000	38500	173000;b42-58
crack	31000	186000	38000	177000;b39-b43
crack	38000	179000	38000	177000;57-b43
crack	38000	177000	38500	173000;b43-58
crack	37500	200000	37500	197000;b44-b45
crack	37500	197000	39500	196000;b45-b46
crack	39500	196000	43000	192000;b46-b47
crack	38500	200000	39500	196000;b48-b46
crack	39500	200000	42500	195000;b49-b51
crack	41000	200000	42500	195000;b50-b51; gr12 bound centr:55000,68000,184000,193000
crack	42500	195000	43000	192000;b51-b47
crack	43000	192000	43000	188000;b47-b52
crack	43000	188000	48000	182500;b52-b53
crack	48000	182500	49500	178000;b53-b54
crack	49500	178000	51000	177000;b54-b55
crack	51000	177000	52000	178500;b55-b56
crack	52000	178500	53000	179500;b56-40
crack	64000	181000	62000	181000;36-37 gr1/12 bound
crack	62000	181000	61000	180000;37-38 gr1/12 bound
crack	61000	180000	54500	180000;38-39 gr1/12 bound
crack	54500	180000	53000	179500;39-40 gr1/12 bound
crack	64000	181000	64500	182500;36-b57
crack	64500	182500	65500	182500;b57-b58

crack	65500	182500	67000	180000;b58-b59
crack	67000	180000	67000	178000;b59-b60
crack	67000	178000	70500	178000;b60-b61
crack	70500	178000	70000	179500;b61-b62
crack	70000	179500	68000	180500;b62-b63
crack	68000	180500	68000	183000;b63-b64
crack	68000	183000	70000	182500;b64-b65
crack	70000	182500	73000	180000;b65-b66
crack	73000	180000	75500	181000;b66-b67
crack	75500	181000	75500	182500;b67-b68
crack	75500	182500	79000	184500;b68-b69
crack	79000	184500	81000	187000;b69-b70
crack	81000	187000	84000	193000;b70-b80
crack	84000	193000	85000	195000;b80-b81
crack	85000	195000	83000	195500;b81-b82
crack	83000	195500	81000	197500;b82-b83
crack	81000	197500	80000	196000;b83-b84
crack	80000	196000	79000	197000;b84-b85
crack	79000	197000	78000	198000;b85-b86
crack	78000	198000	77000	200000;b86-b87
crack	84000	193000	85500	192500;b80-b89
crack	87500	200000	85500	192500;b88-b89
crack	85500	192500	96000	189000;b89-b90
crack	96000	189000	99000	200000;b90-b91
crack	99000	190000	105000	194500;241-b92
crack	105000	194500	105000	196000;b92-250
crack	108000	200000	108500	193000;b93-b94
crack	108500	193000	112000	200000;b94-b95
crack	99000	182000	99000	179000;253-b96
crack	99000	179000	96500	176000;b96-b97
crack	96500	176000	94000	175000;b97-b98
crack	94000	175000	92000	176000;b98-b101
crack	94000	175000	92000	173000;b98-b99
crack	92000	173000	91500	176500;b99-b100
crack	92000	176000	91500	176500;b101-b100
crack	91500	176500	91000	179000;b100-255
crack	91000	179000	88000	180000;255-b102
crack	91000	179000	90000	178000;255-b104
crack	88000	180000	87500	179500;b102-b103
crack	87500	179500	90000	178000;b103-b104
crack	87500	179500	85000	177000;b103-b105
crack	85000	177000	82000	174000;b105-258
crack	85000	177000	84000	182000;b105-b106
crack	84000	182000	85000	185000;b106-239
crack	85000	177000	88000	176000;b105-b107
crack	90000	178000	88000	176000;b104-b107
crack	88000	176000	87000	175000;b107-256
crack	81000	187000	79000	181000;b70-b108
crack	79000	181000	72000	175000;b108-225
crack	72000	175000	69000	173000;225-b109
crack	69000	173000	65000	170000;b109-224
crack	69000	173000	63000	178000;b109-b110
crack	63000	178000	64000	181000;b110-36
crack	63000	178000	63000	177000;b110-52
crack	65500	182500	64000	173000;b58-b111
crack	64000	173000	65000	170000;b111-224
crack	64000	173000	57000	171000;b111-44
crack	65000	170000	72000	165000;224-b112
crack	72000	165000	73000	163000;b112-b113
crack	73000	163000	72000	151500;b113-b114
crack	68000	158000	72000	151500;260-b114
crack	72000	151500	82000	133000;b114-261
crack	72000	165000	80000	159000;b112-b115
crack	80000	159000	79000	165000;b115-228
crack	80000	159000	80000	158000;b115-b116
crack	80000	158000	88000	155000;b116-b117
crack	88000	155000	95000	153000;b117-b118
crack	95000	153000	97000	152000;b118-b119
crack	97000	152000	96500	150000;b119-b120
crack	96500	150000	96500	145000;b120-b121
crack	96500	145000	96500	141000;b121-b122
crack	96500	141000	95000	135000;b122-b123
crack	96500	145000	95000	141000;b121-b124
crack	95000	135000	95000	141000;b123-b124
crack	95000	135000	94000	129000;b123-376

crack	97000	152000	117000	144000;b119-b125
crack	117500	145000	117000	144000;456-b125
crack	117000	184500	115500	138000;b125-457
crack	103000	127000	108000	123000;383-b126
crack	108000	123000	112500	124000;b126-b127
crack	112500	124000	114000	123000;b127-b128
crack	114000	123000	114000	124000;b128-b129
crack	114000	124000	122000	122000;b129-492
crack	47000	179000	48000	177000;54-b130
crack	48000	177000	51000	175000;b130-b131
crack	51000	175000	53250	175000;b131-b132
crack	45000	179000	56500	169000;55-b133
crack	57000	169500	56500	169000;539-b133
crack	56500	169000	56000	168000;b133-540
crack	56000	168000	57000	165000;540-b134
crack	57000	165000	54000	165500;b134-b135
crack	54000	165500	53000	165000;b135-b136
crack	53000	165000	52000	163500;b136-b137
crack	52000	163500	58000	156000;b137-b138
crack	58000	156000	62000	150000;b138-b139
crack	62000	150000	69000	143500;b139-b140
crack	69000	143500	73000	137500;b140-b141
crack	73000	137500	74000	134000;b141-b142
crack	74000	134000	73000	129000;b142-b143
;-----				
crack	73000	129000	71000	126000;b143-b144
crack	71000	126000	74000	124000;b144-b145
crack	74000	124000	77500	124000;b145-b146
crack	77500	124000	83000	121000;b146-b147
crack	83000	121000	85500	119000;b147-b148
crack	84000	125000	85500	119000;274-b148
crack	85500	119000	86500	115000;b148-285
crack	62000	150000	64000	139000;b139-b153
crack	64000	139000	64000	133000;b153-b152
crack	64000	133000	68000	124000;b152-b151
crack	71000	126000	68000	124000;b144-b151
crack	71000	126000	69500	122000;b144-b149
crack	69500	122000	68500	120000;b149-b150
crack	68500	120000	68000	124000;b150-b151
crack	68000	124000	60500	114000;b151-b180
crack	69500	122000	70000	120000;b149-b154
crack	70000	120000	72000	118000;b154-b155
crack	72000	118000	74000	117500;b155-b156
crack	74000	117500	77000	115000;b156-b157
crack	77000	115000	79500	111500;b157-b158
crack	79500	111500	81000	113000;b158-296
crack	79500	111500	78000	110000;b158-297
crack	70000	120000	72000	112000;b154-b159
crack	72000	112000	74000	107500;b159-b160
crack	74000	107500	76500	105000;b160-b170
crack	76500	105000	78500	104000;b170-b171
crack	78500	104000	77500	107000;b171-299
crack	78500	104000	81500	100000;b171-300
crack	76500	105000	76500	103000;b170-b172
crack	76500	103000	81500	100000;b172-300
crack	72000	112000	72000	110000;b159-b173
crack	72000	110000	73500	105000;b173-b174
crack	73500	105000	76500	103000;b174-b172
crack	73500	105000	77000	94000;b174-b175
crack	77000	94000	80000	89500;b175-b385
crack	81500	100000	82000	98000;300-b176
crack	82000	98000	82000	97000;b176-b177
crack	82000	97000	85500	95000;b177-b178
crack	85500	95000	86000	96000;b178-304
crack	85500	95000	85000	94000;b178-305
crack	82000	97000	83000	91000;b177-b179
crack	83000	91000	85000	89000;b179-308
crack	52000	163500	51000	161000;b137-b181
crack	51000	161000	51500	154000;b181-b182
crack	51500	154000	51500	147000;b182-b183
crack	51500	147000	52000	144000;b183-b184
crack	52000	144000	54000	141000;b184-b185
crack	54000	141000	55000	137000;b185-b186
crack	55000	137000	57000	128000;b186-b187
crack	57000	128000	59000	124000;b187-b188

crack	59000	124000	60500	121000;b188-b189
crack	60500	121000	60500	114000;b189-b180
crack	60500	114000	59000	112000;b180-b197
crack	51000	161000	49000	157000;b181-b190
crack	49000	157000	49500	152000;b190-b191
crack	49500	152000	51500	154000;b191-b182
crack	49500	152000	49500	150000;b191-b192
crack	49500	150000	51500	147000;b192-b183
crack	49500	150000	50000	140000;b192-b193
crack	50000	140000	55000	131000;b193-b194
crack	55000	131000	57500	125000;b194-b195
crack	57500	125000	58500	121000;b195-b196
crack	58500	121000	59000	112000;b196-b197
crack	49500	152000	49000	150000;b191-b198
crack	49000	150000	49000	140000;b198-b199
crack	49000	140000	51000	135000;b199-b200
crack	51000	135000	51500	133000;b200-b201
crack	51500	133000	44000	142000;b201-96
crack	51500	133000	53000	131000;b201-97
crack	59000	112000	62000	109000;b197-b202
crack	62000	109000	63500	106000;b202-b203
crack	63500	106000	67500	98000;b203-b204
crack	67500	98000	68000	95000;b204-b205
crack	68000	95000	73500	86000;b205-b456
crack	68000	95000	64000	102000;b205-b206
crack	64000	102000	63500	106000;b206-b203
crack	62000	109000	62000	101000;b202-b207
crack	62000	101000	63500	98000;b207-b208
crack	63500	98000	62500	93000;b208-b209
crack	62500	93000	62500	86000;b209-b210
crack	62500	86000	63000	83000;b210-b211
crack	63000	83000	64500	81000;b211-b450
crack	59000	112000	57000	109000;b197-b212
crack	57000	109000	54000	105000;b212-b213
crack	54000	105000	51500	104000;b213-b243
crack	54000	105000	55500	103000;b213-b214
crack	55500	103000	55000	102000;b214-b244
crack	55000	112000	54000	105000;99-b213
crack	57000	109000	58000	102000;b212-blank
crack	58000	102000	58000	96500;blank-b215
crack	58000	96500	56000	94000;b215-b247
crack	56000	94000	55000	91000;b247-b216
crack	55000	91000	54000	89000;b216-b217
crack	54000	89000	51500	86000;b217-b218
crack	51500	86000	51000	84000;b218-b219
crack	51000	84000	53000	81500;b219-b220
crack	53000	81500	54500	79500;b220-b221
crack	54500	79500	60000	69000;b221-b445
crack	54500	79500	55000	74000;b221-b222
crack	55000	74000	57000	68000;b222-b223
crack	57000	68000	59000	63000;b223-b224
crack	59000	63000	61000	53000;b224-b375
crack	53000	81500	52500	79000;b220-b225
crack	52500	79000	51500	75000;b225-b226
crack	51500	75000	53000	71000;b226-b227
crack	53000	71000	56500	64000;b227-b228
crack	56500	64000	59000	57000;b228-b229
crack	59000	57000	60000	51000;b229-b376
crack	25000	118000	30000	117500;85-b230 gr13 co-ord cntr:20000,37000,93000,102000
crack	30000	117500	33000	117000;b230-b231
crack	33000	117000	36000	116000;b231-b232
crack	36000	116000	38000	114500;b232-b233
crack	38000	114500	41000	114500;b233-b234
crack	41000	114500	43000	113000;b234-b235
crack	43000	113000	46000	111000;b235-b236
crack	46000	111000	46500	109000;b236-b237
crack	46000	111000	52000	114000;b236-b201d
crack	52000	114000	53000	116000;b201d-b201c
crack	53000	116000	55000	117000;b201c-b201b
crack	55000	117000	55000	120000;b201b-98
crack	55000	117000	55000	112000;b201b-99
crack	46500	109000	47000	106000;b237-b238
crack	47000	106000	46000	105000;b238-b239
crack	46000	105000	45000	101000;b239-b240
crack	45000	101000	47000	104500;b240-b241

crack	47000	104500	49000	105000;b241-b242
crack	49000	105000	51500	104000;b242-b243
crack	51500	104000	55000	102000;b243-b244
crack	55000	102000	56000	100000;b244-b245
crack	56000	100000	56500	97000;b245-b246
crack	56500	97000	56000	94000;b246-b247
crack	56000	94000	52500	91000;b247-b248
crack	52500	91000	52000	89000;b248-100
crack	52000	89000	47000	85500;100-b249
crack	47000	85500	44000	81000;b249-102
crack	47000	85500	45000	84000;b249-101
crack	45000	84000	39500	82000;101-b250
crack	39500	82000	39000	80000;b250-b251
crack	39000	80000	35000	78000;b251-b252
crack	35000	78000	36000	79000;b252-b253
crack	36000	79000	35500	80000;b253-b254
crack	35500	80000	36000	82000;b254-b255
crack	36000	82000	34000	81500;b255-b256
crack	34000	81500	32000	80000;b256-b257
crack	32000	80000	31000	82000;b257-b258
crack	31000	82000	32000	83000;b258-b259
crack	32000	83000	28000	84000;b259-b260
crack	28000	84000	26000	83500;b260-b261
crack	26000	83500	17000	83500;b261-b262
crack	17000	83500	12000	87000;b262-b263
crack	12000	87000	8000	92000;b263-b264
crack	8000	92000	4500	97000;b264-b265
crack	4500	97000	3000	101000;b265-b266
crack	3000	101000	1000	103000;b266-b267
crack	1000	103000	0	104500;b267-b268 gr13 co-ords
crack	1000	103000	2000	100000;b267-b269
crack	2000	100000	3500	88000;b269-b270
crack	3500	88000	8000	92000;b270-b264
crack	3500	88000	4000	83500;b270-b274
crack	0	85000	1000	85000;b271-b272 gr14 co-ords cntr:6000,24000,45000,66000
crack	1000	85000	3000	83500;b272-b273
crack	3000	83500	4000	83500;b273-b274
crack	4000	83500	10000	82000;b274-b275
crack	10000	82000	14000	80500;b275-b276
crack	14000	80500	18000	78000;b276-b277
crack	18000	78000	23000	71000;b277-b278
crack	23000	71000	23500	68000;b278-b279
crack	23500	68000	24500	66000;b279-b280
crack	24500	66000	26000	60500;b280-b281
crack	26000	60500	28000	58000;b281-b282
crack	28000	58000	28000	52000;b282-b283
crack	28000	52000	29000	51000;b283-b284
crack	29000	51000	29000	43000;b284-b285
crack	29000	43000	31000	39000;b285-b286
crack	31000	39000	31000	38000;b286-b287
crack	31000	38000	30500	35000;b287-b288
crack	31000	38000	34000	36000;b287-203
crack	30500	35000	30000	33000;b288-b289
crack	30500	35000	36000	31000;b288-211
crack	30000	33000	29000	28000;b289-b290
crack	30000	33000	35000	31000;b289-b214
crack	29000	28000	32000	30000;b290-blank
crack	32000	30000	36000	25000;blank-b306
crack	36000	25000	35000	28000;b306-215
crack	36000	25000	36500	24000;b306-216
crack	29000	28000	22000	31000;b290-b291
crack	22000	31000	16000	34000;b291-b292
crack	16000	34000	12000	37000;b292-b293
crack	12000	37000	9000	39000;b293-b294
crack	9000	39000	4000	41500;b294-b295
crack	4000	41500	2000	45000;b295-b296
crack	2000	45000	0	47500;b296-b297
crack	31000	82000	29000	79000;b258-b298
crack	29000	79000	28500	71000;b298-b299
crack	28500	71000	30500	63000;b299-b300
crack	30500	63000	31000	55000;b300-209
crack	31000	55000	33000	53500;209-b305
crack	33000	53500	34000	53000;b305-196
crack	35000	78000	32000	74000;b252-b301
crack	32000	74000	31500	70000;b301-b302

crack	31500	70000	32000	65000;b302-b303
crack	32000	65000	33000	62000;b303-b304
crack	33000	62000	33000	53500;b304-b305
crack	51000	11000	53000	10000;159-b307 gr15 bound centr:49000,53000,3000,7000
crack	53000	10000	54500	7000;b307-b308
crack	54500	7000	55500	2000;b308-b309
crack	55500	2000	55000	0;b309-b310
crack	55500	39000	56500	33000;b311-b312 gr 16 bound centr:50500,54000,30000,33000
crack	56500	33000	58000	35000;b312-129
crack	56500	33000	55000	31000;b312-b130
crack	55000	31000	53500	30000;130-b313
crack	53500	30000	53000	28500;b313-b314
crack	53000	28500	51000	25000;b314-b315
crack	51000	25000	49500	25000;b315-b316
crack	49500	25000	49000	26000;b316-b317
crack	49000	26000	47500	26000;b317-b318
crack	47500	26000	48000	32000;b318-b319
crack	48000	32000	53000	35000;b319-b320
crack	53000	35000	53500	36500;b320-b321
crack	53500	36500	55000	38000;b321-137
crack	55000	38000	55500	39000;137-b311
crack	57000	27000	59000	28000;b322-b323 gr 17 bound centr:64000,73000,26250,27750
crack	59000	28000	61500	28000;b323-b324
crack	61500	28000	63000	28500;b324-b325
crack	63000	28500	68500	28000;b325-b326
crack	68500	28000	70000	29000;b326-b327
crack	70000	29000	71500	29000;b327-b328
crack	71500	29000	73000	29000;b328-b329
crack	73000	29000	74000	28500;b329-b330
crack	74000	28500	75000	28000;b330-b331
crack	75000	28000	78000	28000;b331-b332
crack	78000	28000	80000	27000;b332-b333
crack	80000	27000	80500	25500;b333-b334
crack	80500	25500	79000	26000;b334-b335
crack	79000	26000	77000	25000;b335-b336
crack	77000	25000	75000	24000;b336-b337
crack	75000	24000	71500	26000;b337-b338
crack	71500	26000	70000	26000;b338-b339
crack	70000	26000	69000	23000;b339-169
crack	70000	26000	69000	26000;b339-b340
crack	69000	26000	68000	25500;b340-b341
crack	68000	25500	66000	25500;b341-b342
crack	66000	25500	64000	25000;b342-b343
crack	64000	25000	61500	25000;b343-b344
crack	61500	25000	59000	22000;b344-b345
crack	59000	22000	57000	25000;b345-b346
crack	57000	25000	57000	27000;b346-b322
crack	57000	25000	53000	18000;b346-162
crack	59000	22000	59500	18000;b345-b347
crack	59500	18000	57500	12000;b347-b348
crack	57500	12000	57000	6000;b348-b349
crack	57000	6000	56000	4000;b349-165
crack	57000	6000	60000	14000;b349-167
crack	77000	25000	76000	23000;b336-b350
crack	76000	23000	73000	19000;b350-b351
crack	73000	19000	68000	15000;b351-b352
crack	68000	15000	66000	12000;b352-b353
crack	66000	12000	63000	0;b353-b354
crack	74000	28500	78000	33500;b330-b355
crack	78000	33500	79000	36000;b355-355b
crack	79000	36000	79500	39000;355b-355c
crack	78000	33500	72000	36000;b355-b356
crack	78000	33500	80500	32000;b355-b426
crack	72000	36000	71500	29000;b356-b328
crack	72000	36000	71500	43000;b356-b357
crack	71500	43000	73500	51000;b357-b358
crack	73500	51000	73000	55000;b358-b439
crack	59000	28000	61000	34000;b323-b359
crack	61000	34000	63000	39000;b359-b360
crack	63000	39000	63500	44000;b360-b364
crack	57000	27000	60000	34000;b322-b361
crack	60000	34000	61000	43000;b361-b362
crack	61000	43000	63000	43500;b362-b363 gr 18 bound cntr:63000,68000,48000,52000
crack	63000	43500	63500	44000;b363-b364
crack	63500	44000	64500	44500;b364-b365

crack	64500	44500	69000	48000;b365-b366
crack	69000	48000	71000	51000;b366-b367
crack	71000	51000	71500	53000;b367-b368
crack	71500	53000	70000	56000;b368-b369
crack	70000	56000	68000	55500;b369-b370
crack	68000	55500	67000	56000;b370-b371
crack	67000	56000	65000	60000;b371-b442
crack	67000	56000	66000	56000;b371-b372
crack	66000	56000	63500	55500;b372-b373
crack	63500	55500	63000	53500;b373-b374
crack	63000	53500	61000	53000;b374-b375
crack	61000	53000	60000	51000;b375-b376
crack	60000	51000	60000	50000;b376-b377
crack	60000	50000	61000	48000;b377-b378
crack	61000	48000	61000	46000;b378-b379
crack	61000	46000	60000	45500;b379-b380
crack	60000	45500	61000	43000;b380-b362
crack	69000	98000	71000	97500;b381-b382 gr 19 bound centr:82500,96000,44000,70000
crack	71000	97500	73000	96000;b382-b383
crack	73000	96000	79000	89000;b383-b384
crack	79000	89000	80000	89500;b384-b385
crack	80000	89500	82000	89500;b385-b386
crack	82000	89500	82000	87000;b386-b387
crack	82000	87000	84000	86500;b387-b388
crack	84000	86500	85000	85000;b388-b389
crack	85000	85000	87500	84000;b389-b390
crack	87500	84000	90000	83500;b390-b391
crack	90000	83500	91000	80500;b391-b392
crack	91000	80500	92000	82500;b392-413
crack	92000	82500	94000	82500;413-b393
crack	92000	82500	96000	77500;b393-b394
crack	96000	77500	98500	74000;b394-b395
crack	98500	74000	97000	72000;b395-b396
crack	97000	72000	97000	69000;b396-b397
crack	97000	69000	99500	67000;b397-b398
crack	99500	67000	99500	64000;b398-b399
crack	99500	64000	102000	61500;b399-b400
crack	102000	61500	103000	57000;b400-b401
crack	103000	57000	107000	52000;b401-418
crack	107000	52000	107000	48000;418-b402
crack	107000	48000	107000	46000;b402-b403
crack	107000	46000	106500	44000;b403-b404
crack	106500	44000	108000	42000;b404-b405
crack	108000	42000	109000	41000;b405-b406
crack	109000	41000	108500	46000;b406-419
crack	109000	41000	110000	35000;b406-420
crack	108000	42000	109000	36000;b405-b407
crack	109000	36000	107500	33000;b407-b408
crack	107500	33000	109500	31000;b408-b409
crack	109500	31000	110000	35000;b409-420
crack	109500	31000	109500	29000;b409-421
crack	107500	33000	106000	30000;b408-b410
crack	106000	30000	103000	29500;b410-433
crack	103000	29500	102500	26000;433-b411
crack	102500	26000	102000	24000;b411-412
crack	102000	24000	97000	20000;412-b413
crack	97000	20000	99000	17000;b413-b414
crack	99000	17000	99000	12000;b414-b415
crack	99000	12000	97500	9000;b415-b416
crack	97500	9000	96000	7000;b416-b417
crack	96000	7000	93000	7000;b417-b418
crack	93000	7000	91000	13000;b418-b419
crack	91000	13000	91500	16000;b419-b420
crack	91500	16000	93000	19000;b420-b421
crack	93000	19000	91000	20500;b421-b422
crack	91000	20500	88000	21000;b422-b423
crack	88000	21000	86000	20000;b423-b424
crack	86000	20000	85000	20000;b424-180
crack	85000	20000	83000	20000;180-179
crack	83000	20000	80000	29000;179-b425
crack	80000	29000	80500	32000;b425-b426
crack	80500	32000	79500	35000;b426-b427
crack	79500	35000	80500	38000;b427-b428
crack	80500	38000	79500	39000;b428-355c
crack	79500	39000	78000	40000;355c-b429

crack	78000	40000	79000	42000;b429-b430
crack	79000	42000	80500	43000;b430-b431
crack	79000	42000	81000	45500;b430-b432
crack	80500	43000	81000	45500;b431-b432
crack	81000	45500	82000	46000;b432-b433
crack	82000	46000	82500	47000;b433-b434
crack	82000	46000	80000	51000;b433-b436
crack	82500	47000	82000	50000;b434-b435
crack	82000	50000	80000	51000;b435-b436
crack	80000	51000	76000	53000;b436-b437
crack	76000	53000	75000	54000;b437-b438
crack	75000	54000	73000	55000;b438-b439
crack	73000	55000	69000	58500;b439-b440
crack	69000	58500	66000	59000;b440-b441
crack	66000	59000	65000	60000;b441-b442
crack	65000	60000	62500	62000;b442-b443
crack	62500	62000	60000	68000;b443-b444
crack	60000	68000	60000	69000;b444-b445
crack	60000	69000	60000	74000;b445-b446
crack	60000	74000	62000	76000;b446-b447
crack	62000	76000	63000	76000;b447-b448
crack	63000	76000	65000	78000;b448-b449
crack	65000	78000	64500	81000;b449-b450
crack	64500	81000	63500	86000;b450-b451
crack	63500	86000	66000	88500;b451-b452
crack	66000	88500	69000	88500;b452-b453
crack	69000	88500	71000	88000;b453-b454
crack	71000	88000	72000	85500;b454-b455
crack	72000	85500	73500	86000;b455-b456
crack	73500	86000	73000	91000;b456-b457
crack	73000	91000	70000	95000;b457-b458
crack	70000	95000	69000	98000;b458-b381
crack	98500	86000	99000	83000;412-b459
crack	100000	76000	99000	83000;415-b459
crack	99000	83000	101500	82000;b459-b460
crack	101500	82000	107000	77000;b460-b461
crack	107000	77000	111000	72000;b461-b462
crack	111000	72000	118000	67000;b462-b463
crack	118000	67000	117000	70000;b463-480
crack	118000	67000	120500	61000;b463-481
crack	124000	22500	123000	23000;b464-b465 gr 20 bound centr:122250,123500,19000,22000
crack	123000	23000	121500	26000;b465-b466
crack	121500	26000	117000	29000;b466-438
crack	123000	23000	121000	22000;b465-b467
crack	121000	22000	121500	20500;b467-444
crack	121500	20500	122000	19000;444-b468
crack	122000	19000	124000	17500;b468-b469
crack	108500	15000	110000	11000;424-b470
crack	110000	11000	110500	8500;b470-425
crack	110000	11000	112500	8000;b470-b471
crack	112500	8000	116000	6000;b471-b472
crack	116000	6000	117000	14000;b472-446
crack	116000	6000	120000	3000;b472-b473
crack	120000	3000	124000	2000;b473-b474
crack	109500	22000	107000	22500;422-b475
crack	107000	22500	102500	26000;b475-b411
crack	123000	32000	121000	34000;450-b476
crack	121000	34000	120000	37000;b476-b477
crack	120000	37000	119500	43000;b477-b478
crack	119500	43000	121000	43000;b478-b479
crack	121000	43000	122500	41000;b479-485

***** (Geometry File End) *****

:Psuedo contacts to reduce block size and allow zoning

;crack	0	66000	39000	66000:Pj1(left block)
;crack	47000	71000	96000	71000:Pj2(mid block)
;crack	80000	135000	114000	135000:Pj3(rmid block)
;crack	90000	102000	106000	102000:Pj4(rmid block)
;crack	104000	70000	108000	70000:Pj5(rmid block)
;crack	90000	102000	106000	102000:Pj6(rmid block)
crack	88000	110000	90000	110000:Pj7(rmid block)
;crack	103000	127000	113000	127000:Pj8(rmid block)
crack	99000	107000	106000	107000:Pj9(rmid block)
crack	101000	98000	106000	98000:Pj10(rmid block)


```

;crack 55000 38000 59000 38000;Pj11(rmid block)
crack 93000 115000 95000 115000;Pj12(rmid block)

hist unbal ; hist1
hist sxx 62000 100000;hist2 (red 2)
hist syy 62000 100000;hist3 (red 3)

hist sst 60000 41000;hist4 (yel 4)selwyn high strain zone
hist sst 43000 40000;hist5 (yel 5)left of gin ck gr
hist sst 69000 98000;hist6 (yel 6)tip of sq. hills gr
hist sst 61000 172000;hist7 (yel 7)cloncurry

sav m2a_block.sav

gen 0 124000 0 200000 auto 1000

insitu stress -210e6 0 -140e6 szz -175e6
bound stress -210e6 0 -140e6
damp auto

;changing whole model to mat=1 (schist)
change 0 200000 0 124000 mat=1 cons=3

;changing all joints to jmat=1
change 0 200000 0 124000 jmat=1 jcon=2

;changing granite blocks to mat=2 (granite) constit model 3
change 57000,60000,175000,180000 mat=2 con=3 ;gr1
change 83000,85000,126000,129000 mat=2 con=3 ;gr2
change 89000,91000,117000,119000 mat=2 con=3 ;gr3
change 97000,99000,124000,126000 mat=2 con=3 ;gr4
change 94000,96000,117000,119000 mat=2 con=3 ;gr5
change 96000,98000,108000,110000 mat=2 con=3 ;gr6
change 85500,87500,100500,102500 mat=2 con=3 ;gr7
change 98000,100000,97000,99000 mat=2 con=3 ;gr8
change 112000,114000,80000,82000 mat=2 con=3 ;gr9
change 122000,124000,66000,67000 mat=2 con=3 ;gr10
change 53000,55000,45000,47000 mat=2 con=3 ;gr11
change 55000,68000,184000,193000 mat=2 con=3 ;gr12
change 20000,37000,93000,102000 mat=2 con=3 ;gr13
change 6000,24000,45000,66000 mat=2 con=3 ;gr14
change 49000,53000,3000,7000 mat=2 con=3 ;gr15
change 50500,54000,30000,33000 mat=2 con=3 ;gr16
change 64000,73000,26250,27750 mat=2 con=3 ;gr17
change 63000,68000,48000,52000 mat=2 con=3 ;gr18
change 82500,96000,44000,70000 mat=2 con=3 ;gr19
change 122250,123500,19000,22000 mat=2 con=3 ;gr20

;changing granite edges to jmat=2 - must follow commands setting jmat=2 blocks
change jmat=2 range minterface 1 2

;changing pseudo joint properties to jmat=5
change jmat=5 range xr 0,39000 yr 65900 66100 ang -5,5;Pj1 properties
;pl hold mat jo
change jmat=5 range xr 47000,96000 yr 70900 71100 ang -5,5;Pj2 properties
;pl hold mat jo
change jmat=5 range xr 80000,114000 yr 134900 135100 ang -5,5; Pj3 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj4 properties
change jmat=5 range xr 104000,108000 yr 69900 70100 ang -5,5; Pj5 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj6 properties
change jmat=5 range xr 88000,90000 yr 109900 110100 ang -5,5; Pj7 properties
;pl hold mat jo
change jmat=5 range xr 103000,113000 yr 126900 127100 ang -5,5; Pj8 properties
;pl hold mat jo
change jmat=5 range xr 99000,106000 yr 106900 107100 ang -5,5; Pj9 properties
;pl hold mat jo
change jmat=5 range xr 101000,106000 yr 97900 98100 ang -5,5; Pj10 properties
;pl hold mat jo
change jmat=5 range xr 55000,59000 yr 37900 38100 ang -5,5; Pj11 properties
;pl hold mat jo
change jmat=5 range xr 93000,95000 yr 114900 115100 ang -5,5; Pj12 properties

;Create Movie files every 100 steps

```

```
;plot ccfail blo bla
;movie on file m2a.dcx step 500
```

```
sav m2a_prop.sav
step 10
sav m2a_stress.sav
```

```
step 500
sav m2a_1.sav
step 500
sav m2a_2.sav
step 500
sav m2a_3.sav
step 500
sav m2a_4.sav
```

```
step 500
sav m2a_5.sav
step 500
sav m2a_6.sav
step 500
sav m2a_7.sav
step 500
sav m2a_8.sav
```

```
return
```

U.6 Model 2b – dry model $\sigma_1 = 112.5^\circ$

```
>1490Ma (Map Interp)MODEL 2 Young Granites- DRY MODEL
```

```
;metasediment properties
prop mat=1 dens 2850 bulk 25e9 shear 25e9 cohesion 10e6 tens 5e6 fric 31 dil 4
```

```
;granite properties
prop mat=2 dens 2650 bulk 49e9 shear 27e9 cohesion 20e6 tens 10e6 fric 37 dil 5
```

```
;contact properties
prop jmat=1 jkn 5e6 jks 1e3 jcoh 4e2 jtens 2e6 jfri 30 jdil 5
;prop jmat=1 jper 300 azero 0.05 ares 0.03
```

```
prop jmat=2 jkn 5e9 jks 1e5 jcoh 10e2 jtens 3e6 jfri 35 jdil 5
;prop jmat=2 jper 238 azero 0.03 ares 0.01
```

```
;Pseudo joints
prop jmat=5 jkn 100e9 jks 40e9 jcoh 190e10 jtens 190e10 jdil 0
;prop jmat=5 jper 0 azero 0 ares 0
```

```
round 100
```

```
block 0,0 0,200000 124000,200000 124000,0
```

```
;*****(Geometry File as Model 2a)*****
```

```
;Pseudo contacts to reduce block size and allow zoning
;crack 0 66000 39000 66000;Pj1(left block)
;crack 47000 71000 96000 71000;Pj2(mid block)
;crack 80000 135000 114000 135000;Pj3(rmid block)
;crack 90000 102000 106000 102000;Pj4(rmid block)
;crack 104000 70000 108000 70000;Pj5(rmid block)
;crack 90000 102000 106000 102000;Pj6(rmid block)
;crack 88000 110000 90000 110000;Pj7(rmid block)
;crack 103000 127000 113000 127000;Pj8(rmid block)
;crack 99000 107000 106000 107000;Pj9(rmid block)
;crack 101000 98000 106000 98000;Pj10(rmid block)
;crack 55000 38000 59000 38000;Pj11(rmid block)
;crack 93000 115000 95000 115000;Pj12(rmid block)
```

```
hist unbal ; hist1
hist sxx 62000 100000;hist2 (red 2)
hist syy 62000 100000;hist3 (red 3)
```

```

hist sst 60000 41000;hist4 (yel 4)selwyn high strain zone
hist sst 43000 40000;hist5 (yel 5)left of gin ck gr
hist sst 69000 98000;hist6 (yel 6)tip of sq. hills gr
hist sst 61000 172000;hist7 (yel 7)cloncurry

sav m2a_block.sav

gen 0 124000 0 200000 auto 1000

insitu stress -210e6 52.5e6 -140e6 szz -175e6
bound stress -210e6 0 -140e6
damp auto

;changing whole model to mat=1 (schist)
change 0 200000 0 124000 mat=1 cons=3

;changing all joints to jmat=1
change 0 200000 0 124000 jmat=1 jcon=2

;changing granite blocks to mat=2 (granite) constit model 3
change 57000,60000,175000,180000 mat=2 con=3 ;gr1
change 83000,85000,126000,129000 mat=2 con=3 ;gr2
change 89000,91000,117000,119000 mat=2 con=3 ;gr3
change 97000,99000,124000,126000 mat=2 con=3 ;gr4
change 94000,96000,117000,119000 mat=2 con=3 ;gr5
change 96000,98000,108000,110000 mat=2 con=3 ;gr6
change 85500,87500,100500,102500 mat=2 con=3 ;gr7
change 98000,100000,97000,99000 mat=2 con=3 ;gr8
change 112000,114000,80000,82000 mat=2 con=3 ;gr9
change 122000,124000,66000,67000 mat=2 con=3 ;gr10
change 53000,55000,45000,47000 mat=2 con=3 ;gr11
change 55000,68000,184000,193000 mat=2 con=3 ;gr12
change 20000,37000,93000,102000 mat=2 con=3 ;gr13
change 6000,24000,45000,66000 mat=2 con=3 ;gr14
change 49000,53000,3000,7000 mat=2 con=3 ;gr15
change 50500,54000,30000,33000 mat=2 con=3 ;gr16
change 64000,73000,26250,27750 mat=2 con=3 ;gr17
change 63000,68000,48000,52000 mat=2 con=3 ;gr18
change 82500,96000,44000,70000 mat=2 con=3 ;gr19
change 122250,123500,19000,22000 mat=2 con=3 ;gr20

;changing granite edges to jmat=2 - must follow commands setting jmat=2 blocks
change jmat=2 range minterface 1 2

;changing pseudo joint properties to jmat=5
change jmat=5 range xr 0,39000 yr 65900 66100 ang -5,5;Pj1 properties
;pl hold mat jo
change jmat=5 range xr 47000,96000 yr 70900 71100 ang -5,5;Pj2 properties
;pl hold mat jo
change jmat=5 range xr 80000,114000 yr 134900 135100 ang -5,5;Pj3 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj4 properties
change jmat=5 range xr 104000,108000 yr 69900 70100 ang -5,5; Pj5 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj6 properties
change jmat=5 range xr 88000,90000 yr 109900 110100 ang -5,5; Pj7 properties
;pl hold mat jo
change jmat=5 range xr 103000,113000 yr 126900 127100 ang -5,5; Pj8 properties
;pl hold mat jo
change jmat=5 range xr 99000,106000 yr 106900 107100 ang -5,5; Pj9 properties
;pl hold mat jo
change jmat=5 range xr 101000,106000 yr 97900 98100 ang -5,5; Pj10 properties
;pl hold mat jo
change jmat=5 range xr 55000,59000 yr 37900 38100 ang -5,5; Pj11 properties
;pl hold mat jo
change jmat=5 range xr 93000,95000 yr 114900 115100 ang -5,5; Pj12 properties

;Create Movie files every 100 steps
;plot ccfail blo bla
;movie on file m2b.dcx step 500

sav m2b_prop.sav
step 10
sav m2b_stress.sav

```

```

step 500
sav m2b_1.sav
step 500
sav m2b_2.sav
step 500
sav m2b_3.sav
step 500
sav m2b_4.sav

```

```

step 500
sav m2b_5.sav
step 500
sav m2b_6.sav
step 500
sav m2b_7.sav
step 500
sav m2b_8.sav

```

```
return
```

U.7 Model 2c – wet model $\sigma_1 = 90^\circ$

```

;>1490Ma (Map Interp)MODEL 2 Young Granites- DRY MODEL

;metasediment properties
prop mat=1 dens 2850 bulk 25e9 shear 25e9 cohesion 10e6 tens 5e6 fric 31 dil 4

;granite properties
prop mat=2 dens 2650 bulk 49e9 shear 27e9 cohesion 20e6 tens 10e6 fric 37 dil 5

;contact properties
prop jmat=1 jkn 5e6 jks 1e3 jcoh 4e2 jtens 2e6 jfri 30 jdil 5
;prop jmat=1 jper 300 azero 0.05 ares 0.03

prop jmat=2 jkn 5e9 jks 1e5 jcoh 10e2 jtens 3e6 jfri 35 jdil 5
;prop jmat=2 jper 238 azero 0.03 ares 0.01

;Pseudo joints
prop jmat=5 jkn 100e9 jks 40e9 jcoh 190e10 jtens 190e10 jdil 0
;prop jmat=5 jper 0 azero 0 ares 0

round 100

block 0,0 0,200000 124000,200000 124000,0

;*****(Geometry File as per Model 2a)*****

;Psuedo contacts to reduce block size and allow zoning
;crack 0 66000 39000 66000;Pj1(left block)
;crack 47000 71000 96000 71000;Pj2(mid block)
;crack 80000 135000 114000 135000;Pj3(rmid block)
;crack 90000 102000 106000 102000;Pj4(rmid block)
;crack 104000 70000 108000 70000;Pj5(rmid block)
;crack 90000 102000 106000 102000;Pj6(rmid block)
crack 88000 110000 90000 110000;Pj7(rmid block)
;crack 103000 127000 113000 127000;Pj8(rmid block)
crack 99000 107000 106000 107000;Pj9(rmid block)
crack 101000 98000 106000 98000;Pj10(rmid block)
;crack 55000 38000 59000 38000;Pj11(rmid block)
crack 93000 115000 95000 115000;Pj12(rmid block)

hist unbal ; hist1
hist sxx 62000 100000;hist2
hist syy 62000 100000;hist3

hist sst 60000 41000;hist4 selwyn high strain zone
hist sst 43000 40000;hist5 left of gin ck gr
hist sst 69000 98000;hist6 tip of sq. hills gr
hist sst 61000 172000;hist7 cloncurry

```

```

sav m2c_block.sav

gen 0 124000 0 200000 auto 1000

insitu stress -210e6 0 -140e6 szz -175e6
bound stress -210e6 0 -140e6
damp auto

;changing whole model to mat=1 (schist)
change 0 200000 0 124000 mat=1 cons=3

;changing all joints to jmat=1
change 0 200000 0 124000 jmat=1 jcon=2

;changing granite blocks to mat=2 (granite) constit model 3
change 57000,60000,175000,180000 mat=2 con=3 ;gr1
change 83000,85000,126000,129000 mat=2 con=3 ;gr2
change 89000,91000,117000,119000 mat=2 con=3 ;gr3
change 97000,99000,124000,126000 mat=2 con=3 ;gr4
change 94000,96000,117000,119000 mat=2 con=3 ;gr5
change 96000,98000,108000,110000 mat=2 con=3 ;gr6
change 85500,87500,100500,102500 mat=2 con=3 ;gr7
change 98000,100000,97000,99000 mat=2 con=3 ;gr8
change 112000,114000,80000,82000 mat=2 con=3 ;gr9
change 122000,124000,66000,67000 mat=2 con=3 ;gr10
change 53000,55000,45000,47000 mat=2 con=3 ;gr11
change 55000,68000,184000,193000 mat=2 con=3 ;gr12
change 20000,37000,93000,102000 mat=2 con=3 ;gr13
change 6000,24000,45000,66000 mat=2 con=3 ;gr14
change 49000,53000,3000,7000 mat=2 con=3 ;gr15
change 50500,54000,30000,33000 mat=2 con=3 ;gr16
change 64000,73000,26250,27750 mat=2 con=3 ;gr17
change 63000,68000,48000,52000 mat=2 con=3 ;gr18
change 82500,96000,44000,70000 mat=2 con=3 ;gr19
change 122250,123500,19000,22000 mat=2 con=3 ;gr20

;changing granite edges to jmat=2 - must follow commands setting jmat=2 blocks
change jmat=2 range minterface 1 2

;changing pseudo joint properties to jmat=5
change jmat=5 range xr 0,39000 yr 65900 66100 ang -5,5;Pj1 properties
;pl hold mat jo
change jmat=5 range xr 47000,96000 yr 70900 71100 ang -5,5;Pj2 properties
;pl hold mat jo
change jmat=5 range xr 80000,114000 yr 134900 135100 ang -5,5; Pj3 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj4 properties
change jmat=5 range xr 104000,108000 yr 69900 70100 ang -5,5; Pj5 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj6 properties
change jmat=5 range xr 88000,90000 yr 109900 110100 ang -5,5; Pj7 properties
;pl hold mat jo
change jmat=5 range xr 103000,113000 yr 126900 127100 ang -5,5; Pj8 properties
;pl hold mat jo
change jmat=5 range xr 99000,106000 yr 106900 107100 ang -5,5; Pj9 properties
;pl hold mat jo
change jmat=5 range xr 101000,106000 yr 97900 98100 ang -5,5; Pj10 properties
;pl hold mat jo
change jmat=5 range xr 55000,59000 yr 37900 38100 ang -5,5; Pj11 properties
;pl hold mat jo
change jmat=5 range xr 93000,95000 yr 114900 115100 ang -5,5; Pj12 properties

sav m2c_prop.sav
step 10
sav m2c_stress.sav

step 500
sav m2c_1.sav
step 500
sav m2c_2.sav
step 500
sav m2c_3.sav
step 500
sav m2c_4.sav

```

```

:Establishing fluid pressure
fluid dens=1000;fluid density of 1000kgm'3
set flow steady;set steady state flow
bo pp=125e6
pfix pressure=125e6

```

```

step 500
sav m2c_5.sav
step 500
sav m2c_6.sav
step 500
sav m2c_7.sav
step 500
sav m2c_8.sav

```

```

step 500
sav m2c_9.sav
step 500
sav m2c_10.sav

```

```

step 500
sav m2c_11.sav
step 500
sav m2c_12.sav

```

```

step 500
sav m2c_13.sav
step 500
sav m2c_14.sav

```

```
return
```

U.8 Model 2d – wet model $\sigma_1 = 112.5^\circ$

```
>1490Ma (Map Interp)MODEL 2 Young Granites- DRY MODEL
```

```
:metasediment properties
prop mat=1 dens 2850 bulk 25e9 shear 25e9 cohesion 10e6 tens 5e6 fric 31 dil 4
```

```
:granite properties
prop mat=2 dens 2650 bulk 49e9 shear 27e9 cohesion 20e6 tens 10e6 fric 37 dil 5
```

```
:contact properties
prop jmat=1 jkn 5e6 jks 1e3 jcoh 4e2 jtens 2e6 jfri 30 jdil 5
:prop jmat=1 jper 300 azero 0.05 ares 0.03
```

```
prop jmat=2 jkn 5e9 jks 1e5 jcoh 10e2 jtens 3e6 jfri 35 jdil 5
:prop jmat=2 jper 238 azero 0.03 ares 0.01
```

```
:Pseudo joints
prop jmat=5 jkn 100e9 jks 40e9 jcoh 190e10 jtens 190e10 jdil 0
:prop jmat=5 jper 0 azero 0 ares 0
```

```
round 100
```

```
block 0,0,0,200000 124000,200000 124000,0
```

```
:*****(Geometry File as per Model 2a)*****
```

```
:Pseudo contacts to reduce block size and allow zoning
```

```

:crack 0 66000 39000 66000;Pj1(left block)
:crack 47000 71000 96000 71000;Pj2(mid block)
:crack 80000 135000 114000 135000;Pj3(rmid block)
:crack 90000 102000 106000 102000;Pj4(rmid block)
:crack 104000 70000 108000 70000;Pj5(rmid block)
:crack 90000 102000 106000 102000;Pj6(rmid block)
crack 88000 110000 90000 110000;Pj7(rmid block)
:crack 103000 127000 113000 127000;Pj8(rmid block)
crack 99000 107000 106000 107000;Pj9(rmid block)
crack 101000 98000 106000 98000;Pj10(rmid block)
:crack 55000 38000 59000 38000;Pj11(rmid block)

```

```

crack    93000    115000    95000    115000;Pj12(rmid block)

hist unbal ; hist1
hist sxx 62000 100000;hist2
hist syy 62000 100000;hist3

hist sst 60000 41000;hist4 selwyn high strain zone
hist sst 43000 40000;hist5 left of gin ck gr
hist sst 69000 98000;hist6 tip of sq. hills gr
hist sst 61000 172000;hist7 cloncurry

sav m2d_block.sav

gen 0 124000 0 200000 auto 1000

insitu stress -210e6 52.5e6 -140e6 szz -175e6
bound stress -210e6 0 -140e6
damp auto

;changing whole model to mat=1 (schist)
change 0 200000 0 124000 mat=1 cons=3

;changing all joints to jmat=1
change 0 200000 0 124000 jmat=1 jcon=2

;changing granite blocks to mat=2 (granite) constit model 3
change 57000,60000,175000,180000 mat=2 con=3 ;gr1
change 83000,85000,126000,129000 mat=2 con=3 ;gr2
change 89000,91000,117000,119000 mat=2 con=3 ;gr3
change 97000,99000,124000,126000 mat=2 con=3 ;gr4
change 94000,96000,117000,119000 mat=2 con=3 ;gr5
change 96000,98000,108000,110000 mat=2 con=3 ;gr6
change 85500,87500,100500,102500 mat=2 con=3 ;gr7
change 98000,100000,97000,99000 mat=2 con=3 ;gr8
change 112000,114000,80000,82000 mat=2 con=3 ;gr9
change 122000,124000,66000,67000 mat=2 con=3 ;gr10
change 53000,55000,45000,47000 mat=2 con=3 ;gr11
change 55000,68000,184000,193000 mat=2 con=3 ;gr12
change 20000,37000,93000,102000 mat=2 con=3 ;gr13
change 6000,24000,45000,66000 mat=2 con=3 ;gr14
change 49000,53000,3000,7000 mat=2 con=3 ;gr15
change 50500,54000,30000,33000 mat=2 con=3 ;gr16
change 64000,73000,26250,27750 mat=2 con=3 ;gr17
change 63000,68000,48000,52000 mat=2 con=3 ;gr18
change 82500,96000,44000,70000 mat=2 con=3 ;gr19
change 122250,123500,19000,22000 mat=2 con=3 ;gr20

;changing granite edges to jmat=2 - must follow commands setting jmat=2 blocks
change jmat=2 range minterface 1 2

;changing pseudo joint properties to jmat=5
change jmat=5 range xr 0,39000 yr 65900 66100 ang -5,5;Pj1 properties
;pl hold mat jo
change jmat=5 range xr 47000,96000 yr 70900 71100 ang -5,5;Pj2 properties
;pl hold mat jo
change jmat=5 range xr 80000,114000 yr 134900 135100 ang -5,5; Pj3 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj4 properties
change jmat=5 range xr 104000,108000 yr 69900 70100 ang -5,5; Pj5 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj6 properties
change jmat=5 range xr 88000,90000 yr 109900 110100 ang -5,5; Pj7 properties
;pl hold mat jo
change jmat=5 range xr 103000,113000 yr 126900 127100 ang -5,5; Pj8 properties
;pl hold mat jo
change jmat=5 range xr 99000,106000 yr 106900 107100 ang -5,5; Pj9 properties
;pl hold mat jo
change jmat=5 range xr 101000,106000 yr 97900 98100 ang -5,5; Pj10 properties
;pl hold mat jo
change jmat=5 range xr 55000,59000 yr 37900 38100 ang -5,5; Pj11 properties
;pl hold mat jo
change jmat=5 range xr 93000,95000 yr 114900 115100 ang -5,5; Pj12 properties

sav m2d_prop.sav

```

```
step 10
sav m2d_stress.sav
```

```
step 500
sav m2d_1.sav
step 500
sav m2d_2.sav
step 500
sav m2d_3.sav
step 500
sav m2d_4.sav
```

```
;Establishing fluid pressure
fluid dens=1000;fluid density of 1000kgm3
set flow steady;set steady state flow
bo pp=125e6
pfix pressure=125e6
```

```
step 500
sav m2d_5.sav
step 500
sav m2d_6.sav
step 500
sav m2d_7.sav
step 500
sav m2d_8.sav
```

```
step 500
sav m2d_9.sav
step 500
sav m2d_10.sav
```

```
step 500
sav m2d_11.sav
step 500
sav m2d_12.sav
```

```
step 500
sav m2d_13.sav
step 500
sav m2d_14.sav
```

```
return
```

U.9 Fluid Discharge Model -xgrad

```
>1490Ma (Map Interp)MODEL 2 Young Granites- DRY MODEL
```

```
;metasediment properties
prop mat=1 dens 2850 bulk 25e9 shear 25e9 cohesion 10e6 tens 5e6 fric 31 dil 4
```

```
;granite properties
prop mat=2 dens 2650 bulk 49e9 shear 27e9 cohesion 20e6 tens 10e6 fric 37 dil 5
```

```
;contact properties
prop jmat=1 jkn 5e6 jks 1e3 jcoh 4e2 jtens 2e6 jfri 30 jdil 5
;prop jmat=1 jper 300 azero 0.05 ares 0.03
```

```
prop jmat=2 jkn 5e9 jks 1e5 jcoh 10e2 jtens 3e6 jfri 35 jdil 5
;prop jmat=2 jper 238 azero 0.03 ares 0.01
```

```
;Pseudo joints
prop jmat=5 jkn 100e9 jks 40e9 jcoh 190e10 jtens 190e10 jdil 0
;prop jmat=5 jper 0 azero 0 ares 0
```

```
round 100
```

```
block 0,0,0,200000 124000,200000 124000,0
```

```
;*****(Geometry File as per Model 2a)*****
```



```

:Pseudo contacts to reduce block size and allow zoning
;crack 0 66000 39000 66000;Pj1(left block)
;crack 47000 71000 96000 71000;Pj2(mid block)
;crack 80000 135000 114000 135000;Pj3(rmid block)
;crack 90000 102000 106000 102000;Pj4(rmid block)
;crack 104000 70000 108000 70000;Pj5(rmid block)
;crack 90000 102000 106000 102000;Pj6(rmid block)
crack 88000 110000 90000 110000;Pj7(rmid block)
;crack 103000 127000 113000 127000;Pj8(rmid block)
crack 99000 107000 106000 107000;Pj9(rmid block)
;crack 101000 98000 106000 98000;Pj10(rmid block)
;crack 55000 38000 59000 38000;Pj11(rmid block)
crack 93000 115000 95000 115000;Pj12(rmid block)

hist unbal ; hist1
hist sxx 62000 100000;hist2
hist syy 62000 100000;hist3

hist sst 60000 41000;hist4 selwyn high strain zone
hist sst 43000 40000;hist5 left of gin ck gr
hist sst 69000 98000;hist6 tip of sq. hills gr
hist sst 61000 172000;hist7 cloncurry

sav m2fgx_block.sav

gen 0 124000 0 200000 auto 1000

insitu stress -210e6 52.5e6 -140e6 szz -175e6
bound stress -210e6 0 -140e6
damp auto

;changing whole model to mat=1 (schist)
change 0 200000 0 124000 mat=1 cons=3

;changing all joints to jmat=1
change 0 200000 0 124000 jmat=1 jcon=2

;changing granite blocks to mat=2 (granite) constit model 3
change 57000,60000,175000,180000 mat=2 con=3 ;gr1
change 83000,85000,126000,129000 mat=2 con=3 ;gr2
change 89000,91000,117000,119000 mat=2 con=3 ;gr3
change 97000,99000,124000,126000 mat=2 con=3 ;gr4
change 94000,96000,117000,119000 mat=2 con=3 ;gr5
change 96000,98000,108000,110000 mat=2 con=3 ;gr6
change 85500,87500,100500,102500 mat=2 con=3 ;gr7
change 98000,100000,97000,99000 mat=2 con=3 ;gr8
change 112000,114000,80000,82000 mat=2 con=3 ;gr9
change 122000,124000,66000,67000 mat=2 con=3 ;gr10
change 53000,55000,45000,47000 mat=2 con=3 ;gr11
change 55000,68000,184000,193000 mat=2 con=3 ;gr12
change 20000,37000,93000,102000 mat=2 con=3 ;gr13
change 6000,24000,45000,66000 mat=2 con=3 ;gr14
change 49000,53000,3000,7000 mat=2 con=3 ;gr15
change 50500,54000,30000,33000 mat=2 con=3 ;gr16
change 64000,73000,26250,27750 mat=2 con=3 ;gr17
change 63000,68000,48000,52000 mat=2 con=3 ;gr18
change 82500,96000,44000,70000 mat=2 con=3 ;gr19
change 122250,123500,19000,22000 mat=2 con=3 ;gr20

;changing granite edges to jmat=2 - must follow commands setting jmat=2 blocks
change jmat=2 range minterface 1 2

;changing pseudo joint properties to jmat=5
change jmat=5 range xr 0,39000 yr 65900 66100 ang -5,5;Pj1 properties
;pl hold mat jo
change jmat=5 range xr 47000,96000 yr 70900 71100 ang -5,5;Pj2 properties
;pl hold mat jo
change jmat=5 range xr 80000,114000 yr 134900 135100 ang -5,5; Pj3 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj4 properties
change jmat=5 range xr 104000,108000 yr 69900 70100 ang -5,5; Pj5 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj6 properties
change jmat=5 range xr 88000,90000 yr 109900 110100 ang -5,5; Pj7 properties

```

```
;pl hold mat jo
change jmat=5 range xr 103000,113000 yr 126900 127100 ang -5,5; Pj8 properties
;pl hold mat jo
change jmat=5 range xr 99000,106000 yr 106900 107100 ang -5,5; Pj9 properties
;pl hold mat jo
change jmat=5 range xr 101000,106000 yr 97900 98100 ang -5,5; Pj10 properties
;pl hold mat jo
change jmat=5 range xr 55000,59000 yr 37900 38100 ang -5,5; Pj11 properties
;pl hold mat jo
change jmat=5 range xr 93000,95000 yr 114900 115100 ang -5,5; Pj12 properties

sav m2fgx_prop.sav
step 10
sav m2 fgx _stress.sav

step 500
sav m2 fgx _1.sav
step 500
sav m2 fgx _2.sav
step 500
sav m2 fgx _3.sav
step 500
sav m2 fgx _4.sav

;Establishing fluid pressure
fluid dens=1000;fluid density of 1000kgm'3
set flow steady;set steady state flow
bo pp=125e6
pfix pressure=125e6

step 500
sav m2 fgx _5.sav
step 500
sav m2 fgx _6.sav
step 500
sav m2 fgx _7.sav
step 500
sav m2 fgx _8.sav

;Flow Modelling no Mechanical deformation
set mech off;suppressing mechanical deformation
pfix pressure=0
bo pp=0
step 10;allow settling
pfree
step 10; allow settling

; Apppling fluid pressure gradient of 1Mpa in x direction
bo pp 1e6 pxgrad -1e6 range 0 200000 -1 1
bo pp 1e6 pxgrad -1e6 range 0 200000 123999 124001
bo pp 0 range 123999 124001 0 200000
bo pp 1e6 range -1 1 0 200000

; flow calculation
step 500
sav m2_fgx_9.sav
step 500
sav m2_fgx_10.sav

step 500
sav m2_fgx_11.sav
step 500
sav m2_fgx_12.sav

step 500
sav m2_fgx_13.sav
step 500
sav m2_fgx_14.sav

return
```

U.10 Fluid Discharge Model – granite fluid source

```

;>1490Ma (Map Interp)MODEL 2 Young Granites- DRY MODEL

:metasediment properties
prop mat=1 dens 2850 bulk 25e9 shear 25e9 cohesion 10e6 tens 5e6 fric 31 dil 4

:granite properties
prop mat=2 dens 2650 bulk 49e9 shear 27e9 cohesion 20e6 tens 10e6 fric 37 dil 5

:contact properties
prop jmat=1 jkn 5e6 jks 1e3 jcoh 4e2 jtens 2e6 jfri 30 jdil 5
:prop jmat=1 jper 300 azero 0.05 ares 0.03

prop jmat=2 jkn 5e9 jks 1e5 jcoh 10e2 jtens 3e6 jfri 35 jdil 5
:prop jmat=2 jper 238 azero 0.03 ares 0.01

:Pseudo joints
prop jmat=5 jkn 100e9 jks 40e9 jcoh 190e10 jtens 190e10 jdil 0
:prop jmat=5 jper 0 azero 0 ares 0

round 100
block 0,0 0,200000 124000,200000 124000,0

:*****(Geometry File as per Model 2a)*****
:Pseudo contacts to reduce block size and allow zoning
:crack 0 66000 39000 66000;Pj1(left block)
:crack 47000 71000 96000 71000;Pj2(mid block)
:crack 80000 135000 114000 135000;Pj3(rmid block)
:crack 90000 102000 106000 102000;Pj4(rmid block)
:crack 104000 70000 108000 70000;Pj5(rmid block)
:crack 90000 102000 106000 102000;Pj6(rmid block)
crack 88000 110000 90000 110000;Pj7(rmid block)
:crack 103000 127000 113000 127000;Pj8(rmid block)
crack 99000 107000 106000 107000;Pj9(rmid block)
crack 101000 98000 106000 98000;Pj10(rmid block)
:crack 55000 38000 59000 38000;Pj11(rmid block)
crack 93000 115000 95000 115000;Pj12(rmid block)

hist unbal ; hist1
hist sxx 62000 100000;hist2
hist syy 62000 100000;hist3

hist sst 60000 41000;hist4 selwyn high strain zone
hist sst 43000 40000;hist5 left of gin ck gr
hist sst 69000 98000;hist6 tip of sq. hills gr
hist sst 61000 172000;hist7 cloncurry

sav m2fs_block.sav

gen 0 124000 0 200000 auto 1000

insitu stress -210e6 52.5e6 -140e6 szz -175e6
bound stress -210e6 0 -140e6
damp auto

:changing whole model to mat=1 (schist)
change 0 200000 0 124000 mat=1 cons=3

:changing all joints to jmat=1
change 0 200000 0 124000 jmat=1 jcon=2

:changing granite blocks to mat=2 (granite) constit model 3
change 57000,60000,175000,180000 mat=2 con=3 ;gr1
change 83000,85000,126000,129000 mat=2 con=3 ;gr2
change 89000,91000,117000,119000 mat=2 con=3 ;gr3
change 97000,99000,124000,126000 mat=2 con=3 ;gr4
change 94000,96000,117000,119000 mat=2 con=3 ;gr5
change 96000,98000,108000,110000 mat=2 con=3 ;gr6
change 85500,87500,100500,102500 mat=2 con=3 ;gr7
change 98000,100000,97000,99000 mat=2 con=3 ;gr8
change 112000,114000,80000,82000 mat=2 con=3 ;gr9
change 122000,124000,66000,67000 mat=2 con=3 ;gr10

```

```
change 53000,55000,45000,47000 mat=2 con=3 ;gr11
change 55000,68000,184000,193000 mat=2 con=3 ;gr12
change 20000,37000,93000,102000 mat=2 con=3 ;gr13
change 6000,24000,45000,66000 mat=2 con=3 ;gr14
change 49000,53000,3000,7000 mat=2 con=3 ;gr15
change 50500,54000,30000,33000 mat=2 con=3 ;gr16
change 64000,73000,26250,27750 mat=2 con=3 ;gr17
change 63000,68000,48000,52000 mat=2 con=3 ;gr18
change 82500,96000,44000,70000 mat=2 con=3 ;gr19
change 122250,123500,19000,22000 mat=2 con=3 ;gr20

;changing granite edges to jmat=2 - must follow commands setting jmat=2 blocks
change jmat=2 range minterface 1 2

;changing pseudo joint properties to jmat=5
change jmat=5 range xr 0,39000 yr 65900 66100 ang -5,5;Pj1 properties
;pl hold mat jo
change jmat=5 range xr 47000,96000 yr 70900 71100 ang -5,5;Pj2 properties
;pl hold mat jo
change jmat=5 range xr 80000,114000 yr 134900 135100 ang -5,5; Pj3 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj4 properties
change jmat=5 range xr 104000,108000 yr 69900 70100 ang -5,5; Pj5 properties
;pl hold mat jo
;change jmat=5 range xr 90000,106000 yr 101900 102100 ang -5,5; Pj6 properties
change jmat=5 range xr 88000,90000 yr 109900 110100 ang -5,5; Pj7 properties
;pl hold mat jo
change jmat=5 range xr 103000,113000 yr 126900 127100 ang -5,5; Pj8 properties
;pl hold mat jo
change jmat=5 range xr 99000,106000 yr 106900 107100 ang -5,5; Pj9 properties
;pl hold mat jo
change jmat=5 range xr 101000,106000 yr 97900 98100 ang -5,5; Pj10 properties
;pl hold mat jo
change jmat=5 range xr 55000,59000 yr 37900 38100 ang -5,5; Pj11 properties
;pl hold mat jo
change jmat=5 range xr 93000,95000 yr 114900 115100 ang -5,5; Pj12 properties

sav m2fslong_prop.sav
step 10
sav m2 fslong _stress.sav
step 500
sav m2 fslong _1.sav
step 500
sav m2 fslong _2.sav
step 500
sav m2 fslong _3.sav
step 500
sav m2 fslong _4.sav

;Establishing fluid pressure
fluid dens=1000
set flow steady
bo pp=10e6
pfix pressure=10e6

step 500
sav m2fslong _5.sav
step 500
sav m2fslong _6.sav
step 500
sav m2fslong _7.sav
step 500
sav m2fslong _8.sav

;suppressing mech and applying fluid gradient
set mech off
pfix pressure=0
bo pp=0
step 10
pfree
step 10

;Applying fluid source to granites low fluid rate
well dom 89024 flow 1e-6;gr12
well dom 89792 flow 1e-6;
```

```
well dom 90560 flow 1e-6;
well dom 9950 flow 1e-6;gr13
well dom 118222 flow 1e-6;
well dom 119292 flow 1e-6;
well dom 120306 flow 1e-6;
well dom 116152 flow 1e-6;
well dom 116200 flow 1e-6;
well dom 130662 flow 1e-6;
well dom 129996 flow 1e-6;
well dom 123130 flow 1e-6;
well dom 124850 flow 1e-6;gr14
well dom 126328 flow 1e-6;
well dom 128356 flow 1e-6;
well dom 128404 flow 1e-6;
well dom 19610 flow 1e-6;gr1
well dom 131862 flow 1e-6;gr16
well dom 134896 flow 1e-6;gr17
well dom 136288 flow 1e-6;
well dom 134560 flow 1e-6;
well dom 134752 flow 1e-6;
well dom 142218 flow 1e-6;gr18
well dom 141492 flow 1e-6;
well dom 154190 flow 1e-6;
well dom 154612 flow 1e-6;gr19
well dom 155402 flow 1e-6;
well dom 156904 flow 1e-6;
well dom 157184 flow 1e-6;
well dom 143934 flow 1e-6;
well dom 144126 flow 1e-6;
well dom 146116 flow 1e-6;
well dom 149784 flow 1e-6;
well dom 149832 flow 1e-6;
well dom 150024 flow 1e-6;
well dom 150674 flow 1e-6;
well dom 159134 flow 1e-6;gr20
well dom 159468 flow 1e-6;
```

```
step 500
sav m2fslong_9.sav
step 500
sav m2fslong_10.sav
step 500
sav m2fslong_11.sav
step 500
sav m2fslong_12.sav
step 5000
sav m2fslong_13.sav
step 5000
sav m2fslong_14.sav
step 5000
sav m2fslong_15.sav
step 5000
sav m2fslong_16.sav
step 5000
sav m2fslong_17.sav
step 5000
sav m2fslong_18.sav
step 5000
sav m2fslong_19.sav
step 5000
sav m2fslong_20.sav
step 50000
sav m2fslong_21.sav
step 50000
sav m2fslong_22.sav
step 50000
sav m2fslong_21.sav
step 50000
sav m2fslong_23.sav
step 50000
sav m2fslong_24.sav
step 50000
sav m2fslong_25.sav
```

```
return
```